AD-A165 651 FATIGUE ANALYSIS EAST COAST AIR COMBAT MANEUVERING RANGE OFFSHORE KITTY H. (U) CREST ENGINEERING INC TULSA OK SEP 76 27-771-100 CHES/NAVFAC-FPO-7616 N62477-76-C-0179 F/G 13/13 1/6 UNCLASSIFIED NĽ



MICROCOPY RESOLUTION TEST CHART
NATIONAL BURFAU OF STANDARDS 1963 A

PREPARED FOR ITIES ENGINEER ATMENT OF TH

The ocean structure investigated herein, a three-pile structure with

20. DISTRIBUTION/AVAILABILITY OF ABSTRACT 21. ABSTRACT SECURITY CLASSIFICATION

22b. TELEPHONE

202-433-3881

22c. OFFICE SYMBO

SECURITY CLASSIFICATION OF THIS PAGE

Offshore Kitty Hawk, North Carolina.

22a. NAME OF RESPONSIBLE INDIVIDUAL

SAME AS RPT.

Jacqueline B. Riley

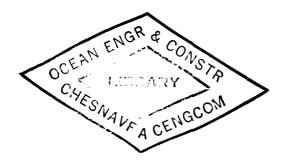
DD FORM 1473, 84MAR

BLOCK 19 (Con't)

Action (Contractor) (Contractor)

equilaterally spaced jacket legs, is installed in a water depth (MLW) of 105 feet. The structure is secured to the ocean floor permanently by tubular piles through the jacket legs into the seabed. A superstructure is attached to the piling above the jacket.

•••



Securify Managen second second formal second

FATIGUE ANALYSIS

EAST COAST AIR COMBAT MANEUVERING RANGE

OFFSHORE KITTY HAWK, NORTH CAROLINA

CONTRACT NO. N62477-76-C-0179

MODIFICATION NO. P0001

Report No. 27-771-100

Prepared for

NAVAL FACILITIES ENGINEERING COMMAND DEPARTMENT OF THE NAVY CHESAPEAKE DIVISION

Ву

CREST ENGINEERING, INC. TULSA, OKLAHOMA

DISCLAIMER NOTICE

THIS DOCUMENT IS BEST QUALITY PRACTICABLE. THE COPY FURNISHED TO DTIC CONTAINED A SIGNIFICANT NUMBER OF PAGES WHICH DO NOT REPRODUCE LEGIBLY.

TABLE OF CONTENTS :

SECTION	TITLE	PAGE	
1.0	INTRODUCTION		
	1.1 Introduction 1.2 Engineering Data 1.3 Procedures of Analysis 1.4 Summary 1.5 Personnel Resumes	1.01 1.02 1.04 1.05 1.06	
2.0	ELEVATIONS AND PLANS		
	2.1 Introduction 2.2 Elevations and Plans	2.01 2.02	
3.0	WAVE FORCES ON STRUCTURE		
4.0	3.1 Introduction 3.2 Percentage Distribution of Wave Height Occurrence 3.3 Drag and Inertia Coefficients 3.4 Current Velocity Distribution Profiles 3.5 Wave Height and Base Shear Relationship 3.6 Tranfer Function	3.01 3.02 3.04 3.05 3.18 3.32	
4.0	FATIGUE LIMIT STRESS ;	4 01	
	 4.1 Introduction 4.2 Punching Shear Stress Range vs. Cycles of Load 4.3 Punching Shear Stress Range vs. Wave Height 4.4 Limit Punching Shear Stress for Fatigue 4.5 Nominal Brace Stress Range vs. Cycles 	4.01 4.02 4.04 4.11	
	of Load 4.6 Nominal Brace Stress Range vs. Wave Height 4.7 Limit Nominal Brace Stress for Fatigue 4.8 Hurricane Effects on Fatigue Limit Stress 4.9 Fatigue Strength of a T-Joint	4.13 4.14 4.21 4.23 4.32	
5.0	FATIGUE LIFE OF STRUCTURE '		
	 5.1 Introduction 5.2 Fatigue Life - Punching Shear Stress Control 5.3 Fatigue Life - Nominal Brace Stress Control 	5.01 5.02 5.03	
6.0	MODIFIED GOODMAN DIAGRAM FOR DESIGN .		
	6.1 Introduction6.2 AWS Allowable Fatigue Stress Range	6.01 6.02	

SECTION	TITLE		
	6.3	Modified Goodman Diagram for Simple T, Y and K Joints - Nominal Brace Stress	6.04
	6.4	Modified Goodman Diagram for Simple K Joints - Punching Shear Stress	6.06
	6.5 6.6	Safe Nominal Brace Stress Range for Fatigue Safe Punching Shear Stress Range for Fatigue	6.09 6.10

7.0 REFERENCE

APPENDICES

- A. PUNCHING SHEAR STRESS
 - A.1 Punching Shear Stress K-Joints 105' MLW Jacket

07 ft. Wave Height - Load Condition #1 & #2

17 ft. Wave Height - Load Condition #3 & #4

27 ft. Wave Height - Load Condition #5 & #6

42 ft. Wave Height - Load Condition #7 & #8

- A.2 Punching Shear Stress T-Joints Design Wave 105' MLW Jacket
- A.3 Punching Shear Stress T-Joints Design Wave 93 MLW Jacket
- A.4 Punching Shear Stress T-Joints Design Wave 81' MLW Jacket
- B. STRESS ANALYSIS

07 ft. Wave Height - Load Condition #1 & #2

17 ft. Wave Height - Load Condition #3 & #4

27 ft. Wave Height - Load Condition #5 & #6

42 ft. Wave Height - Load Condition #7 & #8

C. WAVE FORCES .--

02 ft. Wave Height

07 ft. Wave Height

12 ft. Wave Height

17 ft. Wave Height

22 ft. Wave Height

27 ft. Wave Height

32 ft. Wave Height

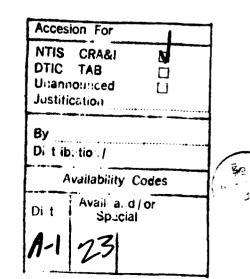
37 ft. Wave Height

42 ft. Wave Height

47 ft. Wave Height

52 ft. Wave Height

57 ft. Wave Height



BESTELLIN HARRY (BESTELLIN BESTELLIN BELLEVA), BELLEVA), KALL

SECTION 1

INTRODUCTION

1.1 INTRODUCTION

*This report evaluates the fatigue limit strengths for the design of a tripod-type ocean structure for the East Coast Air Combat Maneuvering Range Offshore Kitty Hawk, North Carolina.

The ocean structure investigated herein, a three-pile structure with equilaterally spaced jacket legs, is installed in a water depth (MLW) of 105 feet. The structure is secured to the ocean floor permanently by driving tubular piles through the jacket legs into the seabed. A superstructure is attached to the piling above the jacket.

ENGINEERING DATA 1.2

Engineering data which serves as the basis for the fatigue analysis are listed as follows:

Environmental Conditions A.

105 feet MLW Depth

Wave and Current Characteristics

Provided in Glenn and Associates Report:

NORMAL WAVES, AND STORM WIND, TIDE, WAVE

AND CURRENT CHARACTERISTICS, AND WAVE

FORCES: VICINITY 36°N, 75°W, OFFSHORE

KITTY HAWK, NORTH CAROLINA, May 1976

Drag Coefficient above MLW	$C_D = 0.74$
Drag Coefficient below MLW	$c_0 = 1.02$
Inertial Coefficient	$C_{M} = 1.34$
Fouling Thickness below MLW	2 inches

Major Structural Dimensions В.

True Batter of Piling & Jacket Leg	1:6	
Width at Jacket Base (Mudline)	64 feet	
Width at Jacket Top (Work Point Level)	29 feet	
Pile Out Side Diameter	42 inches	
Jacket Leg Out Side Diameter	45.5 inches	
Upper Deck Area	362.5 sq. ft.	
Equipment Deck Area	591.5 sq. ft.	

Height of Structure (From Mudline to Upper Deck)

180 feet

C. <u>Material</u>

All structural shapes or fabricated tubular goods are ASTM A-36 Structural Steel except for the material used for the joint cans which is ASTM A-633, Grade A.

1.3 PROCEDURES OF ANALYSIS

The significant parameters relative to the fatigue strength analysis of the ocean structures are, structural geometry, member sizes, wave characteristics and wave height distribution, dynamic response of the structure, and the yield strength of the material.

The geometry of the idealized platform structure* under consideration is given in Section 2. This structure is subjected to a sequence of lateral loads produced by waves of varying heights and periods. A total of 12 waves with wave heights ranging from 2 feet to 57 feet at 5 feet increment are analyzed. The relationship of structural base shear to wave force is expressed graphically in Section 3. Transfer functions relating the wave height and the base shear of the structure are established accordingly.

Reference 4 presents closed-form method of analysis for determining the fatigue damage attributing ocean waves to structures having dynamic amplification characteristics of negligible magnitude. The aforementioned technique is applied in Section 4 to evaluate the fatigue limit stress. In the process of numerical computations, four waves with wave heights of 7, 17, 27 and 42 feet, respectively, are selected to produce lateral loads on the idealized platform structure. Evaluation of fatigue limit stress for two joints in the structure are considered for the cases of consistent appearance of

^{*} The structural geometry and member properties were developed in Report No. 27-771-96.

severe storms and of the infrequent hurricane effects on the fatigue strength over the lifetime of the structure. The predicted fatigue life of the structure is then presented in Section 5.

In Section 6 are given the safe nominal brace stress range and safe punching shear stress range for fatigue. Both stress ranges are expressed by means of Modified Goodman Diagram.

1.4 SUMMARY

The results of the study on the fatigue analysis may be drawn as follows:

Fatigue Limit Stress:

Punching Shear Stress Range (K-Joint)	11,523 psi
Punching Shear Stress Range (T-Joint)	6,100 psi
Nominal Brace Stress Range	22,000 psi

Fatigue Life:

Fatigue Life Controlled by Punching	
Shear Stress (K-Joint)	140 years
Fatigue Life Controlled by Punching	
Shear Stress (T-Joint)	20 years
Fatigue Life Controlled by Nominal	
Brace Stress	741 years

1.5 PERSONNEL RESUMES

The personnel whose resumes follow were actively engaged in this project.

CREST OFFSHORE, INC.





Chingmiin (Charlie) Chern

Senior Engineer

University	Degree	Year
National Taiwan	Bachelor of Science	
University	Civil Engineering	1961
North Dakota	Master of Science	
State University	Civil Engineering	1966
Lehigh	Ph. D.	
University	Civil Engineering	1969
Tulsa University	Graduate Study in	
•	Business Administration-	
	Management	1974



Member American Society of Civil Engineers Member International Association of Structural and Bridge Engineers

Member American Society of Engineering Education Registered Professional Engineer in Oklahoma

Experience:

1973 to Present

Crest Offshore, Inc.

Senior Civil Engineer Engaged in the feasibility studies, structural analysis and design of offshore structures, equipment supports and other various types of petroleum related civil engineering works. Assignments include:

- ... Evaluation of engineering designs from other agencies.
- ... Analysis and design of offshore structures for oil industry.
- ... Analysis and design of supports and foundations for onshore refinery facilities.
- ... Development of a sequence of computer programs for the analysis of offshore structures.



eat herresess expressed thesisines passaged annihity consider passage.

CREST OFFSHORE, INC.

Chingmiin (Charlie) Chern

Senior Civil Engineer

Experience Continued:

1969 to 1973	North	Dakota	State	University

Associate Engaged in fu Professor of engineering (engineering tion management)

Engaged in full-time lecture instruction for civil engineering (graduate school division) and construction management. Also served as consultant to local industry (undergraduate school division) in the area of computer applications in engineering.

1966 to 1969 Fritz Engineering Laboratory

Research Assisted in the design and testing of various types of steel structures.

1966 North Dakota State Highway Department

Highway Responsible for construction surveying. Engineer

1965 U.S. Forest Service

Assistant Assisted in surveying responsibilities.

Crew Chief

SECTION 2 ELEVATIONS AND PLANS

2.1 INTRODUCTION

The idealized platform structure shown in this section was obtained from Report NO. 27-771-96.

CREST OFFSHORE, INC.

Sheet 2:02 of _16__

By C. Chern Client U.S. NAVY ___ subject Fatigue Analysis ____ Date B = 5 = 76 Job No. 27 - 771-100 _ calculation Elevations & Plans ____

2.2 ELEVATIONS AND PLANS

CREST OFFSHORE, INC. Sheet 2.03 of 16_ By C. Chern client U.S. NAUX _ subject Fatigue Analysis _ _ Date 8=5-76 Job No. 27-771-100_ calculation Elevations & Plans EL (+) 75'-0" EL.(+) 60'-0" EL. (+) 45'-0" EL. (+) 16'-6" EL. (+) 12'-0" च्छि हो देख MLW EL. 000" EL.G) 13'-0" Θ EL.6) 41'-0"

EL(-)105'-0"

(00)

1

(ii)

FV.

OFFSHORE, INC. **CREST** Sheet 2:04 of 16__ By C. Chern CHANY __ Subject Footique Analysis_ Date 8-5-76 Job No. 27-77-100 _ calculation Flexations & Plans _ EL.(+) 75' - 0" EL. (+) 60'-0" EL.(+) 45'-0" EL.(+) 16'-6" EL (+) 12'-0" *(*50*3*) 50)513/510 MLW EL.(+) 0'-0" EL.(-) 13'-0" (70%) EL.(-)41'-0" EL.(-) 73'-0"

EL.(-) 105'-0"

8

žų,

CREST OFFSHORE, INC.

Sheet Z ___of _ Z ___

By _ CVET Client 11.5 SAVY _ Subject Fortigue Analysis _ ____

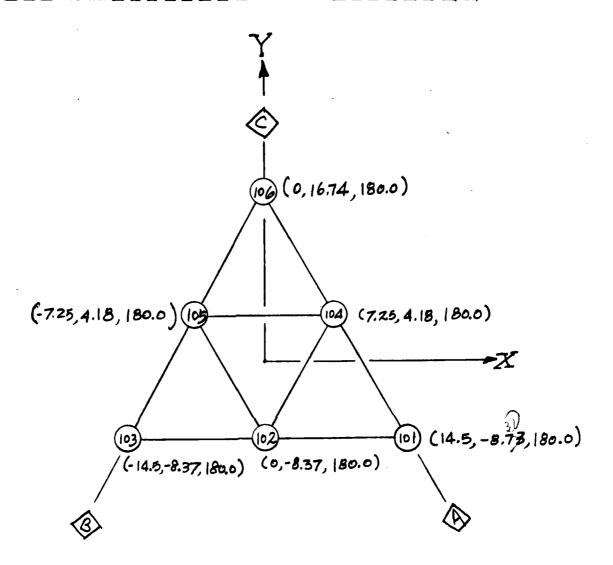
Date 3-5-Zh Job No. 27-771-100 Calculation Elevations # Hans _ ___

EL.(+) 75'-0" EL.(+) 60'-0" EL. (+) 45'-0" EL. (+) 16'-6" EL. (+) 12'-0" MLW EL. (+) 0'-0" Ei. (-) 13'-0" EL.(-)41'-0" EL.(-)73 -0" 1911)

1

15

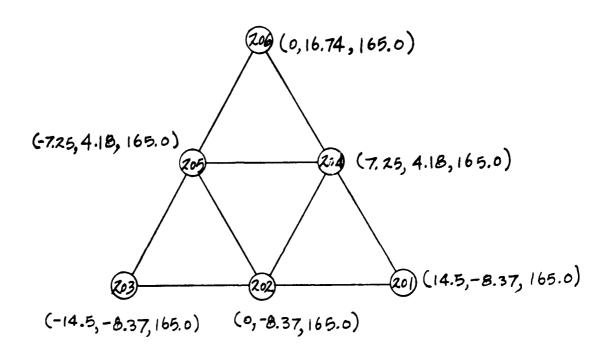
By C. Chern client U.S. NAVX _ subject Fatigue Analysis _ _ _ _ Date 8-5-76 Job No. 27-771-100_ calculation Elevations & Plans _ _ _



PLAN @ EL. (+) 75'-0"
Upper Deck

 ∇^τ

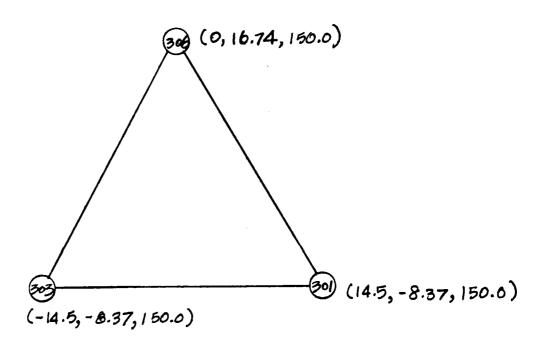
By C. Chern client U.S. NAVY _ subject Fatigue Analysis _ ___ Date 8-5-76 Job No. 27-77/-100 _ calculation Elevations & Plans _ _



PLAN @ EL. (+) 60'-0"

Equipment Deck

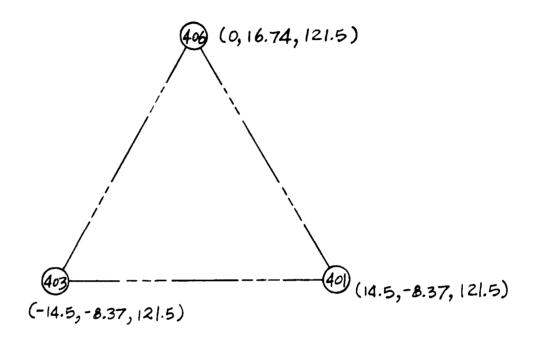
By C. Chern _ client U.S. NAUY _ subject Fatigue Analysis _ ____
Date 8-5-76 Job No. 27-771-100 _ calculation Elevations & Plans _ ___



PLAN @ EL.(+) 45'-0"

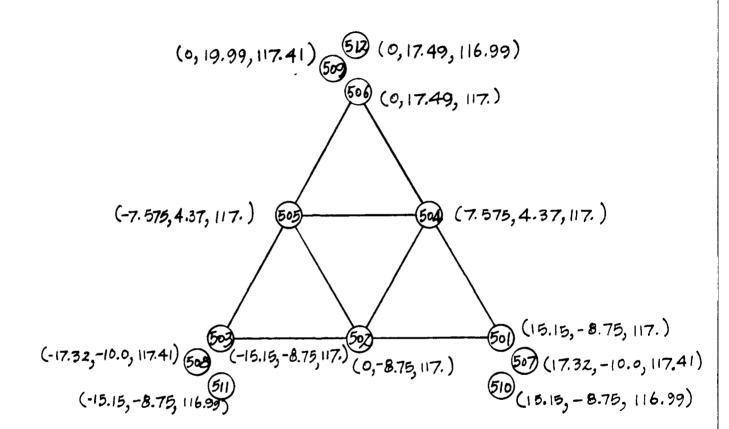
By C. Chern Client U.S. NAVY __ subject Fatigue Analysis _____

Date 8-5-76 Job No. 27-72/-100 _ Calculation Elevations & Plans ____



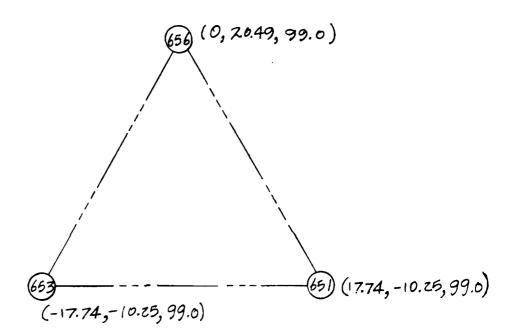
PLAN @ EL.(+) 16'-6"

By C. Chern Client U.S. NAVY __ subject Fatigue Analysis _____
Date 8-5-76 Job No. 27-771-100 _ calculation Elevations & Plans ____



PLAN @ EL. (+) 12'-0"

By C. Chern client U.S. NAUY __ subject Fatigue Analysis _____ Date 8-5-76 Job No. 27-771-100 _ calculation Elevations & Plans ____

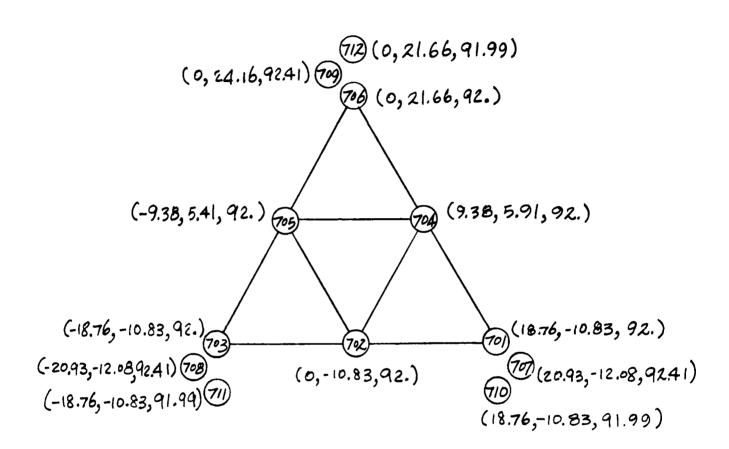


PLAN @ EL. (-) 6'-0"

4

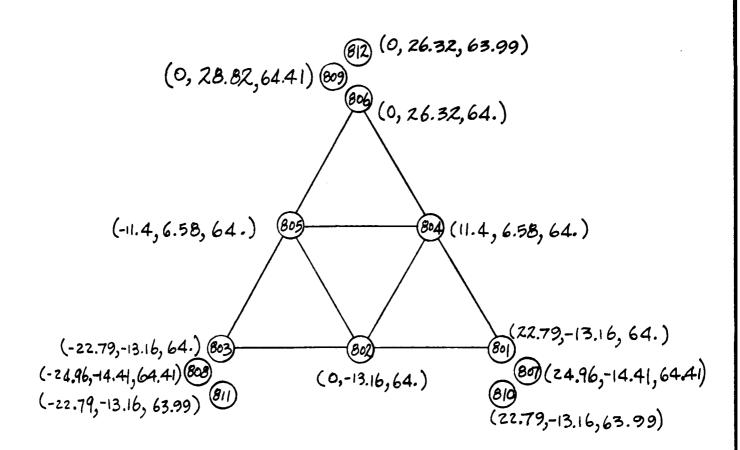
Sheet 2 - 12 of 16

By C. Chern Client U.S. NAVY __ subject Fatigue Analysis ____ Date 8-5-76 Job No. 27-77/-100 _ calculation Elevations & Plans ____



PLAN @ EL. (-) 13'-0"

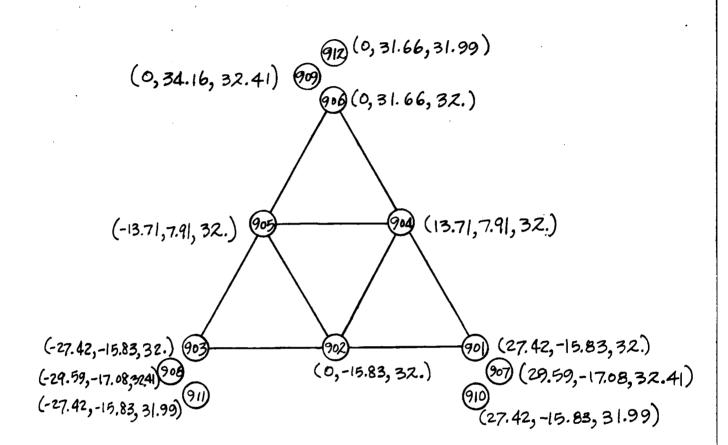
By C. Chern client U.S. NAUY __ subject Fatigue Analysis _____ Date 8-5-76 Job No. 27-771-100 _ calculation Flevations & Plans ____



PLAN @ EL. (-) 41'-0"

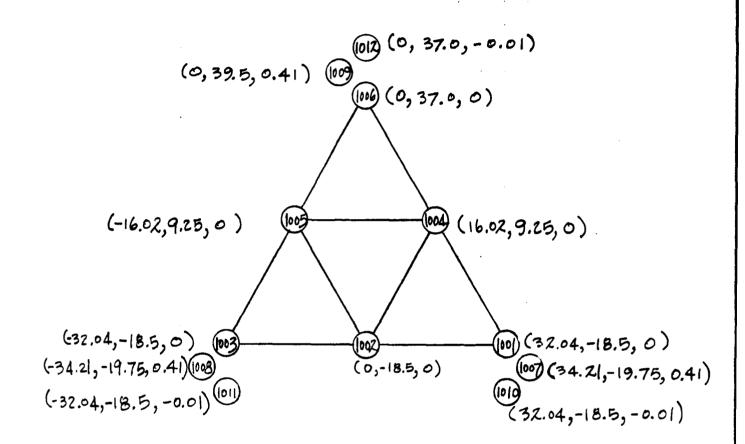
Ciri

By C. Chern Client U.S. NAUY __ subject Fatigue Analysis _____
Date 8-5-Za Job No. 27-JZL-100_ calculation Flexations & Plans ____



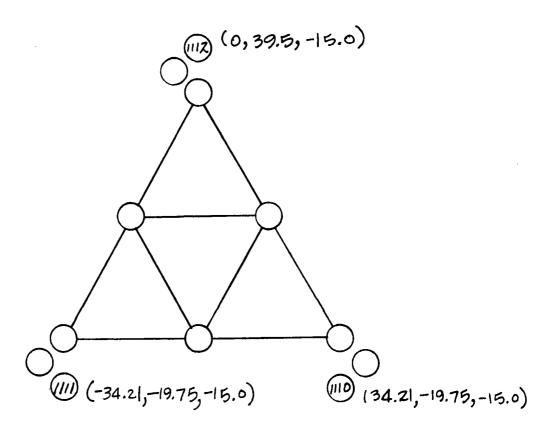
PLAN @ EL. (-) 73-0"

By C. Chern client U.S. NAUX _ subject Fatigue Analysis _ ___ Date 8-5-76 Job No. 27-771-100_ calculation Elevations & Plans _ ___



PLAN @ EL.(-) 105-0"

By C. Chern client U.S. NAIV subject Fatigue Analysis _______
Date 8-5-76 Job No. 27-771-100 calculation Elevations & Plans ____



PLAN @ EL. (-) 120'-0"

SECTION 3

WAVE FORCES ON STRUCTURE

3.1 INTRODUCTION

Base shears on the platform structure attributable to waves and ocean currents are presented hereinafter. Stoke's Fifth Order Gravity Wave Theory* was employed to perform the calculation of wave forces on the structure. In the computations, it was assumed that the approaching wave direction was at 60 degrees with respect to the X-axis (See Page 2.06).

A transfer function relating the base shear and wave height relationship was obtained by means of the least squares approximation.

Computer printout of the wave force is compiled in APPENDIX C.

^{*} A computer program on Stoke's Theory is available through Synercom Technology, Inc., Houston, Texas

CREST OFFSHORE, INC.

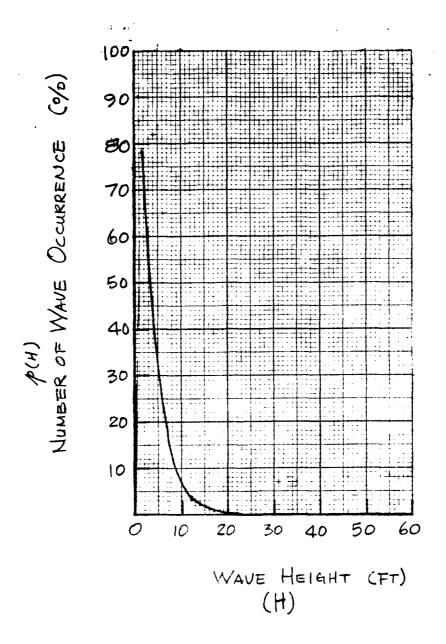
Sheet 3.02 of 41

By C. Cherne client U.S. NAUY _ subject Fatigue Analysis _____ Date 6-30-76 Job No. 27-771-100 _ calculation Wave Forces on Structure _

3.2 PERCENTAGE DISTRIBUTION OF WAVE HEIGHT OCCURRENCE

REF: Table 39, Glenn's Report

WAVE HEIGHT CATEGORY (FEET)	NUMBER OF Waves	PERCENTAGE OF OCCURRENCE
0-4 (2)	76,040,000	.76.932
5-9 (7)	18,380,000	18,596
10-14 (12)	3,563,000	3.605
15-19 (17)	689,000	0.697
20-24 (22)	135,400	0.137
25-29 (27)	26, 250	0.027
30 - 34 (32)	5,100	0.005
35-39 (37)	999	0.001
40 - 44 (42)	200	0.000
45-49 (47)	41	0.000
50-54(52)	8	0,000
55-59 (57)	2	0.000
SUMMATION	98,840,000	100.000



Probability Density Function p(H)

Sheet 3:04 of 41___

By C. Chara client U.S. NAUX _ subject Fatigue Analysis _ ____ Date 6-30-76 Job No. 27-771-100 _ calculation Wave Forces on Structure

3.3 DRAG AND INERTIA COEFFICIENTS

The following values are used in the computer program to produce wave forces on the structure:

Drag Coefficient:

CD = 0.74 for members above MLW = 1.02 for members below MLW

Inertia Coefficient:

Cm = 1.34 for all members

Marine Fouling

Addition of 2-inch on effective diameter for members below MLW.

Sheet ____ of 41___

By C. Chern client U.S. NAVX _ subject Fatigue Analysis _ ___ Date 8 = 5 = 76 Job No. 27 = 77/- 100 _ calculation Wave Forces on Structure _

3.4 CURRENT VELOCITY DISTRIBUTION PROFILES

Ref.: A.H. Glerin & Associates Report.

Sheet 3:06 of 41__

By C. Chern client U.S. NAVY __ subject Fatigue Analysis _____ Date 7-1-76 Job No. 27-771-100 _ calculation Wave Forces on Structure __

Wave Height = 2 FT Reviod = 5.9 Sec.

Total Tide = 1.7 FT

Still Water Level = 105 + 1.7 = 106.7 FT

Surface Current = 1.3 ft/sec. = 0.8 knot

			
ELEVATION ABOVE	l .		CURRENTVELOCITY
MUDLINE (FT)	OF DEPTH	OF SURFACE CURRENT	(FT/SEC)
106.7	0	100	1.3 (0.8)
96.0	10	93	1.2 (0.7)
8 5.4	20	84	1.1 (0.7)
74.7	. 30	77	1.0 (0.6)
64.0	40	70	0.9 (0.5)
53.4	50	64	0.8 (0.5)
42.7	60	55	0.7 (0.4)
32.0	70	48	0.6 (0.4)
21.3	80	41	0.5 (0.3)
10.7	90	32	0.4 (0.2)
0	100	14	0.2 (0.1)

Sheet 3.0 Zot 41__

By C. Chern client U.S. NAUX _ subject Fatigue Analysis _ ____ Date 7-1-76 Job No. 27-771-100 _ calculation Wave Forces on Structure _ _

Wave Height = 7 FT Period = 7.6 Sec.

Total Tide = 1.9 FT

Still Water Level = 105 + 1.9 = 106.9 FT

Surface Current = 1.3 ft/sec. = 0.8 knot

ELEVATION ABOVE MUDLINE (FT)		PERCENTAGE OF SURFACE CURRENT	CURRENT VELOCITY (FT/SEC)
106.9	. 0	100	1.3 (0.8)
96.2	10	93	1.2 (0.7)
85.5	20	84	1.1 (0.7)
74.8	. 30	フフ	1.0 (0.6)
64.	40	70	0.9 (0.5)
53.4	50	64	0.8 (0.5)
42.7	60	55	0.7 (0.4)
32.0	70	48	0.6 (0.4)
21.3	80	41	0.5 (0.3)
10.7	90	32	0,4 (0,2)
O	100	14	0.2 (0.1)

Sheet 3:08 of 41__

By C. Chern client U.S. NAUY __ subject Fatigue Analysis _____ Date 7-1-76 Job No. 27-771-100 _ calculation Wave Forces on Structure _

Wave Height = 12 FT Reviod = 8.3 Sec.

Total Tide = 2.2 FT

Still Water Level = 105 + 2.2 = 107.2 FT

Surface Current = 1.4 ft/sec = 0.8 knot

ELEVATION ABOVE	PERCENTAGE	PERCENTAGE	CURRENTVELOCITY
MUDLINE (FT)	OF DEPTH	OF SURFACE CURRENT	(FT/SEC)
107.2	0	100	1.4 (0.8)
96.5	10	93	1.3 (0.8)
85.8	20	84	1.2 (0.7)
75.0	30	77	1.1 (0.7)
64.3	40	70	1.0 (0.6)
53.6	50	64	0.9 (0.5)
42.9	60	55	0.8 (0.5)
32.2	70	48	0.7 (0.4)
21.4	80	41	0.6 (0.4)
10.7	90	32	0.4 (0.2)
0	100	14	0.2 (0.1)





Sheet 3.02 of 41__

By C. Chern client U.S. NAVY _ subject Fatigue Analysis _ ____ Date 7-1-76 Job No. Z7-771-100 _ calculation Wave Forces on Structure ___

Wave Height = 17 FT Reviod = 8.8 Sec.

Total Tide = 2.7 FT

Still Water Level = 105 + 2.7 = 107.7 FT

Surface Current = 1.5 ft/sec. = 0.9 knot

ELEVATION ABOVE MUDLINE (FT)	PERCENTAGE OF DEPTH	PERCENTAGE OF SURFACE CURRENT	CURRENT VELOCITY (FT/SEC)
107.7	0	100	1.5 (0.9)
96.9	10	93	1.4 (0.8)
86.2	20	84	1.3 (0.8)
75.4	. 30	77	1.2 (0,7)
64.6	40	70	1.1 (0.7)
53.9	50	64	1.0 (0.6)
43.1	60	55	0.8 (0.5)
32.3	70	48	0.7 (0.4)
21.5	80	4-1	0.6 (0.4)
10.3	90	32	0.5 (0.3)
0	100	14	0.2 (0.1)

Sheet 3:12 of 41__

By C. Chern Client U.S. NAUY __ subject Fatigue Analysis _ ____ Date J=1=Z6_ Job No. 27-771-100 _ calculation Wave Forces on Structure _

Wave Height = 22 FT Reviod = 9.4 Sec.

Total Tide = 3.2 FT

Still Water Level = 105 + 3.2 = 108.2 FT

Surface Current = 1.7 ft/sec. = 1.0 Knot

ELEVATION ABOVE PERCENTAGE PERCENTAGE CURRENT VELOCIT

MUDLINE OF DEPTH OF SURFACE

ELEVATION ABOVE	i	PERCENTAGE	CURRENTVELOCITY
MUDLINE (FT)	OF DEPTH	OF SURFACE CURRENT	(FT/SEC)
108.2	0	100	1.7 (1.0)
97.4	10	93	1.6 (0.9)
86.6	20	84	1.4 (0.8)
75.7	. 30	フフ	1.3 (0.8)
64.9	40	70	1.2 (0.7)
54.1	50	64	1.1 (0.6)
43.3	60	55	0.9 (0.5)
32.5	70	49	0.8 (0.5)
21.6	80	4_	0.7 (0.4)
10.8	90	32	0.5 (0.3)
0	100	14	0.2 (0.1)

Sheet 3:11 of 41__

By C. Chern Client U.S. NAUX _ subject Fatigue Analysis _ ____ Date 7=1=76 Job No. 27-771=100 _ calculation Wave Forces on Structure _

Wave Height = 27 FT Period = 9.8 Sec.

Total Tide = 3.7 FT

Still Water Level = 105 + 3.7 = 108.7 FT

Surface Current = 2.0 ft/sec = 1.2 knot

ELEVATION ABOVE MUDLINE (FT)	PERCENTAGE OF DEPTH	PERCENTAGE OF SURFACE CURRENT	CURRENT VELOCITY (FT/SEC)
108.7	0	100	2.0 (1.2)
97.8	10	93	1.9 (1.1)
87.0	20	84	1.7 (1.0)
76.1	. 30	フフ	1.5 (0.9)
65.2	40	70	1.4 (0.8)
54.4	50	64	1.3 (0.8)
43.5	60	55	1.1 (0.7)
32.6	70	48	1.0 (0.6)
21.7	80	4-1	0.8 (0.5)
10.9	90	32	0.6 (0.4)
0	100	14	0.3 (0.2)

Sheet 3:12 of 41 ___

By C. Chern client U.S. NAVY __ subject Fatigue Analysis _____ Date 7=1=76 Job No. 27-771-100 _ calculation Wave Forces an Structure _

Wave Height = 32 FT Period = 10.4 Sec.

Total Tide = 4.3 FT

Still Water Level = 105 + 4.3 = 109.3 FT

Surface Current = 2.3 ft/sec = 1.4 knot

ELEVATION ABOVE MUDLINE (FT)	PERCENTAGE OF DEPTH	PERCENTAGE OF SURFACE CURRENT	CURRENT VELOCITY (FT/SEC)
109.3	. 0	100	2.3 (1.4)
98.4	10	93	2.1 (1.2)
87.4	20	84	1.9 (1.1)
76.5	. 30	フフ	1.8 (1.0)
65.6	40	70	1.6 (0.9)
54.7	50	64	1.5 (0.9)
43.7	60	55	1.3 (0.8)
32.8	70	48	1.1 (0.7)
21.9	80	4	0.9 (0.5)
10.9	90	32	0.7 (0.4)
0	100	14	0.3 (0.2)





Sheet 3.13 of 41__

By C. Chern client U.S. NAUX ___ subject Fatigue Analysis ____.

Date J-1-76 Job No. 27-JJ1-100 _ calculation Wave Forces on Structure ___.

Wave Height = 37 FT Reviod = 10.9 Sec.

Total Tide = 4.9 FT

Still Water Level = 105 + 4.9 = 109.9 FT

Surface Current = 2.7 ft/sec. = 1.6 knot

ELEVATION ABOVE	ł		CURRENTVELOCITY
MUDLINE (FT)	OF DEPTH	OF SURFACE CURRENT	(FT/SEC)
109.9	0	100	2.7 (1.6)
98.9	10	93	2.5 (1.5)
87.9	20	84	2.3 (1.4)
76.9	30	77	2.1 (1.2)
65.9	40	70	1.9 (1.1)
54.9	50	64	1.7 (1.0)
44.0	60	55	1.5 (0.9)
33.0	70	48	1.3 (0.8)
22.0	80	41	1.1 (0.7)
11.0	90	32	0.9 (0.5)
0	10 C	14	0.4 (0.2)



By C. Chern Client U.S. NAUY __ subject Fatigue Analysis _____ Date 7-1-76 Job No. 27-77 L-100 _ calculation Wave Forces on Structure.

Wave Height = 42 FT Period = 11.4 Sec.

Total Tide = 5.4 FT

Still Water Level = 105 + 5.4 = 110.4 FT

Surface Current = 3.1 ft/sec. = 1.8 knot

ELEVATION ABOVE	PERCENTAGE	PERCENTAGE	CURRENT VELOCITY
MUDLINE (FT)	OF DEPTH	OF SURFACE CURRENT	(FT/SEC)
110.4	0	100	3.1 (1.8)
99.4	10	93	2.9 (1.7)
88.3	20	84	2.6 (1.5)
77.3	. 30	フフ	2.4 (1.4)
66.2	40	70	2.2 (1.3)
55.2	50	64	2.0 (1.2)
44.2	60	55	1.7 (1.0)
33.	70	48	1.5 (0.9)
22.1	80	41	1.3 (0.8)
11.0	90	32	1.0 (0.6)
0	100	14	0.4 (0,2)

Sheet 3:15 of 41__

By C. Chern Client U.S. NAUY __ subject Eatique Analysis _____ Date J=1-76_ Job No. 27-JJL-100_ calculation Wave Forces on Structure_

Wave Height = 47 FT Period = 12.0 Sec.

Total Tide = 6.0 FT

Still Water Level = 105 + 6 = 111.0 FT

Surface Current = 3.5 ft/sec. = 2.1 knot

ELEVATION ABOVE		_	CURRENTVELOCITY
MUDLINE (FT)	OF DEPTH	OF SURFACE CURRENT	(FT/SEC)
111.0	0	100	3.5 (2.1)
100.0	10	93	3.3 (2.0)
88.8	20	84	2.9 (1.7)
77.7	30	77	2.7 (1.6)
66.6	40	70	2.5 (1.5)
55.5	50	64	2.2 (1.3)
44.4	60	55	1.9 (1.1)
33.3	70	48	1.7 (1.0)
22.2	80	4	1.4 (0.8)
11.1	90	32	1.1 (0.7)
0	100	14	0.5 (0.3)

Sheet 3.1 100 41__

By C. Chern Client U.S. NAUY _ subject Fatigue Analysis _ ____ Date 7-1-76 Job No. 27-77/-100 _ calculation Wave Forces on Structure_

Wave Height = 52 FT Period = 12.6 Sec.

Total Tide = 6.6 FT

Still Water Level = 105 + 6.6 = 111.6 FT

Surface Current = 3.9 ft/sec = 2.3 knot

ELEVATION ABOVE MUDLINE	PERCENTAGE OF DEPTH	PERCENTAGE OF SURFACE	CURRENT VELOCITY
(FT)		CURRENT	(FT/SEC)
111.6	0	100	3.9 (2.3)
100.4	10	93	3.6 (2.1)
89.3	20	84	3.3 (2.0)
78.1	. 30	フフ	3.0 (1.8)
67.0	40	70	2.7 (1.6)
55,8	50	64	2.5 (1.5)
44.6	60	55	2.1 (1.2)
33.5	70	48	1.9 (1.1)
22.3	80	4-1	1.6 (0.9)
11.2	90	32	1.2 (0.7)
0	100	14	0.5 (0.3)





Sheet 3:17 of 41__

By C. Cheric Client U.S. NAVY _ subject Fatigue Analysis _ ____ Date 7-1-76 Job No. ZZ-771-100 _ calculation Wave Forces on Structure _

Wave Height = 57 FT Reviod = 13.2 Sec.

Total Tide = 7.2 FT

Still Water Level = 105 + 7.2 = 112.2 FT

Surface Current = 4.3 ft/sec. = 2.5 knot

ELEVATION ABOVE		1 — 1	CURRENTVELOCITY
MUDLINE (FT)	OF DEPTH	OF SURFACE CURRENT	(FT/SEC)
112.2	0	100	4.3 (2.5)
101.0	10	93	4.0 (2.4)
89.8	20	84	3.6 (2.1)
78.5	. 30	77	3.3 (2.0)
67.3	40	70	3.0 (1.8)
56.1	50	64	2.8 (1.7)
44.9	60	55	2.4 (1.4)
33.7	70	48	2.1 (1.2)
22.4	80	41	1.8 (1.1)
11.2	90	32	1.4 (0.8)
0	100	14	0.6 (0.4)





 $\mathcal{C}_{\mathcal{A}}^{(i)}$

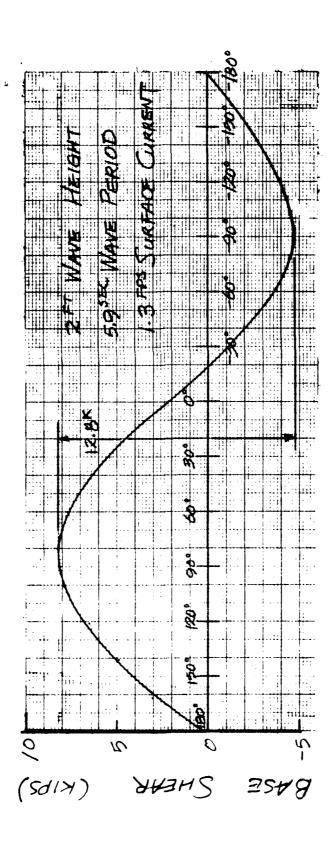
Sheet 3:18 of 41__

By C. Chern Client U.S. NAVY _ subject Fatigue Analysis _____ Date 8-6-76 Job No. 27-771-100 _ calculation Wave Fox es on Structure.

3.5 WAVE HEIGHT AND BASE SHEAR RELATIONSHIP

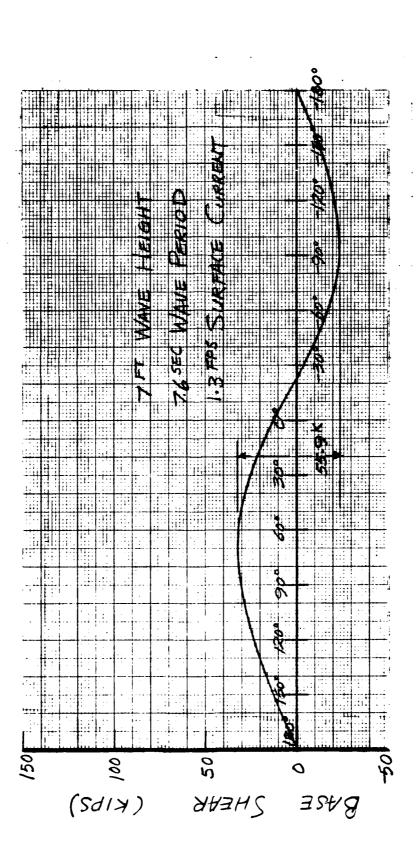
4,00

By C. Chern Client U.S. NAUY _ subject Fatigue Analysis _ ____ Date 7-20-76 Job No. 27-77L-100 _ Calculation Wave Forces on Structure _



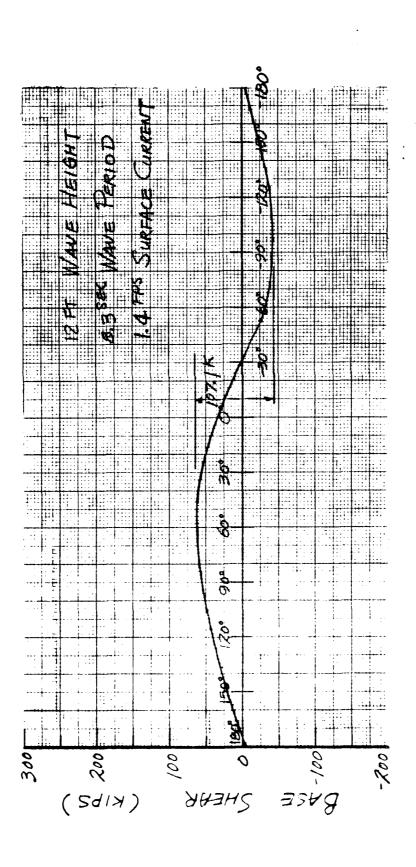
PHASE ANGLE WAVE-TO-STRUCTURE

By C. Shern client U.S. NAUX _ subject Fatigue Analysis _ ____ Date Z-20-Z6 Job No. 27-ZZ/-100 _ calculation Wave Forces on Structure.



WAVE - TO - STRUCTURE PHASE ANGLE

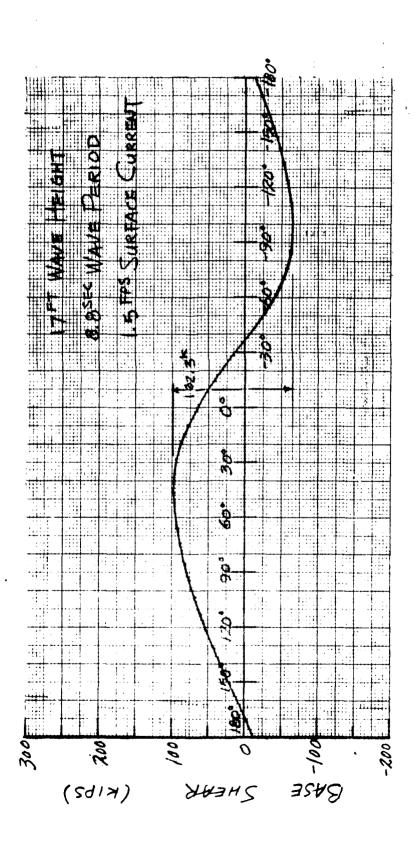
By C. Chern Client U.S. NAVY _ subject Fatigue Analysis _ Date 7-20-76 Job No. 27-271-100 _ calculation Wave Forces on Structure



彩

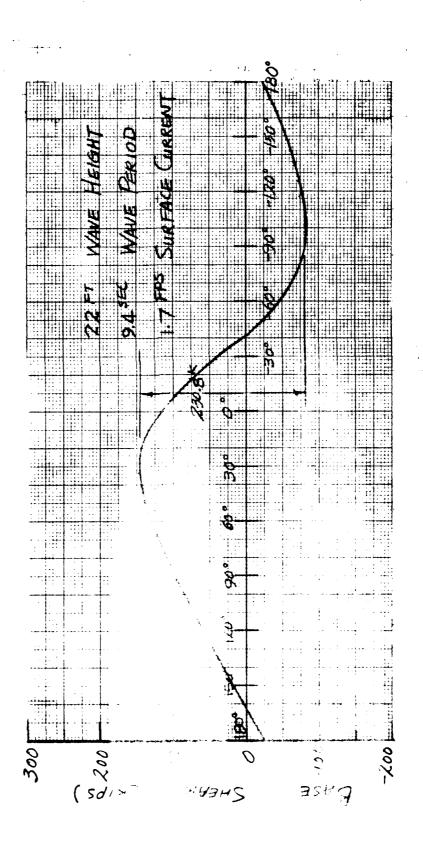
6.4.

By C. Chern client U.S. NAUX _ subject Fatigue Analysis _____ Date 7=20=76 Job No. 27-77/-100 _ calculation Wave Forces on Structure.



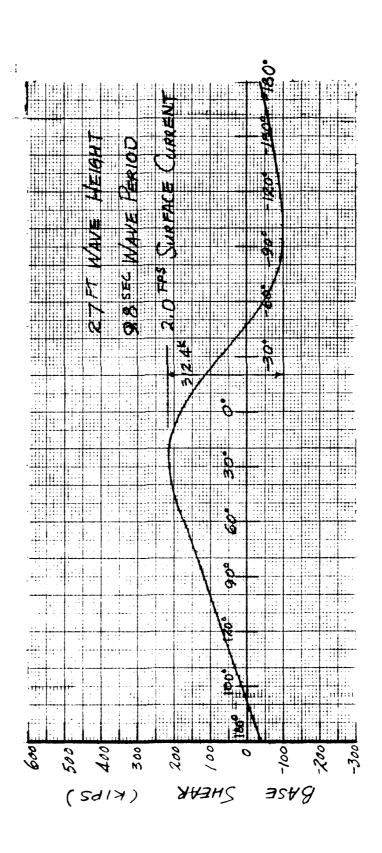
PHASE ANGLE WAVE-TO-STRUCTURE (C

By S. Chern_ client LI.S. NAVY __ subject Fatigue Analysis _____ Date 7-20-76 Job No. 27-771-100 _ calculation Wave Forces on Structure



PHASE ANGLE WAVE-TO-STRUCTURE (DE

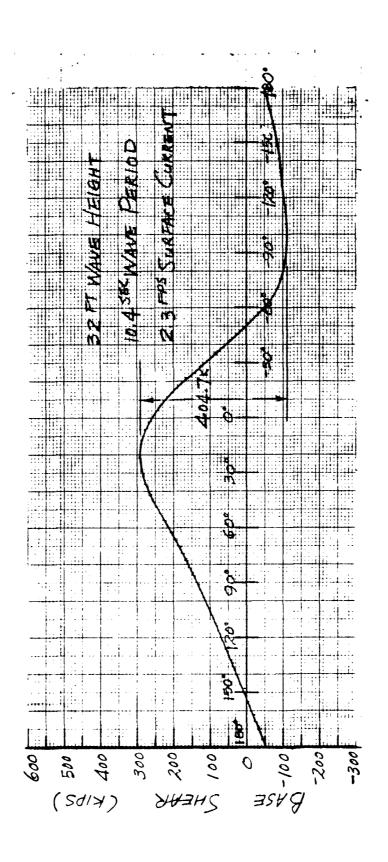
By C. Chern client U. S. NAUX _ subject Fatigue Analysis ____ Date 7-20-76 Job No. 27-771-100 _ calculation Ware Forces on Structure



ANGLE

d.

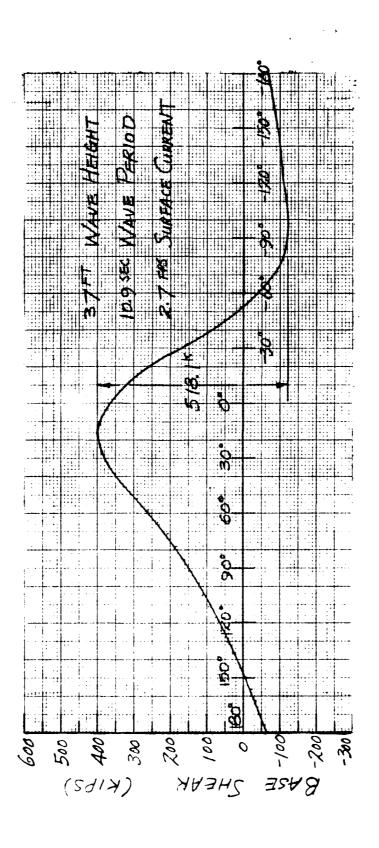
By C. Chern client U. S. NAVY __ subject _ Eatigue Analysis _____ Date 7-20-76 Job No. 27-771-100 _ calculation Wave Forces on Structure



PHASE ANGLE WAVE-TO-STRUCTURE (DEGR

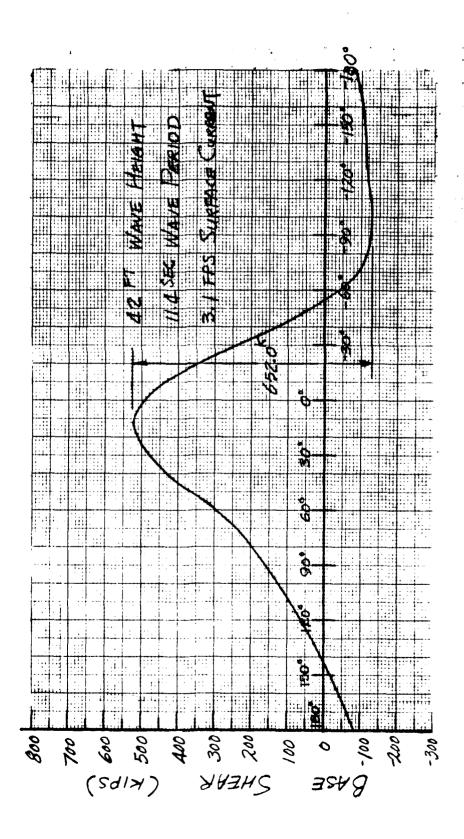
1

1



WAVE - TO- STRUCTURE PHASE ANGLE

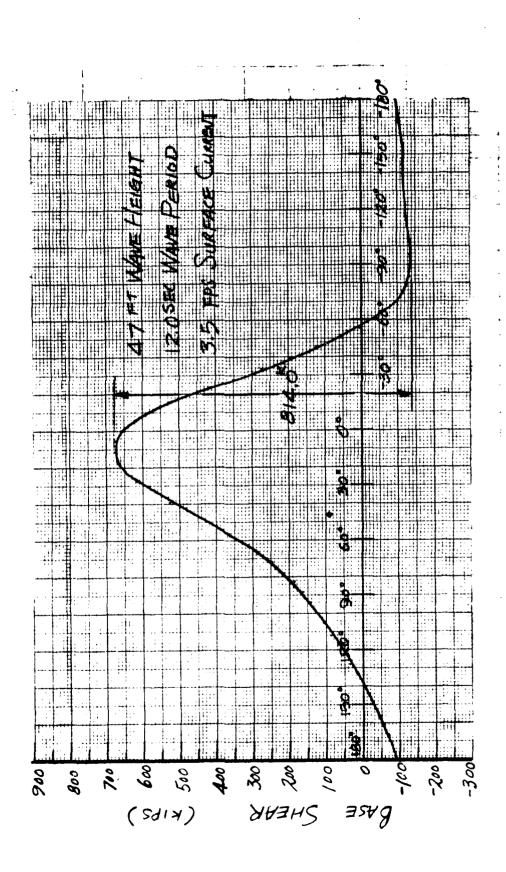
By C. Chern_ Client U.S. NAVY _ subject Fatigue Analysis _ Date 7-20-76 Job No. 27-771-100 _ calculation Wave Forces on Structure _



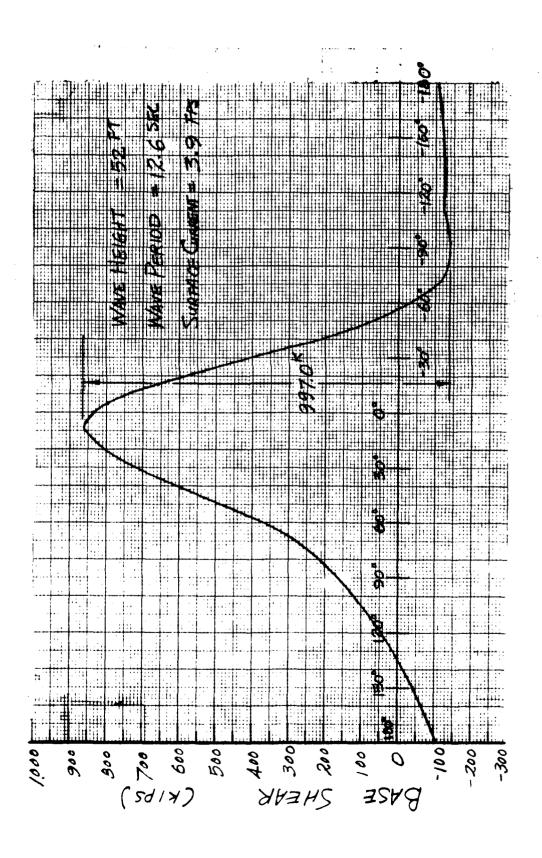
PHASE ANGLE WAVE - TO - STRUCTURE (DEGREES

4

By C. Chern Client U.S. NAVY _ subject Fatigue Analyzis _ ____
Date Z-20-76 Job No. 27-771-100 _ calculation Wave Forces on Structure.



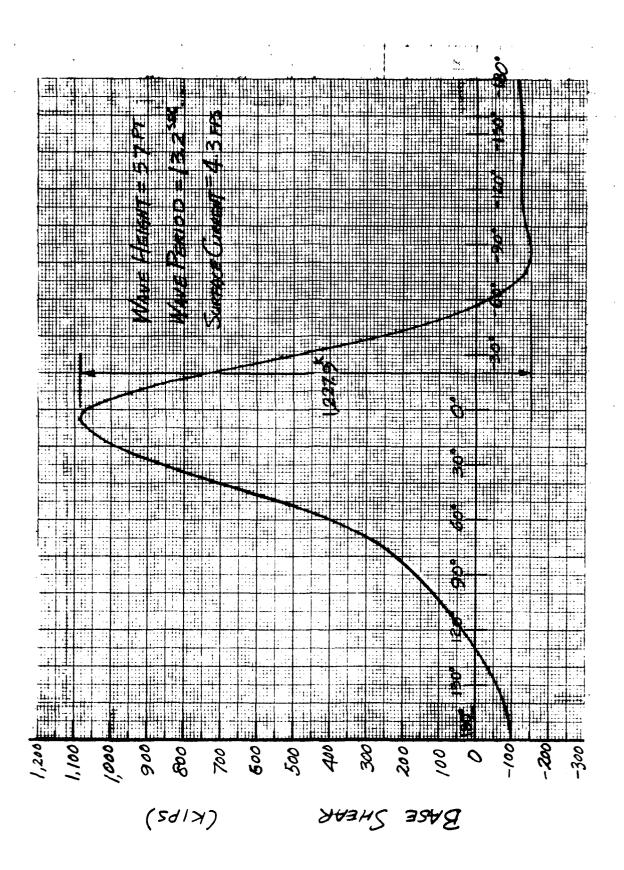
(DEGREES WAVE - TO- STRUCTURE By C. Chern client U. S. NAVY _ subject Fatigue Analysis _ ___ Date Z-20-ZE Job No. ZZ-ZZ/-100 _ Calculation Wave Forces on Structure _



(DEGREES MAVE - TO- STRUCTURE

XX.

By C. Chern Client U.S. NAVY __ subject Fatigue Analysis ____ Date 7=19-76 Job No. 27-77/-100 _ calculation Wave Forces on Structure.



WAVE - TO - STRUCTURE (DEGREES,

sheer 2:51 of 41__

By C. Chern_ client U. S. NAUX _ subject Fatigue Analysis _ ____ Date 7-20-76 Job No. 27-771-60 _ calculation Wave Forces on Structure

BASE SHEAR US. WAVE HEIGHT

WAVE	BASE SHEAR		
HEIGHT	POSITIVE	NEGATIVE	RANGE
FT	KIPS	KIPS	KIPS
2	8.2	4.6	12.8
7	32./	23.8	55.9
12	62.4	44.7	107.1
17	97.9	64.4	162.3
22	148.3	82.5	230.8
27	214.8	97.6	312.4
32	293.5	111.2	404.7
37	396.5	121.6	518.1
42	521.3	130.7	652.0
47	677.5	136.8	814.0
52	854.6	142.4	997.0
57	1,081.5	146.4	1,227.9
61.3*	1,428.7	319.5	

OFFSHORE, INC.

Sheet 3.32 of 41__

By C. Chern Client U.S. NAUY __ subject Fafigue Analysis _____ Date 8-6-76 Job No. ZZ-771-100 _ calculation Wave Farces on Structure _

3.6 TRANSFER FUNCTION

A. BASE SHEAR RANGE
Assuming that a second-order polynomial is selected as the approximating transfer function

$$V_R = a_2 H^2 + Q_1 H + Q_2$$
 (1)

where VR = base shear range, kips H = wave height, feet az, a,, a = constant coefficients

Error at data point i is then

$$\mathcal{E}_{i} = (a_{2}H_{i} + a_{1}H_{i} + a_{0} - V_{Ri})$$
 (2)

i=1,2, ..., m m = number of data The sum of the error squares is points

$$S = \sum_{i=1}^{m} \mathcal{E}_{i}^{2} = \sum_{i=1}^{m} (a_{2}H_{i}^{2} + a_{1}H_{i} + a_{0} - V_{Ri})^{2}$$
 (3)

For S to be a minimum it is necessary that

$$\frac{\partial S}{\partial a_1} = 0$$
; $\frac{\partial S}{\partial a_1} = 0$; $\frac{\partial S}{\partial a_2} = 0$

Sheet 3:32 of 41__

By C. Chern Chent LLS NAUX _ subject Fortigue Analysis _ ____ Date 8=10-76 Job No. 27-771-100 _ calculation Wave Forces on Structure.

or
$$\underset{i=1}{\overset{m}{\nearrow}} 2H_{i}^{2}(a_{2}H_{i}^{2}+a_{i}H_{i}+a_{0}-V_{Ri})=0$$

$$\underset{i=1}{\overset{m}{\nearrow}} 2H_{i}(a_{1}H_{i}^{2}+a_{1}H_{i}+a_{0}-V_{Ri})=0$$

$$\underset{i=1}{\overset{m}{\nearrow}} 2(a_{2}H_{i}^{2}+a_{1}H_{i}+a_{0}-V_{Ri})=0$$

$$\underset{i=1}{\overset{m}{\nearrow}} 2(a_{2}H_{i}^{2}+a_{1}H_{i}+a_{0}-V_{Ri})=0$$
(4)

The set of equations shown above may be expressed in matrix form as follows:

$$\begin{bmatrix}
M \\
W \\
i=1
\end{bmatrix}$$

$$M \\
i=1$$

Sheet 3-14 of 41__

By C. Chern Client U.S. NAUY __ subject Fatigue Analysis _____ Date 8 = 10 - 76 Job No. 27 - 771-100 _ calculation Wave Forces on Structures _

Н	H²	H ³	H⁴	Vk	HVR	H ² V _R
2	4	8	16	12.8	25.6	51.2
7	4-9	343	2,401	55.9	391.3	2,739.1
12	144	1,728	20,736	107.1	1,285.2	15,422.4
17	289	4,913	83,521	162.3	2,759.1	46,904.7
22	484	10,648	234,256	230.8	5,077.6	111,707.2
27	729	19,683	531,44	312.4	8,434.8	227,739.6
32	1,024	32,768	1,048,576	404.7	12,950.4	414,412.8
37	1,369	50,653	1,874,161	518.1	19,169.7	709,278.9
42	1,764	74,088	3,111,696	662.0	27, 384.0	1.150,128.0
47	2,209	103,823	4,879,681	814.0	38,258.0	1,798,126.0
52	2,704	140,608	7,311,616	997.0	51,844.0	2,695,888.0
57	3,249	185,193	10,556,001	1,227.9	69,990.3	3, 989,447.[
2 =354	14,018	624,456	29,654,102	5,495.0	237,570.0	11,161,845.0

Sheet 3:32 of 41__

By C. Chern Client U.S. NAVY __ subject Fatigue Analysis _____ Date 8=10=76 Job No. 27-77L-100 _ calculation Wave Forces on Structures _

$$\begin{bmatrix} 29,654,102 & 624,456 & 14,018 \\ 624,456 & 14,018 & 354 \\ 14,018 & 364 & 12 \end{bmatrix} \begin{bmatrix} a_1 \\ a_0 \end{bmatrix} = \begin{bmatrix} 11,161,845 \\ 237,570 \\ 5,495 \end{bmatrix}$$

$$\begin{bmatrix} 2,115.43 & 44.55 & 1.0 \\ 1,764. & 39.60 & 1.0 \\ 1,168.17 & 29.50 & 1.0 \\ \end{bmatrix} \begin{bmatrix} a_2 \\ a_1 \\ a_0 \end{bmatrix} = \begin{bmatrix} 796.25 \\ 671.10 \\ 457.92 \end{bmatrix}$$

$$\begin{bmatrix} 351.43 & 4.95 \\ 595.83 & 10.10 \end{bmatrix} \begin{bmatrix} a_2 \\ a_1 \end{bmatrix} = \begin{bmatrix} 125.15 \\ 213.18 \end{bmatrix}$$

$$\begin{bmatrix} 71.0 & 1.0 \\ 58.99 & 1.0 \end{bmatrix} \begin{bmatrix} a_1 \\ a_1 \end{bmatrix} = \begin{bmatrix} 25.28 \\ 21.11 \end{bmatrix}$$

$$12.01 \, \Omega_2 = 4.17$$

$$Q_1 = 0.3472$$
 ($= 0.35$)

$$Q_1 = 25.28 - 71 \times 0.35 = 0.43$$

$$V_R = 0.35 H^2 + 0.43 H + 36.38$$
 (6)

#

13

Sheet 3.36 of 41__

WAVE HEIGHT		BASE SHEAR	EKKOR	
Н	From Curve Fitting Vai	FROM DATA POINT	Vr Vr.	
FT	Kips	Kips	KIPS	
2	38.48	12.8	25.68	
7	56.54	55.9	0.64	
12	91.94	107.1	-15.16	
17	144.84	162.3	-17.46	
22	215.24	230.8	-15.56	
27	303.14	312.4	-9.26	
32	408.54	404.7	3.84	
37	531.44	518.1	13.34	
42	671.84	652.0	19.84	
47	829.74	814.0	15.74	
52	1,005.14	997.0	8.14	
57	1,198.04	1,227.9	-29,86	

Sheet 3.3 Z of 41__

By C. Chern client U.S. NAVY __ subject Fatigue Analysis ____ Date 8-10-76 Job No. 27-771-100_ calculation Wave Forces on Structures_

B. BASE SHEAR (POSITIVE - CREST APPROACHING STRUCTURE)

Assuming that the approximating transfer function is

$$V_{p} = b_{2}H^{2} + b_{1}H + b_{2} \tag{7}$$

According to Eq. (5) shown on Page 3.33, it gives

$$\begin{bmatrix}
M & H_{i}^{4} & M & M & M \\
M & M & M & M & M \\
M & M & M & M & M \\
M & M & M & M & M \\
M & M & M & M & M \\
M & M & M & M & M \\
M & M & M & M & M \\
M & M & M & M & M \\
M & M & M & M & M \\
M & M & M & M & M \\
M & M & M & M & M \\
M & M & M & M & M \\
M & M & M & M & M \\
M & M & M & M & M & M \\
M & M & M & M & M & M \\
M & M & M & M & M & M \\
M & M & M & M & M & M & M \\
M & M & M & M & M & M & M \\
M & M & M & M & M & M & M \\
M & M & M & M & M & M & M \\
M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M & M \\
M & M & M & M & M & M & M$$

i=1,2, ---, m

4.

Sheet 3:300 41__

By C. Chern client U.S. NAUY __ subject Fatigue Analysis _____ Date 8 = 10 - 76 Job No. 27 - 771-100 _ caiculation Wave Forces on Structures_

Н	H ²	H ³	H ⁴		HVp	H²Vp
2	4			8.2	16.4	32.8
7	49			32.1	224.7	1,572.9
12	144			62.4	748.8	8,985.6
17	289			97.9	1,664.3	28, 293.1
22	484			148.3	3,262.6	71,777.2
27	729			214.8	5,799.6	156,589.2
32	1,024			293.5	9, 392.0	300,544.0
37	1,369			396.5	14,670.5	542,808.5
42	1,764			521.3	21,894.6	919,573,2
47	2,209			6775	31,842.5	1,496,597.5
52	2,704			854.6	44,439.2	2,310,838.4
57	3,249			1,081.5	61,645.5	3,513,793.5
Z=35A	14,018	624,456	29,654,102	4,388.6	195,600.7	9,351,405.9

Sheet 3.29 of 41__

By C. Chern Client U. S. NAUY _ subject Fatique Analysis _ ____ Date 8 = 10-76 Job No. 27-771-100 _ calculation Wave Forces on Structures _

$$\begin{bmatrix}
29,654,102 & 624,456 & 14,018 \\
624,456 & 14,018 & 354 \\
14,018 & 354 & 12
\end{bmatrix}$$

$$\begin{bmatrix}
62,351,405.9 \\
195,600.7 \\
4,388.6
\end{bmatrix}$$

$$\begin{bmatrix}
2,115.43 & 44.55 & 1.0 \\
1,764. & 39.60 & 1.0 \\
1,168.17 & 29.50 & 1.0
\end{bmatrix}$$

$$\begin{bmatrix}
b_2 \\
b_1 \\
b_2 \\
b_1 \\
b_2 \\
b_1 \\
b_2 \\
b_2 \\
b_3 \\
b_4 \\
b_6 \\
b_7.72$$

$$\begin{bmatrix} 351.43 & 4.95 \\ 595.83 & 10.10 \end{bmatrix} \begin{bmatrix} b_2 \\ b_1 \end{bmatrix} = \begin{bmatrix} 114.56 \\ 186.82 \end{bmatrix}$$

$$\begin{bmatrix} 71.0 & 1.0 \\ 58.99 & 1.0 \end{bmatrix} \begin{bmatrix} b_2 \\ b_1 \end{bmatrix} = \begin{bmatrix} 23.14 \\ 18.50 \end{bmatrix}$$

$$12.01 b_2 = 4.64$$

$$b_2 = 0.3863 \quad (=0.39)$$

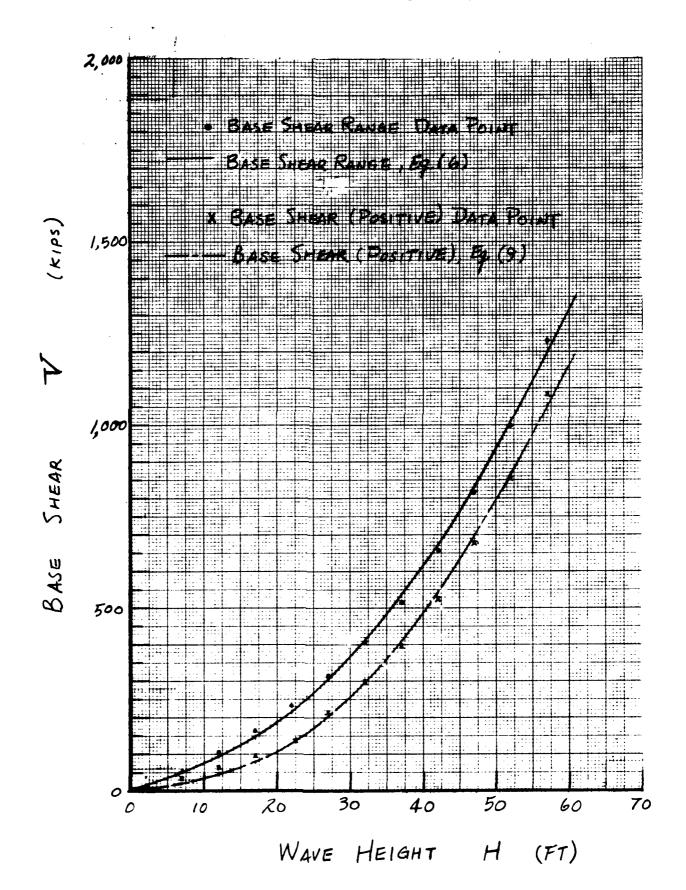
$$b_1 = 23.14 - 71 \times .39 = -4.55$$

Sheet 3.40 of 41__

By C. Chern Client U.S. NAUY __ subject Fatigue Analysis ____ Date & -10-76 Job No. 27-77L-100 _ calculation Wave Forces on Structures _

WAVE HEIGHT	BASE SHEAR	BASE SHEAR	ERROR
Н	FROM CURVE FITTING	FROM DATA POINT	
	Vpi	Vpo	Vp: -Vpo
FT	K1P5	KIPS	KIPS
2	36.82	8.7	28.62
7	31.62	32.	-0.48
12	45.92	62.4	-16.48
17	79.72	97.9	-18.18
22	133.02	148.3	-15.28
27	205.82	214.8	-8.98
32	298.12	293.5	4.62
37	409.92	396.5	13.42
42	541.22	521.3	19.92
47	692.02	677.5	14.52
52	862.32	854.6	7.72
57	1,052.12	1,081.5	-29.38

By C. Chern client U.S. NAVY __ subject Eatigue Analysis _____ Date 8=10-76 Job No. 27-77 L-100 _ calculation Wave Forces on Structures _



SECTION 4

FATIGUE LIMIT STRESS

4.1 INTRODUCTION

This section evaluates the fatigue limit stress ranges for punching shear stress and nominal brace stress. The method used to perform the calculation is in accordance with that in Reference 4.

In the course of data preparation for the computation of hurricane effects on the fatigue life, two assumptions are made as follows:

- (1) The significant wave height distribution can be expressed in terms of the Weibull distribution; and
- (2) The possible number of hurricane occurrence in 20 years period is 6.

The punching shear stress computation is shown in APPENDIX A.

Stress analyses of the idealized platform structure subjected to wave and ocean currents are compiled in APPENDIX B.

4

Sheet 4.0201 31

(1)

By C. Chern Client U.S. NAUY __ subject Fatigue Analysis _____ Date B = 4-76 Job No. 27-771-100 _ calculation Fatigue Limit Stress _ _

4.2 PUNCHING SHEAR STRESS RANGE US. CYCLES OF LOAD

From Eq.(1) of Ref.4

$$N = K/S^m$$

where N = Number of Stress cycles to failure

K = Constant

S = Stress range

m = constant

From Eq.(1) ln N = lnk - m ln S

at condition a: ln Na = ln K - m ln Sa)

ln Nb = ln K - m ln Sb at condition b:

$$: m = \frac{\ln (Na/Nb)}{\ln (Sb/Sa)}$$

K = N.Sm and

From AWS D 1.1-72 Fig. 10.7.4 (Ref. 1)

Line K-K for punching shear stresses

In the range of interest: Sa = 10500 Psi

Na= 103 cycles

Sb = 2500 Psi No=106 cycles

Sheet 4:03 of 31__

By C. Chern client U.S. NAUX _ subject Fatigue Analysis _ ____ Date 8-4-76 Job No. 27-771-100_ calculation Fatigue Limit Strees _ ___

$$M = \frac{\ln \left(\frac{10^3}{10^6}\right)}{\ln \left(\frac{2500}{10500}\right)} = 4.81$$

and
$$K = 10^6 \times (2500)^{4.81} = 2.21 \times 10^{22}$$

Sheet 4.04 of 31__

By C. Chern client U.S. NAVY __ subject Fatigue Analysis _____ Date 8-4-76 Job No. 27-771-100 _ calculation Fatigue Limit Stress ____

4.3 PUNCHING SHEAR STRESS RANGE US. WAVE HEIGHT

From Eq.(2) of Ref. 4

(2)

where S = Stress range

C = Constant

H = Wave height

9 = constant

From Eq. (2) ln S = ln C + g ln H

at condition a: ln Sa = en C + g ln Ha

at condition b: ln Sb = ln C + g ln Hb

 $\therefore q = \frac{\ln(Sa/Sb)}{\ln(Ha/Hb)}$

Sheet 4:0 Dot 31__

By C. Chern client U.S. NAUY _ subject Eatigne Analysis _ Date B = 4-76 Job No. 27-771-100 _ calculation Fatigue Limit Stress _ _

Joint #803 (BRACE #803-#906)

Mars Usians	JOINT F	PLUCHING SHEAT	R STRESS
WAVE HEIGHT	CREST	TROUGH	RANGE
FT	 <51	< S1	KSI
7	0.167	0.121	0.288
17	<i>o</i> .538	0.356	0.894
27	1.144	<i>o</i> .557	1.701
42	2.687	0.731	3.418
61.3 *	7.454	0.150	7.604

* Design wave height, See Report No. 27-771-96

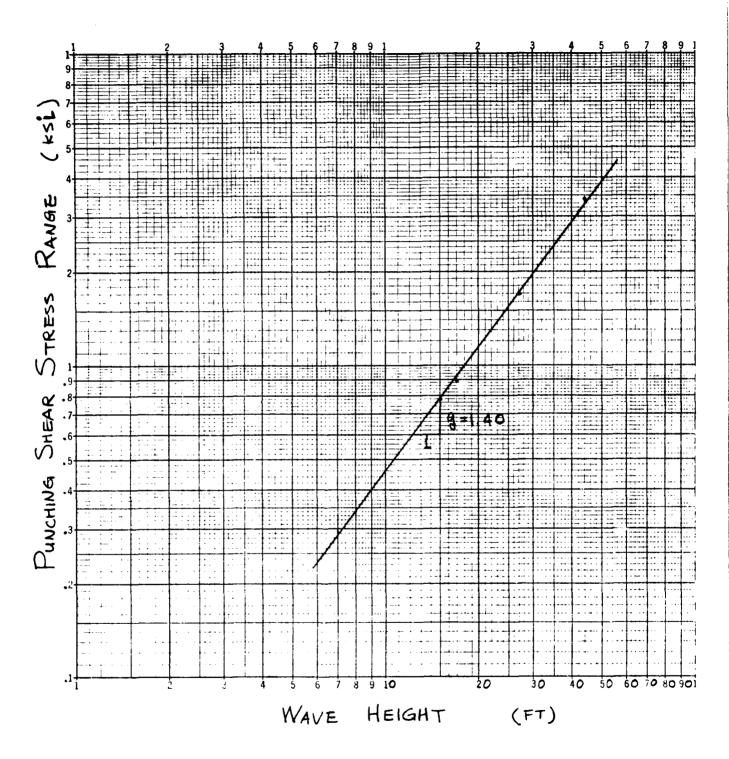
Design condition Vmax = 7.454 KSi

Vmin = 0.150 ksi

Sheet 4.06, 31__

CONDITION	n a	CONDIT	CONDITION b		
WAVE HEIGHT	STRESS RANGE	WAVE HEIGHT	Stress Range (Sb)	3	
FT	K51	FT	K51		
		17	0.894	1.28	
7	7 0.288	27	1.70]	1.31	
		42	3.418	1.38	
1 -7	17 0.894	27	1.701	1.39	
' /		42	3.418	1.48	
27	1.701	42	3.418	1.58	
			AVERAGE	1.40	

By C. Chern client U.S. NAV _ subject Eatigne Analysis ______ Date 8-4-76 Job No. 27-771-100 _ calculation Fatigue Limit Stress gas



JOINT NO. 803 (*803-906)
PUNCHING SHEAR STRESS RANGE US. WAVE HEIGHT

Sheet 4.08 of 31__

By C. Chern Client U.S. NAVY __ Subject Extigne Analysis _____ Date 8 = 4 = Z6 Job No. 27 = Z71 = LDQ _ calculation Fatigue Limit Stress ___

JOINT # 706 (BRACE # 706 - #803)

14/2-2-1-0	JOINT PUNCHING SHEAR STRESS				
WAVE HEIGHT	CREST	TROUGH	RANGE		
ਸ	KS1	KSI	KSI		
7	. 175	.101	.276		
17	.538	.200	.738		
27	1.142	.276	1.412		
42	2.602	.348	2,950		
61.3*	7.606	.350	7.956		

* Design wave height, See Report No. 27-771-96

Design condition: Vmax = 7.606 ksi

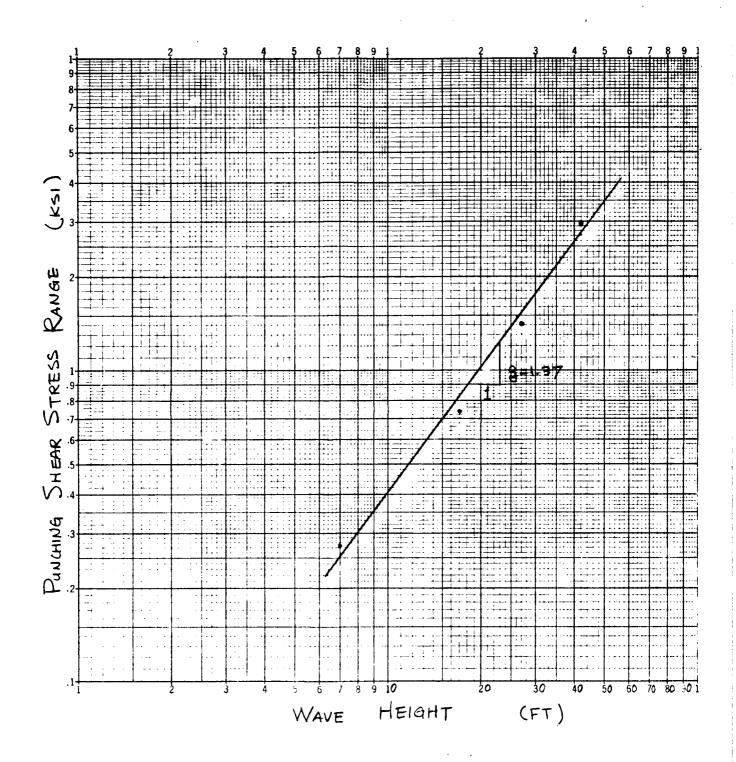
Vmin = 0.350 Ksi

Sheet 4.02 of 3

By C. Charn Client U.S. NAUX _ subject Eatique Analysis_ Date 8-4-76 Job No. 27-771-100 _ calculation Fatique Limit Stress_

CONDITION	a			
WAVE HEIGHT	STRESS RANGE	WAVE HEIGHT (Hb)	STRESS RANGE (Sb)	Þ
FT	KSI	FT	KSI	
		17	.738	1.11
7	.276	27	1,412	1.21
		42	2.950	1.32
17	720	27	1.412	1.40
, ,	-738	42	2.950	1.53
27	1.412	42	2.950	1.66
			AVERAGE	1.37

By C. Chern Client U.S. NAUY __ subject Fatigue Analysis _____ Date 8-4-76 _ Job No. 27-771-100 _ calculation Fatigue Limit Stress ____



JOINT NO. 70.6 (*706-#803)
PUNCHING SHEAR STRESS RANGE US WAVE HEIGHT

Sheet 4:11 of 31_

(12)

By C. Chern client U.S. NAVY __ subject Fatigue Analyzis _____ Date 8-4-76 Job No. 27-771-100 _ calculation Fatigue Limit Stress ____

4.4 LIMIT PUNCHING SHEAR STRESS FOR FATIGUE

· WARRING

From Eqs (10) and (12) in Ref. 4:

where Sr = Stress range for design wave

$$C = Constant defind by Eq.(10)$$

$$C = \frac{\{ln(rM_1)\}^{8m/3}}{M_1\Gamma(1+9m/4)}$$
(10)

r = return period for design wave

K = Constant in fatigue curve K-K

N= number of waves in one year

= Weibull parameter

Y = fatigue life in years

M = Constant.

OFFSHORE, INC.

Sheet 4.12 of 31

By C. Chevil client LI.S. NAUY __ subject Folique Analysis ____ Date 8-4-76 Job No. 27-771-100 _ calculation Fatigue Limit Stress ____

$$m = 4.81$$

3 = 1 P(H) is an exponential distribution

$$M_1 = 98,840,000/20$$

= 4,942,000

$$gm/g = 1.40 \times 4.81/1.0 = 6.73$$

$$\Gamma(1+\frac{9m}{3}) = \Gamma(1+6.73)$$

= 6.73 x 5.73 x 4.73 x 3.73 x 2.73

X 1.73 X [(1.73)

$$\Gamma(1.73) = 0.91466$$

$$\Gamma(7.73) = 2939$$

$$c = \frac{\left\{\ln(50 \times 4,942,000)\right\}}{4,942,000 \times 2939} = 0.0311$$

$$CK = 0.0311 \times 2.21 \times 10^{22} = 6.873 \times 10^{20}$$

$$S_{t} = \left(\frac{6.873 \times 10^{20}}{20}\right)^{\frac{1}{4.81}} = \left(\frac{6.873 \times 10^{10}}{2.0} \times 10^{10}\right)^{\frac{1}{4.81}}$$

Sheet 4:13 of 31_

(1)

By C. Chern Client U.S. NAVY __ subject Eatique Analysis ____.

Date 8-4-76 Job No. 27-77L-100 _ calculation Fatigue Limit Stress ____.

4.5 NOMINAL BRACE STRESS RANGE US. CYCLES OF LOAD

From Eq.(1) of Ref.4

it gives

$$m = \frac{\ln (Na Nb)}{\ln (Sb Sa)}$$

From Line D'-D', Fig. 10.7.4 AWS D1.1-72

In the range of interest:

$$S_a = 22,000 \text{ Psi}$$
 $S_b = 6900 \text{ Psi}$ $N_a = 4.0 \times 10^3 \text{ cycles}$ $N_b = 1.0 \times 10^6 \text{ cycles}$

$$m = \frac{\ln (4.0 \times 10^{3})}{\ln (6900)} = 4.80$$

$$K = 10^6 \times (6900)^{4.80} = 2.67 \times 10^{24}$$

Sheet 4:14 of 31__

By C. Chern client U.S. NAUX __ subject Eatique Analysis ____.

Date 8 = 4 - 76 Job No. 27 - 771 - 100 _ calculation Fatigue Limit Strees ____.

4.6 NOMINAL BRACE STRESS RANGE US. WAVE HEIGHT

$$S = CH^{9}$$
 (2)

it gives

$$g = \frac{\ln (Sa S_b)}{\ln (Ha H_b)}$$

Sheet 4:15of 31__

By C. Chern client U.S. NAVY __ subject Fatigue Analysis _____ Date 8=4-76 Job No. 27=771-100 _ calculation Fatigue Limit Stross _____

JOINT #803 (BRACE #803-#906)

WAVE	NOMINAL BRACE STRESS					
HEIGHT	CRE	CREST TROUGH		RANGE		
	AXIAL	BENDING	AxIAL	BENDING	KANCE	
FT	KSI	KSI	KSI	KSI	KSI	
7	240	Ŧ·056	+.176	±.039	0.511	
17	665	- .285	+.395	± .233	1.578	
27	-1.436	- .582	+.552	± .428	2.998	
42	- 3.374	71.369	+.687	±.599	6.029	
61.3*	-8.463	Ŧ4.677	127	+.132	13.399	

* Design wave height, See Report No. 27-771-96

Design condition:
$$f_{max} = -13.140$$

 $f_{min} = +0.005$

6

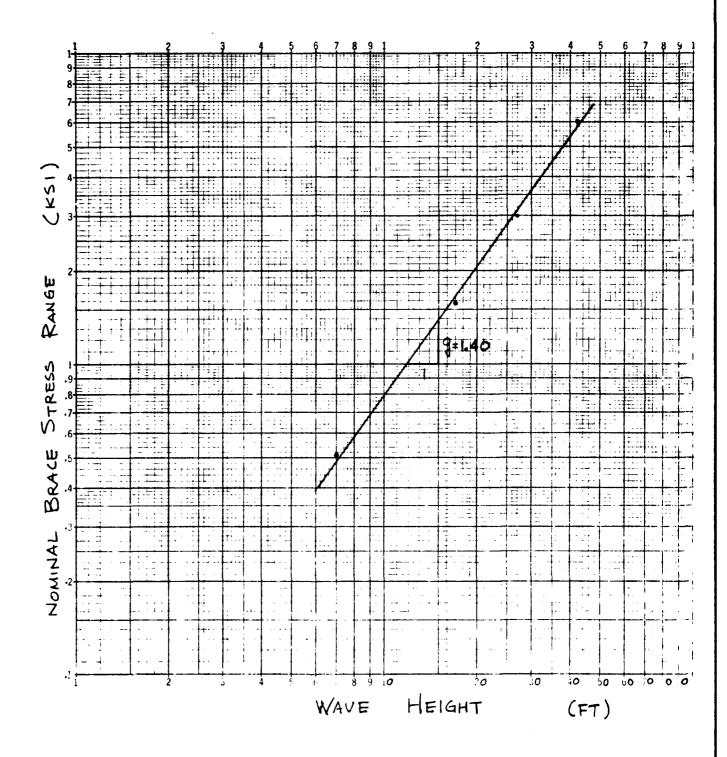
Sheet 4:160+ 31__

By C. Chern client U.S. NAUY __ subject Fatigue Analysis ____ Date 8-4-76 Job No. 27-77/-100 _ calculation Fatigue Limit Stress ____

CONDITIO	on a	CONDITIO	d No	Q
WAVE HEIGHT	STRESS RANGE (Sa)	WAVE HEIGHT	STRESS RANGE (Sb)	7
FT	KSI	FT	KSI	
		17	1.578	1.27
7	0.511	27	2.998	1.31
		42	6.029	1.38
١7	1.578	27	2.998	1.38
, ,	1.576	42	6.029	1.48
27	2.998	42	6.029	1.58
			Average	1.40

(T)

By C. Chris client U.S. NAVY _ subject Fatigue Analysis _____ Date 8-5-76 Job No. 27-771-100 _ calculation Fatigue Limit Stress ____



JOINT #803 (#803-#906)

NOMINAL BRACE STRESS RANGE US. WAVE HEIGHT

Sheet 4-19 of 31__

By C. Cherr Client U.S. NAUY __ subject Eatique Analysis _____ Date 8-5-26 Job No. 27-771-100 _ calculation Fatique Limit Stress ____

JOINT #706 (BRACE #706-#803)

WAVE	NOMINAL BRACE STRESS				
HEIGHT	CRE	LEST TROUGH		ough	D
	AXIAL	BENDING	AXIAL	BENDING	RANGE
FT	KSI	KSI	KSI	K51	KSI
7	+.189	± . /23	137	7.044	0.493
17	+ . 545	± · 414	281	F.077	1.317
27	+ 1.302	± .739	377	Ŧ·108	2.526
42	+3.144	±1.510	447	Ŧ.176	5,277
61.3*	+8.440	±5.146	+.184	F.416	14.186

* Design wave height, See Report No. 27-771-96

Design condition: fmax =+13.586

fmin = -0.232

TOTAL MANAGEMENT OF STREET STREET

(17)

Sheet 4-12 of 31__

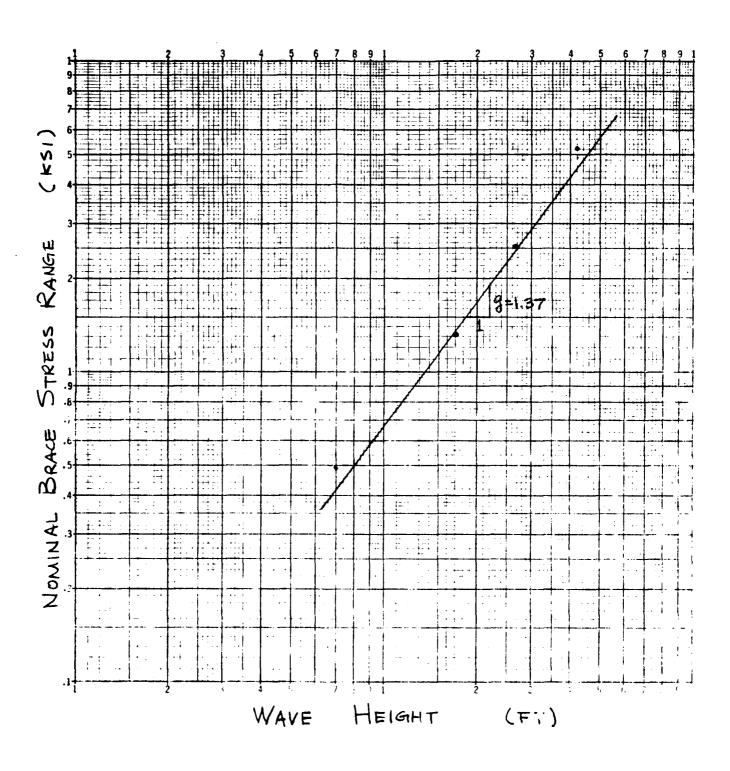
By C. Chern Client LLS. NAVY __ subject Foliging Analysis ______ Date 8-5-76 Job No. ZZ-771-100 _ calculation Faligne Limit Stress _____

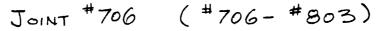
CONDITI	on a	CONDIT	rion b	0
WAVE HEIGHT (Ha)	STRESS RANGE	WAVE HEIGHT (Hb)	STRESS RANGE	7
FT	1<51	PT	KSI	
		17	1.317	1.10
7	0.493	27	2.526	1.21
		42	5.277	1.32
17	1.317	27	2,526	1.41
. ,		42	5.277	1.53
27	2.526	42	5.277	1.67
	1.37			

Sheet 4.20 of 3

By C. Chern Client U.S. NAVY ___ subject Fatigue Analysis _____ Date 8-5-76_ Job No. 27-77/-120 _ calculation Fatigue Limit Stress ___







NOMINAL BRACE STRESS RANGE VS. WAVE HEIGHT



Sheet 4-21 of 31__

By C. Chern client U.S. NAUX _ subject Fatigue Analysis _ ____
Date 8-5-76 Job No. 27-771-100 _ Calculation Fatigue Limid Stress _ ___

4.7 LIMIT NOMINAL BRACE STRESS FOR FATIGUE

$$c = \frac{\{ln(rM_1)\}^{\frac{9m}{3}}}{M_1\Gamma(1+\frac{9m}{3})}$$

t=50 yrs return period for design wave

Y = 20 yrs fatigue Life

3 = 1.0 for exponential distribution of p(H) curve

M = 4,940,000 number of waves in one year

g = 1.40

m = 4.80

()

 $K = 2.67 \times 10^{24}$

 $gm/g = 1.40 \times 4.80/1.0 = 6.72$

 $\Gamma(1+6.72) = 6.72 \times 5.72 \times 4.72 \times 3.72 \times 2.72 \times 1.72 \times 0.9125$

= 2,881

$$C = \frac{\left\{ \ln (50 \times 4,940,000) \right\}^{6.72}}{4,940,000 \times 2,881} = 0.0309$$

Sheet 4.2201 31__

By C. Chern client U.S. NAUX __ subject fatigue Analysis ____ Date B=5-Z6 Job No. 27-771-100 _ calculation Eatique Limit Stress ____

$$c/c = 0.0309 \times 2.67 \times 10^{24} = 8.250 \times 10^{22}$$

$$S_r = \left(\frac{8.250 \times 10^{22}}{20}\right)^{1/4.80}$$

$$= \left(\frac{8.250 \times 10^{12}}{20} \cdot 10^{10}\right)^{1/4.80}$$

$$= 262.95 \times 121.15$$

Sheet 4:23 of 31__

By C. Charr client U.S. NAVY __ subject Fatigue Analysis _____ Date 8-16-76 Job No. 27-771-100 _ calculation Fatigue Limit Stress ____

4.8 HURRICANE EFFECTS ON FATIGUE LIMIT STRESS

Fatigue Damage = Damage due to Normal Waves (Part I)
+ Damage due to Hurricanes (Part I)

(I) Damage due to Normal Waves

According to Ref. 4, long term damage in terms of significant wave height is given by Eq. 16 which follows

$$DN_{r} = M \Gamma(1+qm/2) \Gamma(1+9m/2) \left\{ \frac{h}{\sqrt{2}H_{r}} \right\}^{\frac{1}{4m}}$$
 (16)

if the significant wave height distribution can be expressed in terms of the Weibull distribution:

$$P(H_s) = 1 - e^{-(\frac{H_s}{L})^n}$$
 (6)

where D = fatique damage

Nr = the number of cycles to failure for the Stress range resulting from design wave height

M = the total number of waves

Hs = significant wave height

Hr = design wave height

 $h, \alpha = \text{constants in Eq.}(6)$

Sheet 4 4 6 3 ___

By C. Chara client U.S. NAUX _ subject Fatigue Analysis _ ___ Date 8-16-76 Job No. ZZ-JZI-100 calculation Fatigue Limit Stress _ ___

Constants & and h

$$P(H_s) = 1 - e^{-\left(\frac{H_s}{h}\right)^{\alpha}}$$
 (6)

$$e^{-\left(\frac{Hs}{h}\right)^{\kappa}} = 1 - P(Hs)$$

$$ln\left[e^{-(H_{5h})^{\alpha}}\right] = ln\left[1-P(H_{5})\right]$$

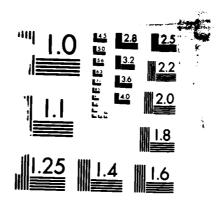
$$\left(\frac{Hs}{h}\right)^{\alpha} = -\ln\left[1-P(Hs)\right]$$

$$\alpha[l_n H_s - l_n h] = l_n[-l_n[1-P(H_s)]$$

$$\propto ln\left(\frac{H_{sa}}{H_{sb}}\right) = ln \frac{ln\left[1-P(H_{sa})\right]}{ln\left[1-P(H_{sb})\right]}$$

$$\alpha = \frac{en \left\{ en \left[1 - P(H_{Sa}) \right] en \left[1 - P(H_{Sb}) \right] \right\}}{en \left(H_{Sa} \right)} \dots (a)$$

FATIGUE ANALYSIS EAST COAST AIR COMBAT MANEUVERING RANGE OFFSHORE KITTY H. (U) CREST ENGINEERING INC TULSA OK SEP 76 27-771-100 CHES/NAVFAC-FPO-7616 N62477-76-C-0179 F/G 13/13 AD-A165 651 2/6 UNCLASSIFIED NL



MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS 1963 A

Sheet 4:25 of 31__

By C. Chevr client U.S. NAUY __ subject Fatigue Analysis _____ Date 8-16-76 Job No. 27-771-100 _ calculation Eatigue Limit Stress ____

Refer to A.H. Glenn and Associates' Report:

Page 2, Hs = Hmax /1.86

\$ Table 39

• •	l l	SIGNIFICANT	NUMBER OF	PROBABILITY	
CATAGORY	Wave Height	WAVE HEIGHT	WAVES IN 20 Yrs	1 _	PROBABILITY DENS. DISTRI.
		Hs	110 20 712	P(Hs)	P(Hs)
FT	FT	FT			
0~4	2	2.15	76,040,000	0.76932416	0.76932416
5~ 9	7	4.84	18,380,000	0.18595710	0.95528126
10 ~ 14	12	7.53	3,563,000	0.03604816	0,99132942
15~19	17	10.22	689,000	0.00697086	0.99830028
20~24	22	12.90	135,400	0.00136989	0,99967017
25~29	27	15.59	26,250	0.00026558	0.99993575
30 ~ 34	32	17.20	5,100	0.0000 5160	0.99998735
35~39	37	20.97	999	0.0000 1011	0.9999746
40~44	42	23.66	200	0.00000202	0.9999948
45~49	47	26.34	41	0.00000042	0.99999990
50 ~54	52	29.03	8	0.00000008	0.99999998
55~59	57	31.72	2	0.0000002	1.00000000
			M=98,840,000	1.00000000	





(Ti)

€.

Sheet 4:25 of 31__

CONDITION	. a	CONDITI	оп Б		1
SIGNIFICANT WAVE HT. (HEA)	CUMULATIVE PROB. P(Hea)	SIGNIFICANT WAVE HT. (HSb)	CUMULATIVE PROB. P(HS)	X	h
FT		FT			FT
		10.22	0,998 30028	0.962	1.489
4.84	4.84 0.95528126	15.59	0.99993575	0.969	1.502
		23.66	0.99999948	0.969	1.502
10.22	10.00	15.59	0.99993575	0.982	1.549
0.99830028	23.66	0.99999948	0.976	1.53	
15.59	0.99993575	23.66	0.9999948	0.970	1.506
		0.971	1.513		

Notes:
$$\alpha = E_{q}.(a)$$

$$h = E_{q}.(b)$$

NO.

774

By C. Chern client U.S. NAUX __ subject Fatigue Aralysis ____ Date B-16-76 Job No. Z7-771-L00 calculation Eatique Limit Stress

The available data for Eq. (16) are as follows:

$$g = 1.40$$
 (Pages 4.06 ± 4.16)

$$m = 4.80$$
 (Pages 4.03 \ \frac{1}{4} \cdot 13)

$$\alpha = 0.971$$

$$h = 1.513$$
 FT $g_{m} = 1.40 \times 4.80 = 6.72$

$$H_r = 61.3$$
 FT $gm/c = 6.92$

$$\Gamma(1+9m/2) = \Gamma(1+3.36) = 3.36 \times 2.36 \times 1.36 \times \Gamma(1.36)$$

= 9.60

$$T(1.36) = .890$$

$$\Gamma(1+9m/2) = \Gamma(1+6.92)$$
= 6.92 × 5.92 × 4.92 × 3.92 × 2.92
× 1.92 × $\Gamma(1.92)$

$$DN_{r} = 98,840,000 \times 9.60 \times 4288 \times \left\{ \frac{1.513}{42 \times 61.3} \right\}^{6.72}$$

for the fatigue damage resulting in 20 years from nonhurricane waves.

Sheet 4:29 of 3/_.

By C. Chern client U.S. NAUX __ subject Fatigue Analysis ____ Date 8-16-76 Job No. 27-771-100 calculation Fatigue Limit Stress ____

Assuming that the expected number of hurricana in 20 years is 6*(n=6) and that the value of 20 percent probability of exceeding the design stress range is selected, then Fig. 4 of Reference 4 gives

 $\frac{DN_r}{\eta} = 4$ $DN_r = 4 \eta = 24 \dots (21)$

(III) TOTAL FATIGUE DAMAGE

 $DN_{r} = 6.23 + 24 = 30 \dots (22)$

for the fatigue damage with a 20 percent chance of being exceeded in 20 years for the design structure.

^{* 7=6} is the largest number of hurricanes available from Fig. 4 of Ref. 4

Sheet 4:30 of 3/_

By C. Cherr client U.S. NAVY __ subject Fatigue Analysis ______ Date &=16-76 Job No. 27-771-100 _ calculation Fatigue Limit Stress _

According to Eq. 24 of Reference 4, the damage is

(24)

(i) For Punching Shear Stress

$$K = 2.21 \times 10^{22}$$

$$m = 4.8$$

$$D = 30 \times (7,956)^{4.8} (2.21 \times 10^{22})$$

= 0.0072

(ii) For Nominal Brace Stress

$$K = 2.67 \times 10^{24}$$

$$m = 4.8$$

$$D = 30 \times (13,586)^{4.8} (2.67 \times 10^{24})$$

$$= 0.00078$$

Sheet 4:3/of 3/_

By C. Chern client U.S. NAUX _ subject Fatigue Analysis _____

Date & = 16 - 26 Job No. 27 - 77/- 100 _ calculation Entique Limit Stress _ ___

According to Eq. (25) of Reference 4, the fatigue limit stress is defined if Disspecified by the designer.

$$S_r = \left(D \, K / 30 \right) / m \tag{25}$$

If D=.5 is selected in 20 years with a 20 percent chance of being exceeded, the limit stress for

is Punching Shear Stress

$$K = 2.21 \times 10^{22}$$

$$m = 4.8$$

$$S_r = (.5 \times 2.2 / \times 10^{22})^{4.8}$$

(ii) Nominal Brace Stress

$$K = 2.67 \times 10^{24}$$
;

$$M = 4.8$$

$$S_r = (.5 \times 2.67 \times 10^{24})^{48}$$

By J. Talbot client U.S. Navy __ subject _ Eatique Analysis _____
Date 10-6-76 Job No. 21-771-120 Calculation Fatigue Limit Stress ____

4.9 Fatigue Strength of a T-Joint

(A) Fatique Limit Stress Under Persistant Severe Storm

Ref. p. 4.12

$$m = 4.81$$

£ = 1.0

9 = 1.40

M= 4,942,000

y = 20 yrs r = 50 yrs

gm = 6.73

Curve T-T of AWS D 1.1-72 (p.6.02)

Sa = 5,250 psi Sb = 1,250 psi $Na = 10^3 eycles$ $Nb = 10^6 eycles$

 $m = \frac{\ln (10^3/10^6)}{\ln (1250/5250)} = 4.81$

 $K = 10^6 \times (1250)^{4.81} = 7.873 \times 10^{20}$

 $\Gamma(1+\frac{9\pi}{5}) = \Gamma(1+6.73)$

= 6.73 \times 5.73 \times 4.73 \times 3.73 \times 2.73 \times 1.73 \times $\Gamma(1.73)$

= 2939

 $C = \frac{\left\{ \ln \left(50 \times 4,942,000 \right) \right\}^{6.73}}{4,942,000 \times 2939} = 0.0311$

CK = 0.0311 x 7.873 x 1020 = 0.2449 x 1020

17

4.33

By V. Talbot Client U.S. Navy __ subject _ Fatigue Analysis _____

Date 10-6-76 Job No. 27-771-100 Calculation _ Fatigue Limit Stress ___.

$$S_r = \frac{\left(0.2449 \times 10^{20}\right)^{1/4.81}}{20}$$

(B) Hurricane Ettects on Fatigue Limit Stress

$$m = 4.81$$

$$Sr = \left(\frac{0.5 \times 7.873 \times 10^{20}}{30}\right)^{1/4.81}$$

(C) Fatigue Life

Sheet ___ of _ _ _ _

By J_Talbot Client U.S. Navy _ subject Fatigue Analysis _ _ _ _ Date 10-6-76 Job No. 27-771-100 calculation Fatigue Limit Stress _ _ _

(D) Maximum T- Joint Punching Shear Stress Range
- 20 year Fatigue Life

Y = 20 yrsC = 0.0311

C - 010 311

 $Nr = \frac{20}{0.0311} = 6.43 \times 10^2$ eyeles

AWS D1.1-72 Fig. 10.7.4, Line T-T, (p.6.02)

Sr = 6.1 ksu

Note: Sr = 6.0 ksc is in good agreement with the result of closed-form analysis Sr = 5.76 ksi)

1

4.35 Sheet _ _ of _ _ _

By J. Talbat Client U.S. Navy _ subject Fatigue Analysis _ ____
Date 10-6-76 Job No. 27-771-100 _ calculation Fatigue Limit Stress _ ___

(E) Check T- Joints for Fatigue Life

Jacket for 105' MLW Structure

T-Voint	Maximum Punching Shear (ksc)	Maximum Punching Shear Range	Stress for Fatigue Life of Zoyrs	Stress for Fatigue Life of 28 yrs
1001	5.169	5. 287	6.10	5.38
1003	5.614	5.381	6.10	5,38
1006	4. 545	4.691	6.10	5.38

Maximum Punching Shear from Appendix A.2

Load Conditions 10-13

Minimum Punching Shear from Appendix A.Z Load Conditions 14-17

Use 1.04 for 93' MLW Structure and 81' MLW Structure

4.36 Sheet ____ of ____

By J. To 1bot Client 45 Navy Subject Fatigue Analysis

Date 10-6-76 Job No. 27-771-100 Calculation Fatigue Limit Stress

Jacket for 93' MLW Structure

	T- Joint	Maximum Punching Shear (ksi)	Maximum Punching Shear Range (ksi)	Stress for Fatigue Life of 20yrs	Stress for Fatigue Life of 28 yrs
_	1001	5.245	5.45	6.10	5.38
	1003	5.902	6.13	6.10	5.38
	1006	4.247	4.41	6.10	5.38

Maximum Punching Shear from Appendix A.3

$$M.5. = 6.13 - 1.00 = +.005$$
 :. OK

Sheet _____ of ____

By J. Talbot Client U.S. Navy __ Subject Fatigue Analysis _____
Date 10-6-76 Job No. 27-771-100 Calculation Fatigue Limit Stress ____

Jacket for 81' MLW Structure

T-Voint	Maximum Punching Shear (ksi)	Maximum Punching Shear Range (Ksi)	Stress for Fotigue Life of 20 yrs	Stress for Fatigue Life of 28 yrs
1001	4.358	4.53	6.10	5.38
1003	3.306	3.44	6.10	5,38
1006	3.613	3.76	6.10	5.38

Moximum Punching Shear from Appendix A. 4

SECTION 5 FATIGUE LIFE OF STRUCTURE

5.1 INTRODUCTION

Comment of the second of the s

Fatigue life of structure is evaluated in accordance with the method presented in Reference 4.

Sheet 5:02 of 3___

By C. Cherr Client U.S. NAUX _ subject Fatigue Analysis _____ Date 8-4-76 Job No. 27-771-100 _ calculation Fatigue Life of Structure.

5.2 FATIGUE LIFE - PUNCHING SHEAR CONTROL

From Eq.(9) in Ref. 4

$$Y = cNr$$
 (9)

where Y= fatigue life in years c = constant defined by Eq.(10) $c = \frac{\{\ln(rM_1)\}^{gm/g}}{M_1\Gamma(1+gm/g)}$ (10)

Design punching shear stress range for joint #706

From Fig. 10.7.4 AWS D1.1-72, Line k-K (p. 602) $N_r = 4.5 \times 10^3$

Since C = 0.0311 $Y = 0.0311 \times (4.5 \times 10^3)$ = 140.0 (Years)

Sheet 5:03 of 3___

By C. Chern client U.S. NAUY __ subject Fatigue Analysis _____ Date B-5-Z6 Job No. ZZ-771-100 _ calculation Fatigue Life of Structure.

5.3 FATIGUE LIFE - NOMINAL BRACE STRESS CONTROL

Y= cNr

Design nominal brace stress range for joint #706

Sr = 13.586 Ksi

From Fig. 10.7.4 AWS D1.1-72, Line D'-D' $N_r = 2.4 \times 10^4$ $Y = 0.0309 \times (2.4 \times 10^4)$

= 741.6 (years)

SECTION 6

MODIFIED GOODMAN DIAGRAM FOR DESIGN

6.1 INTRODUCTION

See a la section de la company de la company

Set forth herein is the graphical representation of fatigue strengths.

The documents employed for determination of strength limitation are as follows:

- (a) Manual of Steel Construction, 7th Edition, American Institute of Steel Construction, New York, N.Y. 1969
- (b) Specification API RP2A, Recommended Practice for Planning, Designing and Constructing Fixed Offshore Platforms, 7th Edition, Americam Petroleum Institute, Dallas, Texas, 1976.

Sheet 6.02 of 10__

By C. Chern Client U.S. NAVY _ subject Fatigue Analysis _____
Date 6-14-76 Job No. 27-771-100 _ calculation Modified Goodman Diagram ___

6.2 AWS ALLOWABLE FATIGUE STRESS RANGES

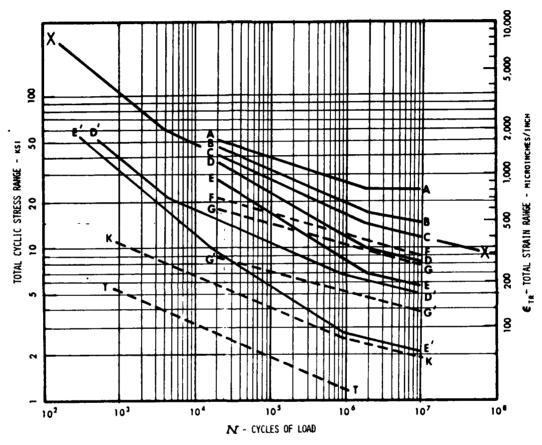


Fig. 10.7.4—Allowable fatigue stress and strain ranges for stress categories. See Table 10.7.3 $AWS \quad D \ 1.1-72$

Sheet 6.03 of 10__

By C. Chern client U.S. NAUY __ subject Fatigue Analysis _ Date 6-16-76 Job No. 27-771-100 _ calculation Madified Goodman Diagram

Stress Categories For Type and Location of Material

AWS D1.1-72

Stress Category	Situation	Kinds of Stress
A	Plain unwelded pipe.	TCBR
ΛΛ	Butt splices, no change in section, complete joint penetra- tion groove welds, ground flush, and inspected by RT or UT.	TCBR
R	Pipe with longitudinal seam.	TCBR
В	Butt splices, complete joint penetration groove welds, ground flush.	TCBR
В	Members with continuously welded longitudinal stiffeners.	TCBR
С	Butt splices, complete joint penetration groove welds, as welded.	TCB'
D	Members with transverse (ring) stiffeners, or miscellaneous attachments such as clips, brackets, etc.	TOPR
D	Tee and cruciform joints with complete joint penetration welds (except at tubular connections).	TCBR
**D′	Simple T, Y, or K connections with complete joint penetra- tion tubular groove welds conforming to Fig. 10.13.1.1.	TCBR in loanch member (NOTE main member must be checked separately per category K or T.
E	Balanced tee and cruciform joints with partial joint pene- tration groove welds or fillet welds (except at tubular con- nections).	TCBR in member
E	Members where doubler wrap, cover plates, longitudinal stiffeners, gusset plates, etc., terminate (except at tubular connections).	TCIH, in member
••E′	Simple T, Y, and K-type tubular connections with partial joint penetration groove welds or fillet welds; also complex tubular connections in which load transfer is accomplished by overlap (negative eccentricity), gusset plates, ring stiffeners, etc.	TCHR in branch member (NOTE — main member in simple T, Y, or K connections must be checked separately per category K or T; weld must also be checked per Category G and 10.5.3.
F	End weld of cover plate or doubler wrap; welds on gusset plates, stiffeners, etc.	Shear in weld.
G	Tee and cruciform joints, simple T, Y or K connections, loaded in tension or bending, having fillet or partial joint penetration groove welds.	Shear in weld, (regardless of direction of loading)
x	Main member at simple T, Y, and K connection.	Hot-spot, stress or strain on the outside surface of the main member, at the toe of weld joining to anch member — measurai in model or prototype connection, or calculated with best available theory.
х	Unreinforced cone-cylinder intersection.	Hot-spot stress at angle, change.
х	Connections whose adequacy is determined by testing an accurately scaled steel model.	Worst measure hot-spot strain, after hakedown.
•••к	Simple K-type tubular connections in which gamma ratio R/T of main member does not exceed 24.	Punching speed on shear area of the nember as defined to 8.3.
•••T	Simple T and Y tubular connections in which gamma ratio R/T of main member does not exceed 24.	Punch a mear on shear area et n member as defin

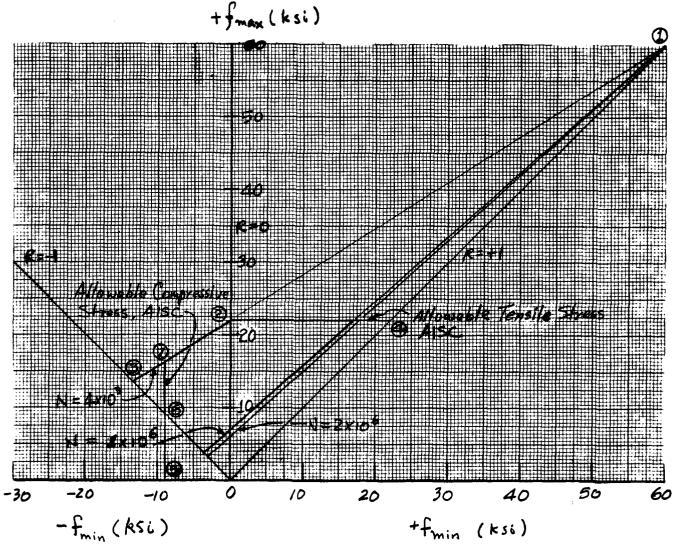
[•] T = tension, C = compression, B = bending, R = reversal

Empirical curves (Fig. 10.7.4) based on tests with gamma (R/T) of 18 to 24; may err on safe side for very heavy R/T greater than 24 reduce allowable stress in proportion to



Date 6-12-76 Job No. 27-771-100 _ calculation Modified Goodman Diagram_

G.3 MODIFIED GOODMAN DIAGRAM FOR SIMPLE T, Y AND K JOINTS - NOMINAL BRACE STRESS



A36 Steel

(NOMINAL STRESSES IN BRANCH MEMBERS)

(AWSD1.1-72 Fig. 10.7.4 Line D'D')

Sheet 6.35 of 10__

By C. Chern client M.S. NAVY __ subject Fatigue Analysis ____ Date 6-16-76 Job No. 27-77L-100 _ calculation Modified Goodman Diagrams

CONSTRUCTION PROCEDURES

1. For A36 steel, tensile strength is in the range of 58~80 ksi (See AISC 5-212, 7th Edition).

Say fu = 60 ksi, locate point @ on line R=+1

2. Refer to AWS diagram, the first kink point on Line D'-D' occurs at S=22 ksi, N=4x103.

Locate point@ (fmax = zzksi) on line R=0

- 3. Connect points Dand and extend to intersect Line R = -1, define point 3.
- 4. For A36 Steel, allowable tensile stress Fz = 22 ksi per AISC. In this particular diagram, Fz coincides with fmax at point. Draw a horizontal line to intersect with line R=+1 at point. Through point.
- 5. Line @-@ defines the allowable design in tension per AISC
- 6. Calculate allowable compressive stress Fa per AISC specification. Set Fa on abscissa (-fmin) to obtain point 3.
- 7. Draw a vertical line through point 5 to intersect line R=-1 at point 6 and line 2-3 at point 7.
- 8. Line @ defines the allowable design in Compression per AISC
- 9. Line 6-3-2-@ defines the boundary of allowable design per AISC \$AWS for a branch member in simple K. T and Y joints for Life cycle N = 4x10

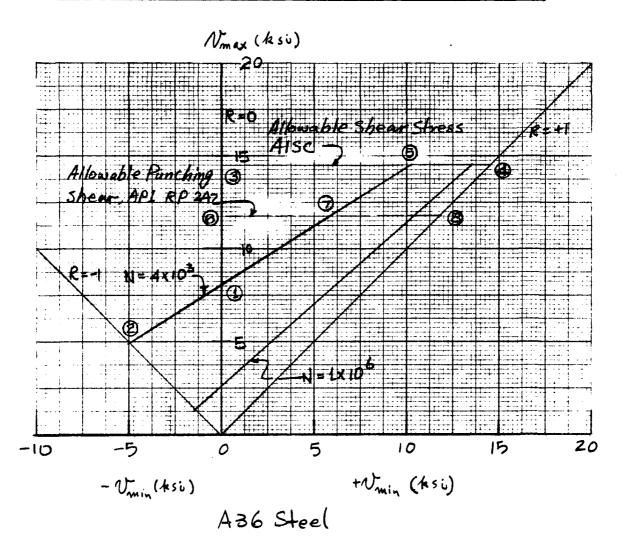
3

4

Sheet 6.06 of 10__

By C. Chern client U. S. NAUX __ subject Fatigue Analysis ____ Date 6-16-76 Job No. 27-77 L-100 _ calculation Modified Goodman Diagram

6.4 MODIFIED GOODMAN DIAGRAM FOR SIMPLE K JOINTS - PUNCHING SHEAR STRESS



(Punching SHEAR STRESS ON MAIN MEMBER)
(FOR R/T RATIO DOES NOT EXCEED 24)

By C. Chern Client U.S. NAVY _ subject Eatique Analysis _ note 6-16-76 Job No. 27-77L-100 _ coloulation Modified Goodman Diagrams

CONSTRUCTION PROCEDURES

Rafer to ANE digram, lines k-k and D'-D' are paralleled each place in the life cycle of N=4x103 and 2 = 1 × 106 , Ukk = Sois

where the is the total stress range in line K-K Smovis the total stross range in line D'D'

- 2. Al N=4x10°, Vmax = 8 ksi, set point Don line R=0.
- 3. Dain = Jain 2.75 =-4.91 ksi where Itain represents

- stress at point 3 in \$6.3 diagram

 to intersect line R=-latpt. Set - Dmin = 4.91 ks u on abscissa and draw a vertical line
- 5. For A36 stal, allowable shear stress Fr = 14.5 KSG rer XISC sprification. Draw a horizontal line through point (Comax = 14.5 + 1) to intersect line P=+1 at
- O. Time & Delines the allowable shear stress per AISC
- T. Connect points () and (2) and extend to intersect line 3-9
- E. Calculate Up ver ATI RPZA Eq. 23. Set point @ at Homax = Np.
- 9 Draw a horizontal line through point @ to intersect line @ D-1) of point @ and Line R=+1 at point @
- 10 Line D-10 defines the allowable punching shear per API RP 2A

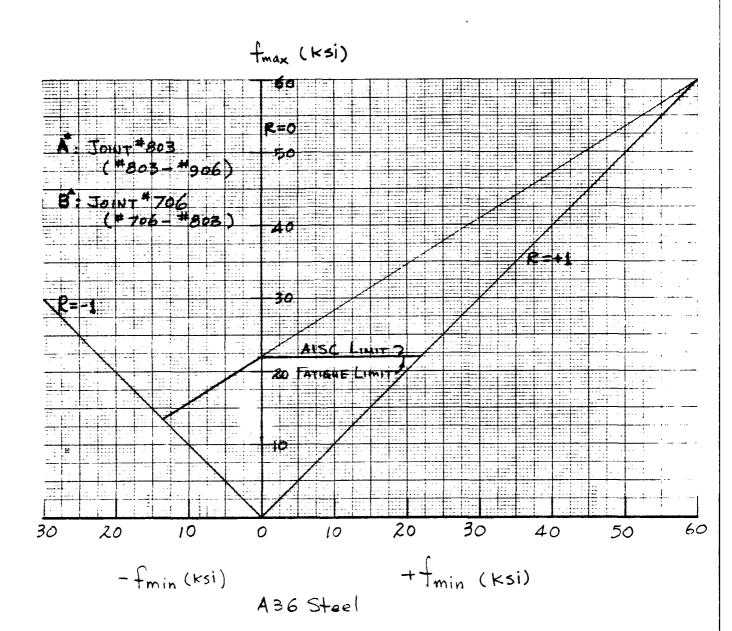
Sheet 3.2.3 of 10

By C. Chern client LLS. NAUX subject Fatigue Analysis _______
Date 6-16-26 Job No. 27-771-100 _ calculation Modified Gradman Diagram _

- 11. Line 3-0-0 defines the boundary of allowable design for shear stress on main member in a simple K-type joint for life cycle N=4x103
- 12. If the value of Up per API RPZA is greater than that of For per AISC specification, line 2 0 0 0 0 000 controls.

By C. Cheric Client U.S. MAUY __ subject Fatigue Analysis _____ Date 8-5-76 Job No. 27-77/-100 _ calculation Madified Goodman Diagrams

6.5 SAFE NOMINAL BRACE STRESS RANGE FOR FATIGUE

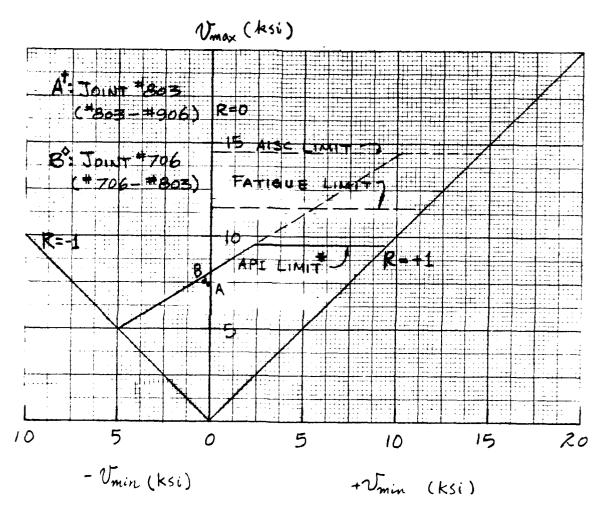


- * See Page 4.15
- A See Page 4.18

By C. Chexn client Ll. S. NAUX _ subject Fatigue Analysis

Date 8-5-76 Job No. 27-771-100 _ calculation Modified Goodman Diagram

6.6 SAFE PUNCHING SHEAR STRESS RANGE FOR FATIGUE



* Punching SHEAR LIMIT FOR JOINT #803 (#803-#906) \$\D0/NT#706 (#706-#803)

† See Page 4.05

4 See Page 4.08

SECTION 7

REFERENCES

American Welding Society

AWS STRUCTURAL WELDING CODE, AWS D1.1-72

2. Tall, L., etc.

STRUCTURAL STEEL DESIGN, Chapter 16 Fatigue, The Ronald Press Company, 1964

3. Welding Research Committee of the Engineering Foundation

CALCULATION AND GRAPHICAL REPRESENTATION OF THE FATIGUE STRENGTH OF STRUCTURAL JOINTS, Committee F Report No. 2, Welding Research Supplement, February 1942

4. Nolte, K. G. and Hansford, J. E.

CLOSED-FORM EXPRESSIONS FOR DETERMINING THE FATIGUE DAMAGE OF STRUCTURES DUE TO OCEAN WAVES, OTC Paper No. 2606, May 1976

5. Martin, C. A.

FATIGUE IN CONSTRUCTIONAL STEELS, Part 1 & 2, Machine Design, August 1965

6. Strommen, J. A.

NEW LOOK AT METAL FATIGUE, Machine Design, July 1974

SECTION 7

REFERENCES

1. American Welding Society

AWS STRUCTURAL WELDING CODE, AWS D1.1-72

2. Tall, L., etc.

STRUCTURAL STEEL DESIGN, Chapter 16 Fatigue, The Ronald Press Company, 1964

3. Welding Research Committee of the Engineering Foundation

CALCULATION AND GRAPHICAL REPRESENTATION OF THE FATIGUE STRENGTH OF STRUCTURAL JOINTS, Committee F Report No. 2, Welding Research Supplement, February 1942

4. Nolte, K. G. and Hansford, J. E.

CLOSED-FORM EXPRESSIONS FOR DETERMINING THE FATIGUE DAMAGE OF STRUCTURES DUE TO OCEAN WAVES, OTC Paper No. 2606, May 1976

5. Martin, C. A.

FATIGUE IN CONSTRUCTIONAL STEELS, Part 1 & 2, Machine Design, August 1965

6. Strommen, J. A.

NEW LOOK AT METAL FATIGUE, Machine Design, July 1974

APPENDIX A
PUNCHING SHEAR STRESS

			¥	22222222				
			\	222222222		Z	966666666666	
			*	22		Z		
			*	22		2		ر ا
		*	4 4	22	22	Z	. 16.	ي يو ر
			**		22			200
<u>a</u>			* * *	22		2		يد فر عا ار
		>	***	222222	2	3		
		***	. A.A.A	222222			200000000000000000000000000000000000000	KI KI KI KI
		***		22		7		
		>		22	2 2		. 40	
	00	*		22	2	2		
		*		25	Z	Z	- 14	i i
_		* *		22	2	2		1 1
	ນບຸບບຸນບຸນ	**		2422222222	Z	Z		#6#5FFFFFFFFFFFFFFFFFFFFFFFFFFFFFFFFFFF
	იიიიიიიიიი	*		2222222222	Z	Z	. L .	
						!		
								,
								•

.600000E+01 3.600000E+01 STRUCTURAL PUSIPHOCESSUR SYSTEM 27-771-01 START/END THETA ANGLE YIELD MUDDOUM U.S. WAVY 82.00 65.90 82.00 92,00 00.01 46.40 API CHOE CHECK, PUNCHING GHEAR FUR TUBULAN MEMBERS 105 FT MLM STRUCTURE • BAPCHK - CREST OFFSHORE, INC. DIAMETER THICKNESS END UF INFURMATION READ - FONCE BO MECUNDS TO BE STATED THICKNESS 47.500 20.000 12.750 14,000 20,000 47.500 KAJUINTO FUN FAFIGUE BRACE PHUPEHITES TABLE 4.000 20.000 TAPUT DAIL .400000+01 200. JUINT 803 803 80% IREBER NUMBER 707 707 707 707 707 707 CASE

SAPCHN - CHEST OFFSHUKE, INC. STRUCTURAL PUSTPROCESSUK SYSTEM

1. NAVY 27-771-01	ALLOWABLE PUNCHING BARAN
FATIGUE 105 FT MLM STRUCTURE U.S. NAVY 27-771-01	FOR /* - O T R E O G * - CALCULATED ALLOWABLE AXIAL BENDING PUNCHING OMERN BARBA
UINIS FUR FATIGUE 10	THICKNESS /= =S T
K FUR - KeJ	CIALETER
PUNCHING SHEAR CHECK FUR - KAJUINIS FUR	CHORD JOINT LOAD BRACE DIAMETER THICKNESS NUMBER NUMBER CASE NUMBER
PUNCHI	COLNT NUMBER
	N N N N N N N N N N N N N N N N N N N

						•							•																							
SINAT STATES			\$0.00°	8	6.403	6		90	6,903	6.903	6		6.403	6,903	9	6		٠.	₹.	6.903	6.403		6	6.903	6	6	!	\$00°	>	0	⊃ >		6	6.403	6	O
OIEAR			900	038	070	.175		.057	097	070	101		.262	162	425	.538		.135	,383	,373	. 200		.568	191	. 506	1,142]	E		929	0/7•		1,25A	•	Λ	•'
	;	0 1	.135	0.00	£50.	.123	. 415	5	27	100	770	970.	.435	186	, 428	* 414	770	. 232	1,159	176.	.077	.108	.591	\$75.	480.	.739	190.		1.730	•	904	.266	. 650		6	<u>.</u>
		671	000	045	.178	.100	640	040	670.	.162	.137	.393	672.	164	. 476	.545	,236	200	.051	,234	.281	.874	.811	,294	•	1.302	.340	. 114	• 07.5	807		2,097	•	•	1.644	•
	4	2	5	Š	200.	6	50	0	.5	200	00	50	1,000	20	.50	9	1.500	•	005	005.	1.000	50	1.000	S	20	ဌ	1,500	000	2000	005.	000**	1.500		005	205	200.1
		•	•	2.1	12.75	• •	2.5	9	2.7	14.75	o• o	٠,	5 0.00	~	ż	•	7.5	0.0	2.7	14.75	٠ •	7.5	20,00	2.7	۲.۷	•	7.5	20.05	, ,	~))	~	0.0	~	~ .	°.
			^	2	3 706	2	1 1	5 70	0 70	15 706	9	:	5 70	407 4	5 70	e E	ŀ	5 70	100	904 5	6	!	5 70	706	2 70	9		902 5) ·	5 ·	2 0 8		5 70	902 70	2 40	2
	!			70	20	2	-	9	2	70	20	1	3	2	2	2	•	3	2	20	20	5	•	2	~	ž	•	20		2;	2	1	•	2	~ ;	
	401			ļ			700					700					106					100					700					700				
	100						700 806					100 000					706 806			!		706 806					706 800					106 606			!	

ALLUMABLE PUNCHING BHEAN 6.409 6.400 6.400 6.400 6.400 4000 6.400 6.400 6.400 6.400 6.403 6.403 6.403 6.403 6.400 6.400 6.400 6.400 4000 4000 4000 4000 4000 U.S. NAVY E G G = 1/ CALCULATED BENDING PUNCHING BYEAR .126 .323 928 025 067 023 121 539 179 132 094 232 356 231 329 329 557 105 FT MLM STRUCTURE BIRUCTURAL PUSTPHOCESSUR SYSTEM 2.410 R.610 170 N C C E C 073 076 710 420 000 000 000 000 000 000 000 AXIAL 1000 379 377 326 552 153 200 200 300 300 300 300 300 KAJUINTS FUR FATIGUE THICKNESS 00000 00000 0000 000000 DIAMETER CASHURE, INC. 20.00 12.75 12.75 20.00 2000 2000 2000 2000 2000 2000 20.00 20.00 ं े . 20 • 60 80 • 60 CHECK FOR 30 M **BRACE** NUMBER 400 B 0 0 0 0 0 0 0 0 0 0 0 0 80 P P = 00 000 000 000 700 602 603 706 602 603 603 408 408 408 705 705 705 705 ° N M S 0 0 0 0 0 0 0 0 0 PUNCHING CHEAR CASE BAPCHA NUMBER 803 106 806 706 603 803 500 603 703 803 103 803 のこのない

## CHECK FUL		:				6				ا ا
AACE DIAMETER TRICAMESS /= -5 T R S D = -/ CALCULATED ALLUMABLE AXIAL BENDING SHEAR	CHEST O		, ,	TURAL FUR FA	X	8 7 8 J		> 4 2		
## 1	20 %		1 E T	. B	- 4	BENDING	₩ X X	LLCWABL UNCHING BHEAK		
909 24 250 1.000 1.372 1.252 2.001 909 2.001 9	706	:	20.00	1.500	3.146	0.00	1,558	100°4		
1000 - 0 000 -	~		20.00	1.000	1.342		2,667	6.903		
905 11,00 1,000 1,000 0,		;	20.00	1.500	0044	110	. 223	9 d		
		1	20.00	1.000	687	1.495	550	6.903		
	I	:	**************************************	; ;					•]
	1									
	ľ									
	1									
								•		
				!						
										· !

		900000000000000000000000000000000000000	888888	33333333333333333333333333333333333333		
-			대 대 대 대 대 대 대 대 대 대 대 대 대 대 대 대 대 대 대 대	100 100 100 100 100 100 100 100 100 100		
	APEX/SL 8.6.0	00 0 00 00 00 00 00 00 00 00 00 00 00 0	30333	00000000 00000000000000000000000000000		
	15,23.59, 10	222222222222222222222222222222222222222	22 22222 22 22 22 22 22 22 22 22 22 22	24 24 2422222222 2422222222		
	*UNITED CO	>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>	*	>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>	-	
				ກຸກກຸກກຸກກຸກ		
			1 1	1111		
	<u>8</u> 230	0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0		11111		
	PUY 206CB					: ::::::::::::::::::::::::::::::::::::

6.250000E-01 3.804273E+01 1.786967E+U2 3.60000E+01 BAPCHE . CREST OFFSHURE, INC. STRUCTURAL PUSTPRUCESSUR STSTEM 27-771-01 ULAMETER THICKNESS STARTZENU THETA ANGLE VIELD 46666666 U.S. NAVY CUDE CHECK, PUNCHING SHEAR FOR TUBULAR MEMBENS 105 FT MLM STRUCTURE END OF INFORMATION READ - FORCE 72 ALCUMDS TO BE BUNTED 20.000 BRACE PHUPENTIES TABLE 47.750 FULLINIS FUR FATIGUE 2.000000E+01 LUAU FACTUR 320 350 LNIOD FEREER CASE

STATEM - CHEST OFFSHUME, INC. STRUCTURAL PUSTPHOCESSUM SYSTEM

27-771-01	
70	
-	,
77	
-	
N	
¥ > 4 ×	
Z	
•	,
0.9	,
9	
	٠
×	
Ξ	
2	
=	
-	
ز	
_	
14	
105 FT MLM STRUCTURE	
_	
لط	
Š	
=	
4	
FUR FATIGUE	
5	
T-JUINTS FL	
Z	
3	
?	
-	
•	
<u>*</u>	
5	
CHECK FUR	
Ē	
ວ້	
*	
Ž	
ŝ	
	1
	į
ÿ	,
Ş	
_	1

S S S S S S S S S S S S S S S S S S S	CASE		7	LAICANESS	PXIAL PXIAL	N O O I I	PUNCTE PUNCTE BY NE ON THE PUNCTE BY NE ON THE	PUNCHENG BUNCHING BUNCHING	
1001 1001 100	2	1001 1001	2 2 2 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	1.620	5.400	3,104	4.265	9.671	10 11,12,13-6-23
1 100		1001 1004 1001 1002	47.75 20.00 20.00	1.620	9.601	4.559	5,169	9.671	of wrong
1 1001 100	1 12	1001 1004 1001 1002	47.75 20.00 2 20.00	1.620	011 8.322 8.809	2.465	4.183 4.373	9.671	
1 1001 1001	61	1001 1001	20.00	1.620.625	116 9.728 4.277	4.204	1.804	9.671	
1 1001 1000	*	1001 1004 1001 1002	20.00	1.620	000	. 145	.118	9.671	
1 1001 100	15	1001 1004	47,75 4 20,00	1.620	800°	. 014 . 070	0 11 0 0	9.671	J. Lg. 12, 12, 17 - Trangh of
001 1001 100	9.	1001 1004	20.00	1,620,625	156	170	123	9.671	Yan'i
1 1001 100	1 17	1001 1004 1001 1002	20,00	1.620	960.	.357	.050	9.671	
1001 Kuoi 8	10	1003-1005 1002 1003	20.00	1.620	9.452	1.602	5.276	9.671	
\$ 1003 Tuby	11	1003 1005	20.00	1,620	10.597	4.562	5.614	9.671	

SAPCHA - CREST OFFSHURE, INC. STRUCTURAL PUSIPACICESSUR SYSTEM

ender and the contract of the

Cont. Contract. Sections of the section of the sect

G G + +/ CALCULATED ALLUMABLE BERDING PUNCHING BAEAN BAEAN	4.862 5.037 9.671 1.693 .674 9.671	4	2,074 2,038 9,671	:	.1045 .131 9.671 .104 .051 9.671	.013 .609 .105 9.671	.271 .141 9.671	.121 .062 9.671	2.015 1.212 9.671 4.500 4.312 9.671	351 3,545	2.974	2,009 1,201 9,671 4,444 4,545 9,671	5.092 3.537 9.671 3.285 2.939 9.671	.030
ATICKNEGO O T K M	1.020 .025 .025 .025 .025		4.518			1,620 ,003	625	.047 .047	1,620 .218 .625 1.273 .625 7.159	1,620 ,200	\$ 625	1.248 1.248 625 7.838	1,620 ,264 ,625 5,871 ,625 4,663	1.620 .006
BEACE DIAMETER	47,75 03 1005 20,00 02 1003 20,00	74	005 1003 - 50.00		003 1005 20.00	47, 75	002 1003 20.00	003 1003 20.00 002 1003 20.00	47,75 004 1006 20,00 005 1000 20,00	47.7	0 7	004 1006 20.00	47.75 004 1006 20,00 005 1006 20,00	47.75

i

SAPCHA - CHEST OFFSHURE, INC. STRUCTURAL PUSTPRUCEUSUR SYSTEM

							Zewin	SHEAK	
900 1000 1000	\$1	1004 1006	47.75 6 20.00	1,620	. 121	9 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	199	114.0	
900 1000 1000	=	1004 1006	i	1,620	00.7	014	950		•
 		1005 1006	1	\$20.	.105	.231	146	9.671	
9001 9001 906	_ 17 _	1004 1006	87,75	1,620	000	010		9.671	† †
	-	1005 1006	00.02	. 625	151.	907	122	9.671	

^\$;

15.24.31 10.00000				FUNIT	TEU CO	EU COMPUTING* 67. APEX/SL 8.8.0	1PEX/3L 8.8.0				
No. No.				 	15		0/01/16.				
UNDONONON					* *	22525555	00000000		2 2	33	
Note		dd			**	22 23			3	35	
DO 00 1 1					*			*	3	3	
UN ON ATT THE SERVICE OF ON FFFFFFF ON ON ATT THE SERVICE OF ON ON FFFFFFFF ON ON ON ON FFFFFFFF ON ON ON ON FFFFFFFF					* *	77		•	20	2	
DU UU VYY VYY 222222		!				25)	14.	2	20	
UN ON ANY ANY 22222222 ON ON PEFFFFFF ON ON PEFFFFFF ON ON PEFFFFFF ON ON ON PEFFFFFFF ON ON ON PEFFFFFFF ON ON ON PEFFFFFFF ON ON ON PEFFFFFFFF ON ON ON PEFFFFFFFF ON ON ON PEFFFFFFFFFFFFFFFFFFFFFFFFFFFFFFFFFFFF		201000001000			>	25	000	44.	3	2	
00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		2020202022		***		2525252	ာ	2666666	200	3	
1		1		* * *	<u>~</u>	255555	0		3	3	
100 00 00 00 00 00 00 00 00 00 00 00 00		a. a.		>		25	ت 20	16.	3	3	
11 00 0 0 1 1		3		-		77	o 0	4.	25	n n	
1		12			:	25	0 70	10.	3	20	
1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	•	9				25	0	4	n	3	
00000000 YY 2222222222 0 000000 FF 000000000 UNDOUDUNUUUU YY 2222222222 0 000000 FF 000000000		. 3				20	, ,	9.4	חח	חח	
AA DODODO D SESSESSES AA DODODODO						***************************************					
		l a	10000000000000000000000000000000000000			2525252525	O	L 14.	ากกากกา	חחח	
]				! - - 		
										,	

			! ! !	: 	,						!



API CODE CHECK, PUNCHING SHEAR FUR TUHULAR MEMBERS

BRACK PRUFERTIES TABLE				
•	AREA	MODULUS	YIELD	•
000000c+01 6.25c00 Luad Factur	5,8042735	1.7A6967E	3.600000E+01	
1,530 1,530 1,530				
1.550				
END OF INFORMATION MEAD - FORCE	סאכנ			

ALLUMABLE PUNCHING SHEAN 9.181 9.181 9.181 9.181 9.181 9.181 9.181 9.181 9.181 9.181 U.S. NAVY CALCULATED PUNCHING SHEAK 3,534 4.686 4.590 5,037 2,610 1,395 2,415 2.241 5.314 2,633 FT MLM STRUCTURE STRUCTURAL PUSTPHINCESSON SYSTEM . 221 2.960 3.140 212 2.998 3.067 1.494 .299 1.732 3.782 1.968 . K 9 C 2.634 1.517 1.925 . 508 1.735 3.523 Ġ .014 8.752 8.288 012 8.463 7.981 4.642 10.748 . 232 001 8.800 4.604 1.771 5.903 THICKNESS /* -S T 4.521 .251 .209 9.514 4.107 8.801 T-JUINTS FUR FATIGUE . 50¢ 1.500 625 625 . \$000 • \$25 • \$25 1.500 500 625 625 . 500 . 625 . 625 . 50¢ . 625 . 625 625 625 625 1.500 UTAMETER APCHA - CHEGI OFFIGHURE, INC. 47.50 20.00 20.00 20.00 20.00 20.00 20.00 20.00 47.50 20.00 20.00 20.00 20.00 20.00 PUNCHING SHEAR CHECK FUR BKACE 1001 1002 1001 1002 1001 1002 1001 1002 1002 1003 1002 1003 1002 1003 1002 1005 1004 1006 1004 1006 LUAU CASE CCI2T NCTOFT 901 1001 1001 903 1003 1005 603 1003 1009 403 1005 1005 900 1000 1000 900 1000 1000 401 1001 1001 405 1003 1005 901 1001 100 901 1001 1001 CHURD



CAPCHA - CREST OFFSHURE, INC. STRUCTURAL PUBLICEUSUR SYSTEM

PUNCHING SHEAR CHECK FOR - TEJUINIS FUR FATIGUE - 95 FT MLM STRUCTURE U.S. NAVY 27-771-01

ALLUMABLE PUNGHING BHEAR	9.00	9,161		
/* *S T R E S S * */ CALCULATED Axial Bending Punching Syeak	1.335	3,663		
E S S I	303 1.679 3.528	2.026		;
ANIAL	1.674	6.341		
TICKNESS	1.500	1.500		
DIAMETER	20.00	20.00		
SAACE NUTBER	1004 1006	1004 1006		
CASE	•	•	- 1	X X
	90e 100e 100e	900 1000 1000	JUINT CHE	END UP HUN . SAFCER
CHUND	400 1	900	END UF	END UF

できないのないのな 一般のななないない

STRUCTURAL PUSIPHOLES INC. STRUCTURAL PUSIPHOCESSUR SYSTEM

Production of the second of th

						•		•			••							
	:	VIELD	77	36	9	9 6	36	25	36		YIELU							
		A ANGLE	00.00	81.62	~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	81.40	81.62	00.0	29.16		MUDULUS	• 7						
		START/END THET	~		N	, ~		nu r			AREA	2,7488945+01						
; ;		THICKNESS	1.500	2000	1,500		. 500	1.500	2005		(NE GG	5,000000E-01_2						
	V 1 V	UIAMETEK	47.500	10.00	47.000	18.000	16.000	2000	10.00	8 TABLE	į	•						4 4
	2	JOINI	1001	2001	1001	1005	1005	900	000	BRACE PHUPENTIES TABLE	470	.800000k+01	FACTOR	055.	1.530	1,530	200 m	
i i	-	3		í						. =		-						

SATIONS - CHEST DFFSHURE, INC. STRUCTURAL PUSIFHUCESSUR STRIER

BLE NG										ı				•												- · · · · · · · · · · · · · · · · · · ·					
ALLOWABLE PUNCHING BREAK			1.0	9.181		•		•		9.181	. 13		1.0	9.181		×	9.191		1.8	-		9.181	2		100	9.181		7	10		
CALCULATED PUNCHING BHEAR		•	2,137	. 35		•	1011		1	N. 619	•		•	62		00	4,038		00	•	:	9	3,506		.662			.87	2,300		
E 3 8/		=	1.507	۶۲.		2 1	200		740.	Z	6.013	870.	2	12	141.	3	5.486	100	4	3.035	192	1,041	2	198		8	455.	3.070	. 50	. 161	•
/5 T H AXIAL		090.	5.171	9.709		• ·	8.561		0	0100	?	• 000	.37	8.547	. 075	4.845	0.650	9 C O	-	7.605	.154	010	6.623	118	.261	8 7	.141	90	3,905	140	۲
SOUTH		1.500	005.	200	3	•	005	•	006.1	> 0 0	006.	1.500	.500	005	1.500		005	1.500	•	005	1.500	.500	200	1,500	005.	004.	1,500	005	005.	1.500	
CIAMETER		47.50	16.00	00.91	47.50	000	10.00		00.1		00.01	47.50	18.00	16,00	47.50	18,00	16.00	47.50	•	16.00	47.50	18,00	10.00	47,50	v	18.00	47.50	16,00	16,00	47.50	•
BRACE	:	•		-			300		800				2 00 1	1004		1003				_			~			1005			1006	!	
LUAD CASE N	:			1001	•	1001	1001	a	1001			01	1001	1001	^	1002	1003	•	-	1003	•	1002	1003	01	1002	1003	•	1000	1005		
NCT OF RE		****			1001		1	1001	•			1 1001			1003 1003			1003 1003			803 1003 1008		į	\$001 E0	•		0001			0001 0	
0101 0101 0101 0101		707 706			1001 109			1001				801 1001 100			001 509	,		903 100			03 100			605 100	:		800 1000			800 T006	



SAPENA - CHEST OFFSHURE, INC. STRUCTURAL PUSIPHUCESSUR SYSTEM

PUNCHING SHEAR CHECK FUR . T-JUINTS FUR FATIGUE OF FT HLM STRUCTURE U.S. NAVY 27-771-01

D ALLUMABLE PUNCHING BHEAK	40.181	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
CALCULATED PUNCHING BHEAR	899	3,613	
THICKNESS /= =S T x E S S = =/ CALCULATED AXIAL BENDING PUNCHING BHEAR	4,266	2.213	
A 88 T .	. 124 6.540	138	ļ
THICKNESS	000. 000. 000.	5000	
UIAMETER	14 . 50 16 . CO	18,00	!
E PACIFICATION CONTRACTOR TO THE PACIFICATION CONTRACTOR TO TH	1004 1006	1004 1006	
CASE	•		3
NOTE OF THE PERSON	909 1009 1009	606 1006 100	JUINI CHE
N N N N N N N N N N N N N N N N N N N	1 000	000	END UF JUINT CHECK

APPENDIX B
STRESS ANALYSIS

RELEASED TRANSPORT THE WORK OF THE PROPERTY OF

PRINTED RESIDENCE SAFERS

Compand	AA DO DO DO AAAAAAAAAAAAAAAAAAAAAAAAAAA	00000000	,00/16.		
ОСПОПОПОПОПО ОО ДА ДА ПО ПО ДА ДА ДА ДА ПО ПО ПО ДА ДА ДА ПО ПО ПО ДА ДА ДА ДА ПО ПО ПО ПО ДА ДА ДА ПО	AA INDODODOO OO AAAAAAAAAAAAAAAAAAAAAAAAAAAA	00000000			
GUGGGGGGGG DDDDDDDD WW WW AND	AA DO		3 3 3 3 3 3 3 3		
A	AA DOD DOD AAAAAAAAAAAAAAAAAAAAAAAAAAAA	00	******		
GGGGGGGGG	AA POO OO AAAAAAAAAAAAAAAAAAAAAAAAAAAAA	20	T. T.		
A	AA DO OO DO	20		,	
No. No.	AA IND DODODO ON AAAAAAAAAAAAAAAAAAAAAAAAAAA	00		, .	
GEORGEOGO DO NA HARANAN AN OO OO ALA ALA OO	AAA OO OO AAAAAAAAAAAAAAAAAAAAAAAAAAAA	1 20) (
A	AAA DO DO DO AAAAAAAA DO			، ر ۱ د	
A	AAAA DO		:	ננ	
NAT NAT	**		ひとひとととととのととと	ور	
AL	A DOUBLING OF THE PROPERTY OF		KKIKKKKKK	00	
CONTROLOGO CON	λ		X		
A	A COUNTY OUT				
αια 33 33 34 44 00 000 Δ. Γ.	λ				
000000000	TENNONDANA PAN TENNON		×	ננ	
000000000	λ			ü	
ממממממממ אא בככככבבכככ מממממממ אא בככככבבכככ מממממממממ אא בככככבבכככ מממממממממ אא בככככבבכככ	ר המתוחתחחחחים .				
חמתמתחתים אא פחסססחס אא לכככככככ		0			2000
		0000000			CONTRACTOR OF THE PROPERTY OF
					guaringanan
					-

		•			
BIRAN BULLETIN BS	THE NEIMUD FUR CALCULATING THE MUMENIS, SHEARS, AND AXIAL FUNCES AT THE EXTREME ENUS UF A MEMBER HAS BEEN MUDIFIED TO CURRECTLY LNCLOUE CUNCENTRATED LUADS ON HOMENIS APPLIED AT THE ENUS UF THE MEMBER, THIS TECHNISUE IS HELIEVED IN GIVE THE FOUE EVALUATION UF THE ACTIONS AT THE ENUS UF A MEMBER HAVI'S END LOADS.	1. ALL MENUER STRESS REPLIES DAY HE EFFECTED. 2. SAREAM STRESSES ALL CHANGE ANERE CONCENTRATED LUADS ANE 3. SAPPLIED AT THE AEMSER END. 4. SERVING UN TURSTONAL STRESSES WILL CHANGE ANERE MUMENT 4. STRESSES UTARA THAN AT THE END ANERE THE LUAD IS APPLIED 4. STRESSES UTARA THAN AT THE END ANERE THE LUAD IS APPLIED ALL WILL WILL CHANGE. 5. MET GENS ALTHRUT END LUADS MILL MOT CHANGE. 5. THE MENDER PURCES AND MUMERIS WERUNT CHANGE.	HAVE YOU REAU BULLETIN NO.4 HEGARDING THE NEW ALLUMACLE STRESS AND CALLY CALCA FEATURES. NOTE - 1F YOU DO NOT HAVE ALL OF THE BULLETINS, YOU HAY URTAIN A CURY BY SURMITING A MON	E CONTRACTOR AND TOTAL COLOR CONTRACTOR AND COLOR COLO	

STRAN A SYNEKCUM TECHNULUSY INC. UEVELUPMENT & RELEASE & MUU 15 REPUESTED FUN THIS ANALYSIS LIAD CN 8 2 7 F MAYE — CREST LUAD CN 8 2 7 F MAYE — CREST LUAD CN 8 2 7 F MAYE — CREST LUAD CN 8 2 7 F MAYE — CREST LUAD CN 8 2 7 F MAYE — CREST LUAD CN 8 2 7 F MAYE — CREST LUAD CN 8 2 7 F MAYE — CREST LUAD CN 8 2 7 F MAYE — CREST LUAD CN 9 F 42 F T MAYE — THUDGH REPUBLICAN PRINCIPLE ON							
# # # # # # # # # # # # # # # # # # #	10 FUR 4514 STEEL.		7.2.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3.	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	N H C H C C C C C C C		
INPUT IN	2.13. K.19. PESCLIS INVALLS FUR L. S. N. C. SEGRENIG L. S. VANNE - ERS. SEGRENIGES	2	801C 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SECTIONS OF SECTIONS AND SECTIONS APPROACH SECTI	M DE KELTER ON THE SECTION AND	**************************************	ELUIELAMIUM CHECK EUIT VALUES

HAVEL BESTER BESTER BESTERE BESTERE FOR FOR THE SAME BESTER FOR THE SECOND BESTERS BESTER BESTER BESTER BESTER

THE COUNTY OF LEAST TO SEE TO SEE THE SEE SEE SEE

ŀ	1			i i		1			1			,			1						į			i			1				:	
i						į			1			ļ			1			:			; 						ļ				ł	
,	1 AP CT SEC. LEN	F T.			00.0	•	•	0000	•	0000	00.0-		00.0-	•	00.0-	•	•	00.00	0	00 00	٥,	٥.	0	C	00"(~	00 00 00 00 00 00 00 00 00 00 00 00 00	٥.	٠.	•		00°0-	0 • 0
	BHEAK			~	3	~	3	٠,	*	•	•	٥	٥	φ.	9	6.0	5.0	7:7	۲.	3		5.5	0.0	5.0	5.0	7.1	1.4	7.7	5.3	~	5.3	3.7
	K2	•			0	•	•	•	•	•	•	•	20.	ė		•	₹.				9	•	٠.	•	•	9	•	•	-	1.0	•	-
	×				0.1	•		•	•	•	æ.	9	2.6		1.6	Ð	7.0	•	Ð	•	•	•		•	•	•	1.0	•	•	1.0	3.	ુ .
	, d	KSI			•	•	•	•	•	;	•	•	;	36.0	;	•	ò	ċ	•	•	•	•	Ġ	ċ	å	÷	ċ	ò	ċ	ō	٥	÷
S.O FEET	12	727		v	^	Š	_	~	~	Š	š	v	v	312.76	\sim	~	v	~_	~	786.9	5.0	3.00	9.0000	1.1750	1.1.50	46000	٠,	1008.	7846.5	7.444.		5.1
3 - MLH 10	17	124		05.5	0.7	24.5	. 7	٠.	60.7		61.5	41.5	61.5	374.76	43.7	72.7	5.5	33,99	155.1	746.4	4 4 0 H Z	2 K2	4896.5	0301.1	0391.1	コ・ハモコロ	1000	10001	,† 10	17004.56		1.450
MEMBER PHUMERTIES	×	オスイ		=	21.	3	2	521.47	41.4	25.0	23.0	2.5.0	25.0	745.54	51.0	45.5	57.	53.R	\$ 90	15.9	13,9	4111.6	9143.6	0706.6	0124.2	01/0	11.5	4017.3	5704.1	578	5754.1	105.3
PLATFURMS - FATI	¥¥	2×1	***		7	-		11,41	ું.	ď	•	ď		Э,	J.			24,55			•	÷	421.44	51.	5.	ζ.	-	σ.	٥		e.	1
NAVY - ACHR PL			110000000 PSI																													
°0°	â	2	9	8.02	10.75	~	~	10.75	~	`.	~	12.75	14.75	00.44	14.00	34.00	٠,	2	13.00	00.07	20,00	30.00	00.54	v	0 : • V	00.00	\$	5.5	45.50	45.50	45.50	10.00
		* N	0~0000006	500	.365	770	. \$05	. 565	1,565	. 200	200.	200	. 200	275.	005	. 375	. 625	2000	30¢.	.625	1955	1.000	1.750	2 C S	000 V	7.75	1,000	0000	٥. د د د	500	9.500	004.
	42105 47147	<u>.</u>	*** * * *	20)) ·) ·	20.0	30.0	<u>۔</u>	•	٠ •	٠.	22.0	? o • o •	Э.	20.0)))	20.0	00.0	•)))	00.0	3 · · ·	ာ	•	ح.	> 0•1	ာ	•	>0. • ∩ •	30.0.	30.9)) (
	8/1					-						-	-	, D	-			-					 .	_		~	→				-	
	2 6 9		ľ	000	105	100	101	٠ د د	ا جو اات	25	125		15/) : = :	0	3	202	→	C Œ	ر ان ان	୍ଦ	, 5	. , , 3. (2		3		ं ज		0 TO. 4	٠, ٦	Ď

STATES AND STATES AND

	,		1	·T	-}	·- F	1 :	- y . =	i	<u> </u>	1	1	r · · 	· · · · ·	1	r	1	1
 				!	ı	i	1		1		†	!		: ! 	1	! !	: 1	† †
	INPUT EC LEN	•	000	, -	ı	i	ı	ı	1	į		1	: 					Ì
1	S E C			1			!	i i		!	1							
10/05/76	20 -	-	000		į												<u> </u>	
	2		N 0 0															
DATE	K.2		200		:		!						 	•				
	KY			Ì														
	> u. dt		36.0	1														
FEET	71		18.20											-				
05.0 E8																		
MLH 1 PERTI	> I	!	802.00															
18 • R PHÜ		•	0.00															
FATLGUE ANALYSIS - MLW 105.0 . CUMPACI MEMBER PHUPENTIES		,	.34															
GUE A PACT	×	•	-															
FAT1	AX	•	0															
FURMS . F E FLANGE	*	•	7.00															
LATFU	DEPTH		2000															
- ACHR PLATF FLANGE/HIUE	!	37	: -	İ														
- 1	FILES	*0000	356 . 500 245 . 500															
-	T T T T T T T T T T T T T T T T T T T	1100	25.5													 		
8.0														 	1			
	FLANGE		05.0															
	2 H Z)))																
	T P SCE	0000	3570									<u> </u>						
	17107 17107 17107	-	1	1														
	1	:	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2															
	8/I		000	1							1			 				
اريا	3	2 = 2		_ و	1	ļ.,.,	1 7 2 2	1	1	ļ	: 	'877.		,	; J ; 3		l <u></u>	<u> </u>

00.00 1.0 30000.00 36.0 U.S. NAVY - ACMR PLATFURMS - FATIGUE ANALYSIS - MLM 105.0 FEET Phismatic Section members 50.00 30000.00 30000.00 PRUPERTIES 2 2 2 3 3

A P A O P D T S A S P -

ı													> • • • • • • • • • • • • • • • • • • •				
⊃ z	2011	9 1 2 3	t 0	۵ /											!		
00 2	* 1	80 P	ļ	50003	000000	300	00 30	0000	- D 11	1 1	200	4					
נג נ רדיר) a d	ں ر	2 2	<u>,</u> 3	D	250	1800	920	2 6 6	762	6 0 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	300				
W 7	ť	×15) L &	Š	7	!	010	₩	:O	•	000	~					!
5	Þ	5	•	102	0		2	•	100	_	200	٥					
,		1000		0.75	705		16 36		001	001	000	0				*	!
K K		(-	4	ŭ iŭ		 > =	9 4 9 4		0 0 0		3 S	<u> </u>					
, ,	4).3		175	S	3	16		100	•	200	0					
5	-	**	-	175	٠ ک	 >	16 5		100	_	200	0					
à	. ••	7	7	175	00	7	16 5		Ç Q		200	0		!		. !	ļ
Υ.		7.		275	00	1	16 3		0.20	İ	900	0					
Y	-+ .	~1 ·	-4	5/2	.	~ .	5 91		0		905	: ن					
X,		1		:75	0 :	-	5		00	- !	200	0					-
Y 1		,		0 6	. .	⊶ . • :	٠ د د		J .		005	ت					
	-		7 J	20) (, -	0 0		9 5		V V C V	2 5					
7		! :	; ;		1.5	7			100		202	0					1 1
.*		,	÷.	000			\$ 91		001		005	0.					
Υ .	•		<u>-</u>	0 0	= u	- ·	5		0		305	0 6		1			1
. 1	W S		ű N	0 0	n .n	 	0 4		9 9		9 C A) 0					
,	١,	•	<u>ښ</u>		0 0	·	15 5		001	-	900	9					
•			7	0	75.9	7	16 3		0.0		005	0		1	•		. 1
•	<u>)</u>		3	3 (2)	0 :	⊶	10 5		001	_	30 5	0.					
		:	3	ا م د) 0 0 0 0 0 7	 	e :		6 S	٠.	705	1 24			1		!
	3		- ^ 	o =	0 5 6 7 7 5	 	0 4				, c	<u>ء</u> د					
1	1	2 13	3) r	0 0		n .			-	3 0 0 2	2 3					
			3	73	0.5	,	1.5		100	• ,	300	 		-			
5	3	· · ·	7	350	0.0	~	16 3		300		500	0					
3	7 1	*	4	300	00	-	16 5		0 2	~	305	0,					
٠.	5 t	•		0	o o	~ ·	94		00	-)))	0					
5	ı K	9 0	:		. •	• •	2 4 4)		0						
5	٠ د د	45454 A				7	16-3		001	100	10		 				!
<u>Y</u>	¥ :	o mbx1			-	~ >	1.5		•								
Σ.	. ند 10 و ع	!	-				1										
7 3	įΣ	101 102											000				
	1 E	201	3														
.E.	D T	0.2 50	'														
F.	ы В Е	01 10	*										1000				
, ,) 0 1	-	~ ;										000				
4	1 L 2 C 3 T) ·	>										200				
L			;										1 1				

U.S. NAVY . ACHR PLATFURMS - FATIGUE ANALYSIS . HLH 105.0 FEET 105 RIDIA FIGHT 101 101 A TYOPE TI TOTA THOLK. PIETORA KADERA コドルシドス PERCER AL TOER FRICKA MI KOEK 4 10 1 1 アモバロたず LINE

ASSERT ESSENCIAL CONTRACTOR DEPOSITS CREATER SAME CREATER

PAGE 3 MLW 105.0 FEET DAIE 10/05/76	7 65	3032	5032	3032	2053	できる ないしょく かんしょう かんしょう かんしょう かんしょう かんしょう かんしょう かんしょう かんしょう かんしょう しょうしゅ しゅうしゅ しゅうしゅう しゅうしゃ しゃくり しゃくり しゃくり しゃくり しゃくり しゃくり しゃくり しゃ	2055	2033 2033	1151	1/5/	0000	0 0 0	0000	3030	3032	3052	2205	2505	5022	5022	1157	1757	nano	0000	, , , , , , , , , , , , , , , , , , , ,	9999	5032	3032	1842	1272	1972		1757	1757
NAVY - ACAR PLATFURRS - FATIGUE ANALYSIS -	3 4 4 5 5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0											•	1111	11:1										111	1111	1111								
° 0° 2	1 1 2 2	544 703 200 543 645 200	700 2	701.2	705	75.5	40,	2 2	704	 . v	707	£ > ^	711	712 023	9 : 2 :	/US 501 200 /US 503 200	7 0 + 10 10 10 10 10 10 10 10 10 10 10 10 10	7 . 7 7 C	1 C		3 to 1	805 1	F 0 1		- 10	#15.	10 A	401	200	>	404	01 40¢ 10 04 404 10	1 406 20	905
	LINE NU. 1S	2.00 2.00 3.00 3.00 3.00 3.00	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	10.1	104 MERO	10 4 4 1 1 0 0 1 1 0 0 1 0 1 0 0 1 0 0 1 0 0 1 0 0 1 0 0 0 1 0	101 Lat		0.11	114 36 60	115 750	115 "EMD	110 75 75	110 75 0	7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	160 75.05	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	10.12. 12.1	7 1 2 0 F	160 TETOTA 167 TETOTA	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	150 "15"	151 757 05	7 7 7 8 9 1 1 1	156 77.50	150 7545	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	7 40 5	[1 0 0	75.40 5	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	O METOR	7 75.05

U.O. NAVY - ACHR PLAIFURIS - FATIGUE ANALYSIS - MLH 105.U FEET LINE NU. 1...5....0....5....5....5....5. 10.71010 10.700 X8.00 10.01010 10.010 9031905

R.F.

5 6 6 7 7 8 .505050	F 6623		m 6/25/	1 6547	/2CO 4	7.50.7		7.524		0000			0000		0000	1 0000 4	j	1 0000 ta	F 0000								0.164 0.188	0.430 0.700		1,136 1,440	
2 V																		٠				20.0	2007				0.153	0.270		904.0	040 0
3 4																					• 00•	3	05.1	,			0.129	0.120		0.611	0.110
5 3																				=	600	2	66.0	. :	0.02		0.107	0.00	20.000	0.366	0.050
1 1 2	51 701 JL	35 /US 2L 36 /U6 JL	20 20	10 404 90	01 401 Ju		01100110	16 500150	7 5 5 7 5 7 5	US 511 K	x 215 00	d 112 11	12 712 "	1 1	12 012	10 410	12 912 7	7 010 010	215 210	1	000	, 3	•	· •	2 2	ے م	0.0		240.1	, 5	2 2 2
		ا .		!		. ~		٠					!								ייני דרה - ז'ט	•) 2 3		1 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	_	7×CF	 	, r	ר ה ה ה	ر ا و

⋖
-
~
٥
٥
-
3
3
Z
-
_
z
•
Œ
-
8

1.77

											•										The same of the sa							Andrew Community and the community of th									
THE PORT OF THE PORT OF THE PORT OF THE		OX HRACE			3 LEVEL 5 LEVEL			יין איין איין איין איין איין איין איין			ר היי היי היי היי היי היי היי היי היי הי			,	יא ליני אין ליני איני אין ליני איני	BUAT LUG					X	*J.		2 3		901 140P		1	•			7 LEVEL	į.	7 LEVEL 7 LEVEL		7	7 LEVEL
	4 4 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	6.74 150	0.57 121.5	6.74 121.5	0.13 117.0	0.15 117.	57 117 °U		0.00 117.	0.00 117.4	3	4.611.81.0	7.44 116.4	0.45 11/0	, , , ,	V.25 111.	, 45 111.	5.25 111	5.45 111	5,25 11	9.75 105	9.75 105.		9.44 105	0.45 99.	0.k5 44.	**	> 52.5	£4 57.C	20.00	0.03 42	5.41 42.0	5,41 746	1.66 46.0 4.08 42.4	2.08 92.E	4.16 42	0.63 01.0
	50.	0 0	14.50	0 M	0.0	-15.15	· -		17.36	-17.35	. v	-15.:5	0	17		15.1	15.		·		-1.55	10.70			17.74	- 17.71-	17.74	3.6	-17.74	13.70	1.8.70	9.58		50.0	50.07-	0.0	18.76
		02 1210	0.7 1.4.70	0 7	05 1.10	01.41 >0	30	50	05 11.10			10 1110	16 1210	70	10	06 1110	00 1.10			7	70 1.10	50 1×10	20.4	117	که _ ۱۲۱ت	76		49 1.10	80 70		0/ 1210	01 1010	01 - 1 - 10	\	2	01 1110	
	NE 40.	\$ 20	, ,	2 -	, ,	<u>-</u>	. c	, ,	ָר ר	ء م . د	, ,	دار	¬	۰ سر			7	o ~	· n	•	, ,	٦ س	¬ -	ר נ	٥.	っ ⁻		"	→)) T		٠,	ר ר		٠ د	⊸ ^

歌

(:::

1 2 2 2 2 2 2 2 2 2
1
11.2
CTTURE TTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTT

A CONTROL OF STREET STR

		+					1						!								:			1					: ! ! ! ! ! ! ! ! ! ! ! ! ! ! ! ! ! ! !			•					1 1 1					:	
					•							•																				•											
00	 -		-	7	-	⊶ ·		⊶ •	~ ·	-	 	• •	• •		•	-		-	-	~ >		 	 	-	0	7	~ .	~ ·	-	• -		-	-	7	·	⊶ . ⊃ :	2 -	• ~	• ~	-			
5		1		1						- 1			-			i			1		- 1			i		i			1											1		>	7
7	<u>.</u>		116	1	ا ساء	<u>.</u>	<u>.</u> !	<u>.</u> .			L 14				. =				4.7	<u>.</u>	2	<u>.</u>	L 4	1	11.6	116	ik 1	L 4	1	- la	<u>.</u>	17	41.	116	3- 1 	M .	4 2		. IL		1 1 F	u	
5.																																											
9 >	3 3	5 3	3	3	3	3	5 :	5 :	5 8	5 3	5 3	5 3	ق	3		5	:5	3	5	5	3 	5 3	5 G	3	3	3	5 :	5 3		5 3	3	5	3	3	ਤ :	5 :	5 3	; <u>;</u>	; <u>ड</u>	5	3	5 (١
. v.																																											
5																																											
3.70	0 0	2 2	9 0	S	9	S	~	9 6	V *	3 0	y #)		-			90	90	3	~	5 0	> 0	2		5 0		-0 P	? •	-	. 60	,	_		_	-	→ (2	•	• •	-			
70	43	1 ~ 1	~	1	~	_	つ :	つ :	> 0	> :	> =	۰ ٦		· ~	1 7	~	~	7	13	3	3	7 :	7 3	~	V	v	v	v 1	v	, N	v	3	•	>	~ 1	•	7 ~					51	4
3	3		~	1	17	~		~ ·	^ ~		•	•		•	-		•	~	~	~ →	ا	~ ~	n. n	_	_	-	-,	•		. ~	~	3	7	3	_	_		_	~	1	7	-	
	0		5 0	ر ا		□	0	3 .	0 0)		0	-	2		୍ଷ	2	2	0	2 2	3 3	n (1) > 0		3	-		5										·					
20	0 1	17	٥	٥	• •	.	· :	•	•	•	• •		. ~		•	~	~	~	۲.	~	'n	0 1	• 7	· •	.	٠	٦,	٠,	• •	, ,		٠.	٠.	٠.	3	?:	> 1		. ~	٩	•	٥	1
- M	W 10			2	~ ·	.	: 	.	. .			٠.		•	. ^.		~		_	~	5	H	-		•		⊷ .	n =	-			2	~	5	•	e.		. 0	ı.		-	- -	
- 2	9 7	7	740	9	- -	מי	• ·			C ,4	: :	. ~	2 2 2	2	2	2	2	150	15.5	130	0 M	0 1 5 1) -	~ ~ ~	22 7	25 7	~ .	. ·	- ^ u ^	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	~ ~ ~	4.50	ر د د ه	2 .	~ ' S'	2.	C	. ~	25.	S	25. 7	ر دی	4
5.		-	×	_	>	. ,	× '>		< >	. !.		4	(►)	4	>	· ~		~	-	×	•- ,	٠ ،	>-	-	-	~	٠,		, · , · <	: >	7	*	۲	7	٠ :	- •	•	٠ >	~	١	> '	7	
1	5	5.5	5	5	₹	٠ أ	5	5	5	5 1	, 5	, 5	3	4	5	3	4	5	5	5	٠ د	٠ ج ا	9	, 4	₹	5	5	5 3	, ,	3	5	3	5	5	5	5 :	9 4	5 3	3	5	5	٠ ١	4
INE NU.	2 2	•	97	265	•	•	3 (> :	, ,	> -) 7)	· >	-	ာ	-	_	-		-			•	_	\sim	v	v •	ÚÌ		ιũ	~	v	V	~	9	~ -	9	•	•	•	*	√	7
	1 1 2 2 3 3 4 4 5 5 6 6 7 7 7	NU. 150050505050505050505050505050505550555.	NU. 15005005050050050050050050050050050050500050050050050050005005005005005005005005005005000500500500	NU. 150550505055050505055050505055050505505050550505505050550505550550555055055505555055	345 LUAD 7 514 653 11.35 06 5.53 06 GLUB UNIF MY 0 545 LUAD 7 514 653 11.35 06 3.53 05 GLUB UNIF MY 0 546 LUAD 7 514 653 11.35 06 3.53 05 GLUB UNIF MY 0 547 LUAD 7 514 653 11.35 06 3.53 05 GLUB UNIF MY 0 547 LUAD 7 514 653 14.67 05 3.53 05 GLUB UNIF MY 0 547 LUAD 7 514 653 14.67 05 5.33 05 GLUB UNIF MY 0	345 LUAD 7 514 653 14.07 05 5.53 05 GLUB UNIF MY 0 545 LUAD 7 514 653 11.53 05 5.53 05 GLUB UNIF MY 0 546 LUAD 7 514 653 11.53 05 5.53 05 GLUB UNIF MY 0 547 LUAD 7 514 653 11.53 05 5.53 05 GLUB UNIF MY 0 547 LUAD 7 514 653 14.07 05 5.53 05 GLUB UNIF MY 0 547 LUAD 7 514 653 14.07 05 5.53 05 GLUB UNIF MY 0 547 LUAD 7 514 653 14.07 05 5.53 05 GLUB UNIF MY 0 547 LUAD 7 514 653 14.07 05 5.53 05 GLUB UNIF MY 0	345 LUAD 7 514 653 8.00 00 5.43 00 GLUB UNIF NV 0 5.45 U.A. 7 7 7 7 7 7 8 8 8 8 8 8 8 8 8 8 8 8 8	345 LUAD 7 514 653 11.53 06 5.53 06 GLUB UNIF NY 0 5.55 LUAD 7 514 653 11.53 06 5.53 05 GLUB UNIF NY 0 5.45 06 LUAD 7 514 653 11.53 05 5.53 05 GLUB UNIF NY 0 5.45 05 LUAD 7 514 653 11.53 05 5.53 05 GLUB UNIF NY 0 5.45 LUAD 7 514 653 14.67 05 5.33 05 GLUB UNIF NY 0 5.45 LUAD 7 501 662 0.00 0.00 0.5 17.74 0.5 GLUB UNIF NY 0 5.45 LUAD 7 501 602 0.00 0.5 17.74 0.5 GLUB UNIF NY 0 5.45 LUAD 7 501 602 0.00 0.5 17.74 0.5 GLUB UNIF NY 0 5.45 LUAD 7 501 602 0.00 0.5 17.74 0.5 GLUB UNIF NY 0 5.45 LUAD 7 501 601 0.00 0.5 17.74 0.5 GLUB UNIF NY 0 6.40 0.00 0.00 0.5 17.74 0.5 0.5 0.00 0.00 0.5 17.74 0.5 0.5 0.00 0.00 0.00 0.5 0.00 0.00 0	345 LUAD 7 514 653 11.35 06 5.43 06 GLUB UNIF HV 0 5.45 06 CLUB UNIF HV 0 5.45 06 CLUB UNIF HV 0 5.45 06 CLUB UNIF HV 0 5.45 05 CLUB UNIF	345 LUAD 7 514 053 11.35 00 5.43 00 6LUB UNIF HV 0	344 LUAD 7 514 053 11.33 00 5.43 00 6LUB UNIF HV 0 345 LUAD 7 514 053 11.33 04 5.53 05 347 LUAD 7 514 053 11.33 04 5.53 05 347 LUAD 7 514 053 11.33 04 5.53 05 347 LUAD 7 514 053 11.33 05 347 LUAD 7 514 053 14.07 05 347 LUAD 7 501 002 0.00 05 347 LUAD 7 501 002 0.00 05 347 LUAD 7 501 002 0.00 05 347 LUAD 7 501 002 0.00 05 347 LUAD 7 501 002 0.00 05 347 LUAD 7 501 002 0.00 05 347 LUAD 7 501 002 0.00 05 348 LUAD 7 501 002 0.00 05 348 LUAD 7 501 002 0.00 05 349 LUAD 7 501 002 0.00 05 340 LUAD 7 501 001 001 0.00 05 340 LUAD 7 501 001 001 001 001 001 001 001 001 001	344 LUAD 7 514 653 11.33 00 5.43 00 6LUB UNIF HV 0	344 LUAD 7 514 053 11.33 00 65.00 00 5.33 00 65.00 00 5.33 00 65.00 00 5.33 00 65.00 00 5.33 00 65.00 00 5.33 00 65.00 00 65.00 00 5.33 00 65.00 00	345 LUAD 7 514 053 11.33 00 5.53 00 6.00 00 6.		343 LUAD 7 514 053 11.33 00 5.33 00 6.10 UNIF MY 0	345 LUAD 7 514 553 11.53 00 5.53 00 6LUA UNIF MY 0 5.55 00 00 5.53 00 6LUA UNIF MY 0 6LUA UNIF M	345 LUAD 7 514 053 8.00 00 5.43 00 6LUB UNIF MY 0 345 LUAD 7 514 053 11.33 05 50505050 345 LUAD 7 514 053 11.33 05 5.33 05 6LUB UNIF MY 0 345 LUAD 7 514 053 11.33 05 50 6LUB UNIF MY 0 345 LUAD 7 514 053 11.33 05 50 6LUB UNIF MY 0 345 LUAD 7 514 053 11.33 05 50 6LUB UNIF MY 0 345 LUAD 7 514 053 12.33 05 6LUB UNIF MY 0 345 LUAU 7 511 001 2.43 04 3.07 02 6LUB UNIF MY 0 345 LUAU 7 511 001 2.43 04 3.07 02 6LUB UNIF MY 0 345 LUAU 7 511 001 5.49 04 3.07 02 6LUB UNIF MY 0 345 LUAU 7 511 001 5.99 05 3.07 02 6LUB UNIF MY 0 345 LUAU 7 512 062 2.31 02 3.07 03 6LUB UNIF MY 0 345 LUAU 7 512 062 2.31 02 3.03 06 6LUB UNIF MY 0 345 LUAU 7 512 062 2.31 02 3.03 06 6LUB UNIF MY 0 345 LUAU 7 512 062 2.31 02 3.03 06 6LUB UNIF MY 0 345 LUAU 7 512 062 2.31 02 3.03 06 6LUB UNIF MY 0 345 LUAU 7 512 062 2.31 02 3.03 06 6LUB UNIF MY 0 345 LUAU 7 512 062 2.31 02 3.03 06 6LUB UNIF MY 0 345 LUAU 7 512 062 2.31 02 3.03 06 6LUB UNIF MY 0 345 LUAU 7 512 062 2.31 02 3.03 06 6LUB UNIF MY 0 346 LUAU 7 512 062 2.31 06 3.03 06 6LUB UNIF MY 0 347 LUAU 7 512 062 2.31 06 3.03 06 6LUB UNIF MY 0 347 LUAU 7 512 062 2.31 06 3.03 06 6LUB UNIF MY 0 347 LUAU 7 512 062 2.31 06 3.03 06 6LUB UNIF MY 0 347 LUAU 7 512 062 2.31 06 3.03 06 6LUB UNIF MY 0 347 LUAU 7 512 062 2.31 06 3.03 06 6LUB UNIF MY 0 347 LUAU 7 512 062 2.31 06 3.03 06 6LUB UNIF MY 0 347 LUAU 7 512 062 2.31 06 3.03 06 6LUB UNIF MY 0 347 LUAU 7 512 062 062 062 062 062 062 062 062 062 06	345 LUAD 7 514 053 11.33 05 5.33 00 6LUB UNIF MY 0 347 LUAD 7 514 053 11.33 05 5.33 05 6LUB UNIF MY 0 347 LUAD 7 514 053 11.33 05 5.33 05 6LUB UNIF MY 0 347 LUAD 7 514 053 11.35 05 5.33 05 6LUB UNIF MY 0 347 LUAD 7 514 053 14.07 05 5.33 05 6LUB UNIF MY 0 347 LUAD 7 514 053 14.07 05 5.33 05 6LUB UNIF MY 0 347 LUAD 7 511 001 2.45 06 3.07 05 6LUB UNIF MY 0 347 LUAD 7 511 001 2.45 06 3.07 05 6LUB UNIF MY 0 347 LUAD 7 511 001 2.45 06 3.07 05 6LUB UNIF MY 0 347 LUAD 7 511 001 2.45 06 3.07 05 6LUB UNIF MY 0 347 LUAD 7 511 001 2.45 06 3.07 05 6LUB UNIF MY 0 347 LUAD 7 511 001 2.45 06 3.07 05 6LUB UNIF MY 0 347 LUAD 7 511 001 2.45 06 3.07 05 6LUB UNIF MY 0 347 LUAD 7 511 001 2.45 06 3.07 05 6LUB UNIF MY 0 347 LUAD 7 511 001 2.45 06 3.07 05 6LUB UNIF MY 0 347 LUAD 7 512 002 2.31 02 5.31 02 6LUB UNIF MY 0 347 LUAD 7 512 002 2.31 02 5.32 02 6LUB UNIF MY 0 347 LUAD 7 512 002 0.37 02 5.44 02 6LUB UNIF MY 0 347 LUAD 7 512 002 0.37 02 6LUB UNIF MY 0 348 LUAD 7 512 002 0.37 02 6LUB UNIF MY 0 349 LUAD 7 512 002 0.37 02 6LUB UNIF MY 0 340 LUAD 7 512 002 0.37 02 6LUB UNIF MY 0 341 LUAD 7 512 002 0.37 02 6LUB UNIF MY 0 341 LUAD 7 512 002 0.37 02 6LUB UNIF MY 0 341 LUAD 7 512 002 0.37 02 6LUB UNIF MY 0 341 LUAD 7 512 002 0.37 02 6LUB UNIF MY 0 341 LUAD 7 512 002 0.37 02 6LUB UNIF MY 0 341 LUAD 7 512 002 0.37 02 6LUB UNIF MY 0 341 LUAD 7 512 002 0.37 02 6LUB UNIF MY 0 341 LUAD 7 512 002 0.37 02 6LUB UNIF MY 0 34 002 0.37 02 6LUB UNIF MY 0 34 002 0.37 02 6LUB UNIF MY 0 34 002 0.37 02 6LUB UNIF MY 0 34 002 0.37 02 6LUB UNIF MY 0 34 002 0.37 02 6LUB UNIF MY 0 34 002 0.37 02 6LUB UNIF MY 0 34 002 0.37 02 6LUB UNIF MY 0 34 002 0.37 02 6LUB UNIF MY 0 34 002 0.37 02 6LUB UNIF MY 0 34 002 0.37 02 6LUB UNIF MY 0 34 002 0.37 02 02 6LUB UNIF MY 0 34 002 0.37 02 02 6LUB UNIF MY 0 34 002 0.37 02 02 02 02 02 02 02 02 02 02 02 02 02	345 LUAD 7 514 053 14.07 00 5.43 00 6.00.05005050500505050505050505	345	345 LUAN 7 514 653 11.33 0.4 5.33 0.6 6LUB UNIF NY 0 5.45 0.5 6LUB UNIF NY 0 5.45 0.5 6LUB UNIF NY 0 6.40 UNIF	344 LUAN	10.00 10.0	344 LUAN 7 514 053 11:33 00 5.33 00 6LUB UNIF NY 0 13.33 00 6LUB UNIF NY 0 13.	100 100	10.00 10.0	10.00 10.0	NO 1 1 1 1 1 1 1 1 1	NO	NO 1 1 1 1 1 1 1 1 1	No. 1	NU. 15. 14 953 11.35 0.9 5.35 0.9 6.0 1.5 5 5 6 5 6 5 6 5 6 5 6 5 6 5 6 5 6 5 6.	No. 1 1	10. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	No. 1 1 1 1 1 1 1 1 1	No. 1 1 1 1 1 1 1 1 1	No. 1 1 1 1 1 1 1 1 1	No. 1 1 1 1 1 1 1 1 1	10 10 10 10 10 10 10 10	No. 1	10. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	10. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.

- MLH 105.0 FEET . ACHH PLAIFURAS . FATIGUE ANALYSIS 20 0 アンマン 9 7 9 9 9 9 Š

STRAC LUTEL DATA

SOCIAL EXCERCIA DISTRIBUI ASSISTAND EXCEPTES (ESCENDIS BERESON BERESON)

the second seconds and seconds

											•																										
103.U PEET	9 9	1 0			* 0					i		ı		7			ļ		1				- ;			i		1						7 × 3	1		i
ANALYGIG & SLW	.055.		SEUS UNIT	UNIF	SECUL UNIT		4120		# # # 200	11.0	>	T N	I II ZO	L I		T LND	F180		1 L I Z O	F ()		200	Z Z		L 120	4170	GLUB UNIF	- I-V	W 120		L L L L L L L L L L L L L L L L L L L	FIND	T .		4140	E I ZO	
PLATFURMS & PATIGUE	4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5		70	3 0	70	**	70	6 0	* \$0	14	9 -	90	27	20	7	20	10	V 3	10		20	12	90	1.0	=	20	0 -	0.2	20	7.0	. 9	10	20	A &	70	10	20
E J	W	3 :	30.05	3	7:	, ,	24	3	7°07	, O	? =	13	Э	∵	2 7	•	3:	•	•	•	. v			3	Ţ	¥.			<u>٠</u>	ָרָיַ יַּ	į	\$	٠.	0 4	. 3	3 :	3 1
	S . C		50	9	300) o	70	20	2	7-	9 3	20	3	20	2	90	0	2 3	S	-	3 3	1.5	/0	7 0	2	0 6	<u> </u>	70	۲٥:	70	0.7	1.	N (0 -	50	* :	3
-	20	0.1	? •	۰	? `	•	-	-:	• •	2	2 3	•	•	:	2	•	٠ د	9 6	3 3	3 .	عادة درو	•	· ^	າ ວ		3 (. י	Ţ	3:	• •	•••	∴.	٠.	9	3	3 3	10.5
	.65.	001806	2 1 2	11 62	20 50 50	20 20	30 05	70 97	20 -17	21 65	2 2 2	23 62	23 65	23 05) •	25 65	62	0 4 0 4 0 4	20 02	ζο ο ;	ر م م م	01 10	21 10	- A	2000	26 70	2 2	20 70	55 70	27 750	22 25	53 70	2 V C	701 001	2	- T	
	15	F 040	- ¦**	3 €	2 :	3 4	Š	3 4 4	5 5	340	• •	3	٥ ١	٠ ١	5 5	342	5		3	3	2 i 2	3	5	3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	3		֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֓֓֓֡֓֓֡֓֡	3	3 (9 9	3	240	٠ ا	4 5	040	o • • • • • • • • • • • • • • • • • • •	
	INE NU.	3 3	549	> :	,					_		• •	-D 1	n -	•			_	-	-	-	•		N N		v.	uγ	•	v	uv	, ~	~	~ •	354	•	•	9 ~

•
_
-
4
۵
_
_
>
_
2
z
-
_
z
4
-
Œ
_
-
n

A N	0	1 0 7	-	-) ~ 	1		1 0 VM		> ;	Ĺ					اح		· >		>	, !;		. >	>		د ا۔		>	> :	> >	ı	>	>	> :			>	>		> >	
-		GEOR UNIF						CLUB UNIF				GEOR UNIF			6100 CN18		## 70 90.45						STOR CALM		MIND 9019								ž	z :			Z	GLOB UNIF			
7	20	90	700	7 40					Λ: •		70	0.0	-4	0.3			4 u	n ~	70	20	603	7 9	,	20	M -	20	50		9 0	^ -	0.2	90	-	~ :	n	70			.	• • •	
7	50	3.		3	. 7.	*	3	•	.	1 =	1	3	3	7	3	7 :	0 T	200		9 : 3 :	.	•	2	•	5				•	•		•	•	•	•		•	•	0.0	• •	
	•	2		1 10		9	90	_ 	9 :	→ ?	3.0	90	-	70	6		9 6	9 0	S	7	3 3) c		50	7 -	20	0.3	_! 	?	9 -	50	50	- 	V :	† -	90	0 3	0	? ~	• 50	3
·	0	9	9 1	3	. 3		7.	7	.	•	2 3	3	3	D	*	Э Б	• ·	9 10	10	•	٠ -	<u>ء</u> ج	•	9°0	30 1 30 3			۲.۵	•	•		9.0	9	•	• •	3	0.0	9.0	10° 51	•	
-	5	3 80	0 K	30	08 80	08 80	UB 80	0 P S O	D 1		3 3	30 93	08 90	00 00	99 99	9))	200	01.0))))) ())	08.40	0) M()		06 80	08 50	000		3 93	37 40	0 P	90	c 6	01100	0110	0110	1001107	0110	
		Y 040			3	X OVE	`	3	× ;		, ,	•	7 040	`	<u> </u>	<u> </u>	4 ×	כנ	3	X 1	י ביב	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	· 3	A 040	Э :	. Y 040	-	7 040	4 7 7 7 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	7 040	- X 040	· 3		X >	י כנ	→	7	اد اد	> X	2	•
	NE NU. 1.	0	-	. ~	3	57	0	~	0 1	, ;	1	2	5.	2	<u>.</u> ک	ا ج	- 1 n 1) Jr.	<u>ت</u>	- î	7	1 c	, Ç	ę	<u> </u>	: • • •	7.0	7	?;	, r	75	70	11	10 C	> > 1:	1 10	4 C	33	74 T	30	1 ~ K

	ı	UATE 10/05/76						•						•																											
		05.0 FEET	•	:	- 1		• -	!				ŀ)	> 0	0	0	0	0 :) Q	0	Э,	•	,)	V N	3	3	· ၁	0 (.	,	•))	, ,	•	اح	9 :	,	0
	 	HLW 1	5.	*	3	> > 1 1	. 1	3	3 3		*		> : # :	> 1 2 1	3	7	3	3	> 1 3 1	***	* *	3) ;	*	*	> > *	*	3 X	*	> 1 B 1	3	. 3	3	> 2 \$ 1	· >	3	*	3	> >		7
		TIGUE ANALYSIS .	5050.	FED 8019			SLOB UNIF	2	3 NO 30 00 00 00 00 00 00 00 00 00 00 00 00	Z	3				2		2	7	6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			2		שלים מאלע	SLIB UNIF			#120 BCJ5	i	7 7	64.00 UNIT		77		7 7	GLUB UNIF	2	2	GLOB URIT		120
:	z 	PLAITCRAG . FAT			20		2 0		- 6		~								37 T				7 0			•	1	. 20		№				~	→	20		-	~ ~	•	-
•	5 7	- ACRR		•	•	• •		•	5 C	• •	9		2	u 1	7	7	40.	3	?			3	2 1 T T	4	~		•	 	2.	2.95	2 4	5.5	. 66		9		45.	2.04	957.7		15.8
		NAVY	7 5			~ ~	70	- ·	· ·	١ ~	0.2		2 4	N N	1 3	20	4	~	***	100	_	-	3 -				-		-	7.	- 20 - 20			2 -	• ~	0.2			N 1	-	
				20	•	9) ·			-	•	? :		2	3	3	•	7 3		3	÷.	•	3		W. B. W.	. 85	• •	X	1.	4 3	3	7	•		Š	15		<u>د</u> د	• •	٠ د
			.05	00160	3100		5	30160		20162	06190	٠:	<u>.</u>			50 71	14 55	50 11	514 653		99 70	11 00		11 50	12 66	612 562 612 562	12 60	2 20	13 60	13 90	20 40	2 20	42 7U	25 25 2	0 / V V	22 70	22 70	5 5 5	2 -	5.5	39 40
				5	3	9	340	4	つ :) A	340	5	3 :	3 2	, ,	כי	340	240	5 •		240) 4 4 7 2	3	9		30	3 3	3 4 5	3	3 3	3	ว็) ;	5 5) 4 0	3	3	55	3	ร้
'			NE NO. 1	. r.). 0.1		. ~				98	ج	. د د د	• •			05 L	٠.	٠ . د د	ב ה	10 L	1	<u> </u>	1 2 1			100	د د	21 L	٦. ۲.	7 7	25 L	ره . د	∵ . ∵ .) .	31	52 L	25 54 F	55 L	56 L

UNIF CNIF A I NO GLUB UNIF UN IF 7 T P 1770 FIND P 1 5 T NO PIND F 4**1**70 UNIF UN I F #**T** Z O UN IF ANALYBIS 6108 6108 6108 6108 9079 FATIGUE . ACAR PLATFURMS 7.30 16.72-33.44-10.72 35.44 14.87 000 0.72 0.00 0.00 0000 0.00 00.0 909 407 30.5 903 しているい しるい LUAU LUAU している 1000 いすいし 1.040 しるひし 2407 しゅいし 2477 1000 しゅつし いるいし Ş LINE

LANCON REPORTED FOR CONTRACT CONTRACTOR SERVICES CONTRACTOR CONTRACTOR RECORDS

					1 1			•													·													
Lw 105.0 FEET 7 8	2 O AI	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	9		ې د		э:	u ~))	~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~		· >	9	V 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	э э		V 0 > 1	>	э:	2 O A		0 IO	ָ כ	7 C C	> >	> :	V 0		3	> :	V N) >	3 :	V 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
FATIGUE ANALYBIS - ML 5 6 6 7		GLUB UNIF	- 1	7 7 7 7 7 7 7		2 2		6L08 UNIF	- :					170 0019 1019			6L08 UNIF		64.00 UNITE		#Two #019			6L08 UNIF	1		ATAO GOLO	SEUB UNIF						4170 GC18
CAR PLAIFURM • F	-6			•		• •	· ·	•		(•				00		0 0		3					•			07			
40	11 5.0			~ 3	2.	• •	2	• •	5.	·		3.		1	7	3.	•••	5	* o			• •	3	 	1	* 3				→ 0		-	· ·	
25.0	0000	2 3	3	2 2	3 :		3 6	• •	. 55	•	3 6	3	55.	ا د د	2	00	00.	Ţ	24.		9 4	7	. 42	200	ું	3 :	9 4		34.	3.0	2 3	5	4.	. i
1 1	625	663 65	663.65	060 070 060 070	46 659	C0 070	56 956	051 70	651 70	051 70	0.00	656 70	050 70	0.00	653 70	653 70	07 850	655 70	0.2.2.40	701	701 30	70.10/	701 80	20 40 7 10 10 10 10 10 10 10 10 10 10 10 10 10	705 80	08 506	20 407	705 80	705 40	70 8 BC	00 X 00 X	000/	706 80	200
NU. 1,5,	7 LUAD 7		LUAU	1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	5.	100	٠ • •	4 C C A	40.1 . ∪	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	5 LUAU	u LUAU	0 4 €		3	.	ר כ ניני	LUAU	ا A ل	L L L L L L L L L L) - - - -	LOAU	ن السال	ר ר כְּ כְּ	LUAU	U (0 €)		L 0 A U	LUAU	Q		1 - LUAÜ	2 LUAU	

				i i	! !			
				•	 Z Z Z	4 H G H D & Z		,
		e. o	> A Z	Y - ACHH	PLATFURMS . F	FATIGUE ANALYSIS -	MLM 105.0 FEET	UATE 10/05/76
LINE NU. 1	1 1	5 5	m o	3 4	7. 2.	5 6 6 7	7 8	
1040	96 90	16.92	3 0	44.0	50	SLOB UNIF	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
756 LUAU A	106 109	000	20		20		N 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
רטיי טיי		9 0	20	10,01	0.2	GLUB UNIF	7 O A	
10AU	~ 0	5	3 3	5	100		5	
֡֓֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	7	1,63	5 6	5	0.3			
LUAU.	9 5	000	20	5	9.5			
7 0 1 0 1	7		<u></u>		; ~	7 7 2 2 3 3	9 0	
רטאָס.		9	2		0.2	2	0	
1 0 4 0 5	3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	• •	3 ~	0 0	5 0	2 2	.	•
1.040	808 908	9	30		20	GLUB UNIF	3	
1040	~ 2	- ·	3 6	10.01	?) C	610d UNITE	3 5	
	3 6	0	2	5 5	04	77	 	
10 A U	800 908	0.00	~ ?		→ (•	
<u>د</u> (0 0	0 0	3	-	70	2 2	9	
LUAU	Ş	0.61	-	5		120	•	
- 	9 4	. 6	20	20.5	20	6100 0419	0	
2 2	9 9	1.03) ~		2	֡֝֞֜֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֓֓֓֓֡֓֓֓֡	> >	
L. 0 & U	3	0	0	9	0.2	3	د •	
LUAU.	10	00.0	60	5		77	Э:	
			u *	10.01	- P	6000 UNITE)	
LUAU	77	\$ 0	-	2		CNI	0	
U 4 U	5	1.63	5 0	20.	5 0	N .	0	
 - - - -	~ ~	3 3	200		100	20 20 20 20 20 20 20 20 20 20 20 20 20 2	ء ء	
LUAU	3.5		, -	5	g	2 2	•	
LUAU	031	0.61	20	0	2.0	3	9	
71 LUA	150	21.03	→ 3		~ €	2	0 :	
75 5050	7 7	000	7	2	,	1 NO PO15	o	
LOAD	25	3	50	10	0.2	2	9	
775 LUAU X	4001000	. c . c	~ }	5 9	- 0	SEUG ON FR	O O O	
- C.A.C.	00100	1.03	*	α' α	,	GLUB UNIF	> >	
٠. د د	00190	1.03	9.0	•	0.2	SECIO UNIE		
1000	7	-		1	W C	STAIL ME 15		
5 5	513 651	3.71	. 4	4.15	7 -			
L U	13 65	3		_	90	GLUB UNIF	_ [
4 0.	6	3 '		۲.	13			

THE PROPERTY AND DESCRIPTION OF THE PARTY OF

(:::

													•																	}												
FEET																																	•						1			
195.0 F	800		-		 .	-			1	~	7	⊸ . ⊃ :	→ •	- - -	• -		7 0	1 0	-	 -	- -	0	1 0	0		 	7 3	7 0	3	-, -, :	~ - > =			1 0	~	 .	- - - -	•	·	-	 .	 -
ML*	7	3	> 3	3	> ; I I	3	`.*	*	3	>	¥ .	> : # :	. 3	2	3	* *	*	> *	*	> 2 3 3	> > k	3	>	> : 	> > 1 3	?	3	*	3	> : 4	>) E 1	*	*	2	*	> : ¥ :	2 3	3	3	2	> ;	3
E ANALYSIS .	050.	ł	- 1	GLUB UNIF		,				GLUS UNIF						GLUB UVIF			פרווף חייוב	31vn a015	6108 Unit		91.0 9019						- 1			GLIIB UNIT		GLUB UNIF	3		פרום ואוני	2	3	2		
HS - FATIGUE	5 5																																									
PLATFUR	5	12			D 7		1.5	2 0	- -	N		 -	• 3		9		20	;	0/	ج -	22		S (3 -	٠ <i>ا</i>	9	-	1	9 3	1 9	9 6	50	90	2		o 0	<u> </u>	. 20	90		٠	-
ACHE	3	4.76	7.	3 :		. 3	•	000	2	?	•	5 5	•	• >	3		`.	יס	~ '	1 / 0 / 4	• •		3 ° 0 ° 3	• :	• 3	• •	•	3	3 (.	2 7	00.7	•	4.04	?	, (5.3	2	3	3	~: `	•
> < Z	7 2	2	=	2 C	• •	200	<u>.</u>	2 0		y .	- - 				70		0	→ ;	2		7.	-				5 5	-	7 0	١	3 4	80	So	07	=	- (0 =	»	9	30		0 -	-
o •	2 2	13,24			7.17	Ā	۲.۶	э.	7	•	•	2 5	, ,	3	•	0	0	.	3		•	•	•	ء ' <u>ء</u>		, ,	2	٠,	•) :	9	3	3	3	3,	2 =	2	2	80.0	2	٠,	- 3
	1 1	•	3	7 -		7 7 7	7	د 	2 . c	0 ·				11 01	2	12 71		00 10	מ'ק מ'מ	2 - -	: =	-	_:	- -	: -	111 661	= :	7	V 1	v 1	2	2	13	S	٠.			15 30	15 00	13 00	• • 	70
		>	ر در که در ک			A UAU	- 040	٠ ٢	~ ·	4 : 4 : 4 : 5 : 5 : 5 : 5 : 5 : 5 : 5 :	! • •	٠ <	7 790	- 7 040	- OAU	7 040	٠ د	7	-		140 4	7 040	X - 140	7 040	1 Y O Y O	5	7 040	4 : 7 : 4		< >	- ×	> 0	A 340	7 . O ₹0	7 040	< > 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	- 7 040	X 040	AC 4	7 7	V V 240	- - -
	INE NO. 1	725 6	د د	ے د م		د . د	_	7	5 × ×) _	· ~		ر ،	30	ر	. ب	. د	۔، د ا	ם ר				در د ا ا	. ~	613 L	. د	. د	۔ ۔ ۔			<u>ب.</u> د		ب س	J .	2	; ₽	27 L	. د) -) - (

Secretary Branch Company (1) And the company of the

T 10/65/76						•					•																		•									
# 105.0 PEET	50		2 2				. >			2 2		1			1	- O -> H	- 1		00	1		2 2	1 0 7	- 1		0 >	>		N 0 1		> :				7 ·		_	
TIGUE ANALYSIS - ML	5	# RAD 19	,	7			Ž	2	# NO 10010	+		9100 9019						# [ND #6.15	3 3	720	9100 0015	1				3	725	GLOB UNIT	4		-	GLUB UA1F	2	2		4 TAO 90 15	2 2	1.5
LATFURMS - FAT	5 2	~ <u>{</u>	90	10	25	. 6	0.2	00	4 0 0	\$0	\$0	0.2	50	n 0	50	40	0.3	1 6	7 0	70	90	0.3	60	0.0	9 0	0.3	90	5 0	0.50	0.5	- 4	e 50	20	30		3	-	-
- ACMK P	3 4		7.26	~	J.,	y y	יא	~	٦.	1	3	3	3 :	3 4	3	. 3		٠, -	<u>, ~</u>	7	~, `		7	•		•	3	7.51	. ~	~	~; •	•	7.3	0.76	~ `		10.7h	`
U.8. NAV.	5 3	•		5		•					C	٥	6 6	96		Ö			, ,						- 0	, 3		٥- -		0		, ,		3			1	3
	20	13.0	0	3	7.5		14.	14.5	V. 2		3° E	4.5	Y .	15.2	1	14.0	200	o		7.5	2°.	14.0	14.0	3 : 20 :	0 1	14.	3	000	7.5	1.5	٠, ۱		7	3.0	3 3		• •	0.0
			20 70	22 70	o	2 2 2	2	22 70	2 7	30	13 62	13 62	20.51	2 2	30	15 62	55 <u>.</u> 70	27 22	2. 2.	25 M	2 2 2	2.7	25 70	90	2 6	90	24 70	564 701 564 701	24 70	06 20	~ ^ = = =		24 70	1 7 c)	? ? \	. ~	1 70
	15	5 :	LUAU Y	5	3 :	. 4	3		LUAU 2	- - - - - - - - - - - - - - - - - - -	340	5 ,	٠.		3	2	LUAU A	3 4	LUAU A		LOBU Z	3 4	340	3	1040	0 4 0	×	LUAU .	340	` 3	3 :	LO 4 0	UAU.				7 0401	7
	Int Nu.	3 4	200	3.7	10 J		_ 	``.	7 :	1	•	-	D 2			25	\$ 5	r r	ຳ	•	s s	ס י	Ð	•	Dε	•	·	~ 10 0 0 0 10	C	•	- ·	٠ ٢	•	-	-	• •	. ~	×

	4 –
	4
	٥
ż	⊢ ⊃
•	3
	7
	z
	-
	Z
	•
	Œ
	-
	97

EXERCIT CONCORD TO SOCIONAL SOCIONO CON CONCORD CONCORD

WERE THEORY SANDOWS NASSESS FROM WELLING

		•										•																													
MLM 105.0 FEET		0 > 3	- (į.									T 0 A	ı			ł					;	~ · · · · · · · · · · · · · · · · · · ·	Į.	0 > 3								1			١,		- 3	T > 1
FATIGUE ANALYSIS . N	5.000.000	GLUB UNIF	E CONTRACTOR OF THE CONTRACTOR			1		GLUB UNIT		LIND DOTES					SLUG UNIF					FIND BOUND			ב ב ב	3	8100 PO 10	5,3	GLUB UNIF			# TNO 9015	3		Z	FLUB UNIF	2 2	3	4 NO 9019		2		GLUB UNIF
PLAIPEAN O	4 4 5 0 0 0 0 0 0 0 0 0 0 0		20					20	:	3 4	20	70	03	70	5 0	03	y -	• 6	3		0.5		÷ 5	-	 - 5	0.5	-	0.2	7	•	50	• •		•	50	!	7 0	-	•	70	-
4 ACRR		~	7.0	- ~	~	~	~	~	``		_		7.0	7.0	1:0	7.0		. ^	~	1.9	. 0	•	. ~	~	16.72	. ~	7.0	7:0	•		0.7	ر د د ر		~	٤.٧	7.7	0 1 V 1	2	2	۵.۶	2.
	7 0	5 0	0	•		90		9	→ ;	9 .0	20	3	0.4	2 0	3 0	03	y -	• 5	-	-	9	 .	, t	-	- ?	30	-	3	1 -	9	60	5 0	•	-	0.2		v -	•		70	
•	50	3	910		3	•	?	9	2:	2 3		-	6.7	~	3	. t	7 -	2 9		`:	7:	•		7	000	•	6.7	6.72	`. *		3.4	<u>ء</u> :	• •		3	٦.	• ·	• =	3	•	•
	5	_	~ ~		_	_	_	•	~ ~			-	_	_	_	_	~ ~		• •	_	-	~ .	100		M :	• •	•	•		• •	~	~ •	• •	•	_	•	3	•		0	_
	- 3		3 S	, ,	3	3	2	>	> :)	, ,	•	3	Э.	3	3 :	3	, ,	. 3	Э	9	> :	2	9	706	2 2	700	2	ာ :	, 3	. >	3 3	, ,	• •	3	э.	ə :	, ,	-	Э,	\rightarrow
	5.		-			!	~			< >	_	*			× :		y ×		1 "				(-		< >		×	- 1	-	· >				_	× '				7	-	-
		3		5 5	3	U 4 ∪ J	3	5	5 5	5 5	4	5	5	5	5	5 1	5 5	5	5	5	5	5 3	5 5	5	LOAU	ס כ	5	5.	5	5	3) . () ()	, ל	3	5	5		5	3	3	1 4 2
	INE NU.	5) 8	O E	~	10 E	>	2	ب د د		3	↑	9	~	10 (3° :)) -	• ~	. ~ ·	4	5	۰ د د	. 0	60		. 7	1.5	*	n 4	~	10	- 1	J	v	v	v.	ヽヽ	JV	~	~ ·	~

. GLUB UNIF 47 NO UNIT C Z J TINO といる #1 Z O 1 2 C GLUB UNIF GLUB UNIF **₩** 777 777 777 120 - FATIGUE ANALYSIS I VO ZZO 145 25 3 GLUB UNI <u>ر</u> الم פרווף חנוש 1 2019 1 2019 1 2019 1 2019 1 2019 1 2019 9079 8079 61.08 61.08 2013 2013 3013 9013 9079 9079 9079 9079 2019 ACHR PLATFURNS 22 . N N 9 22222 9.67 4.67 70.7 . X > 4 0.8. ~ M M M O O O 24.25 24.25 2.25 2.25 2.00 2.00 33333 20200 406 901100 40 51002 LINE NU. 3... S... U. 2407 LUAU LUAU 1000 1040 LUAU LUAU LUAL LUAU しるり こくこう しること しょりつ

•
-
-
_
•
_
٥
-
3
_
Q.
•
_
z
-
z
_
•
-
_
Œ
-
8

(1)	10/05/76				,						•																						
	PAGE UATE	1	-		1							1	1					~4 w4	1					• ••		• •						~ ~	
	10%		>>	.	0 0	> >	- >))) ! !	اح .	> 0 > 2 > 3) (· >	>>	اد -	> >	. >))) } !	>	> 0 > > 1 3	>	> >	دأح	>	> 2 2 3	· >	- 1)) > > I I		2 2	- 1		>
	# - 4	.0	GLOB UNIF	GLUB UNIF	GLOB UNIF	GLOB UNIF	3	GLUB UNIF	3		GLID UNIF		GLUB UNIF	FLOU 5015	GLUB UNIF	GLUB UNIT						1700 0019 6100 0018		GLUB UNIT	2		GLUB UNIF	GLOB UNIF					GLUD UNIT
	2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4					1	1				•	 -	• -	0.2	•			w 6 w 4				N 2	50	18	\$0	2 6	10	70	16	\$ &	15	3 T	10
	D AEA		14.07	100	ູ	80.4	• •	9 50 3 5 4 4	3	70°51	? ?		2	2 9	2	200	3		3	2.5 2.5	٠.	::	٦.	4 ~4	27.5	\$.35		5,35 3,45	, w	~ ~		4.35° 8.45°	~;
	> 4 ×	7 3		-		-4 -		- -	-				•	700	,				1	- N	12	2 2	70	: 2	30	· 2		*	11	D 7	٥	- C	17
	0	5 O	14.07	6.15	00.00	2 3	3	7 to 0		000	3	14.07) D)	00.0	0	90°00	00.0	 	00.0	20°0	3.76	77.	1.940	2.67	\$	0000	3,35	5.35 0.00	00.0	00°0 8.85	5.55	3.35 0.00	00.0
		0	9061005	00140	2011	2 2	01100	01100	00110	9 0	00140	4001004	00160	10011002	210	10021003	01100	10041004	Z100	01 00	20 7	7 M	10 1	9 0	9 -		1	~ ~ ~ ~	. W	2 3 2 4	3 :	603 623 606 626	9 :
23		15	LUAU 7	•	2 A 2	. UAU 1	4	> X	5	4 4	3	LOAU 4	2	L UAU 4	5	LOAU *	5	L A D A A A A A A A A A A A A A A A A A	5	5 5	LUAU -	1 0 4 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0	L 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0	55	7 040	5	5	1.040 4 1.040 x	5	LOAU 2	5.	5 5	LUAU T
		Ş	91 6	3	3.5	0 \ 0 \ 0 \			t		-		_		3		_ [1		21				10	<u> </u>	7	7 Y	2	v •	7:

	•
	-
	•
	٥
	_
•	_ _
	2
	2
	_
	_
	Z
	~ Œ
	-
	•

AND DESCRICT SECRECAL PROPERTY DESCRIPTION OF SECRECAL PROPERTY SECRECAL PROPERTY.

WELL STREET, STREET, STREET,

													•																											
	0	0	. 0 >	3 S S S S S S S S S S S S S S S S S S S			1	~ O >I	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7		>			- 0 >3		HV 0 1	_							i		* C > S	_	- 1		 	HA C 1	~ · · · · · · · · · · · · · · · · · · ·			1	i				1 0 >=
	4	***5********	SLUB UNIF	GLOB UNIE					41v0 9049					A STATE OF THE STA					100000000000000000000000000000000000000				71 to 0010		# TWO 9019							STAN ROTS					MIND BOID			GLUB UNIF
		.050.	15	9.7	2 2	17	20	7	27	* **	25	70	.n y	0.0		26	1.5	.	V 2	7 9	14	23	3	24	3 3	25	90	27) 0	. ~	0,	٠ <u>.</u>		9	60	15	M 10			-
•	M	5	~	~ 3	•		3	3	•	•	•	₹.	~ •	일크	•	S	•	Ů١	٦		•	ů.	n s	•	5.55e		s	₹.	# 4		3.	4 :	. 1	• •		4	•		3	
	2		•	9	7 7	2	26) = -	27	70	<u>.</u>	0.0	7	20	13	9 :	2 3	3 0	15	5	* •	2	3 .	2	9	2	* -	2	3	1:	3	9 0	=	20	1 000	15	50	2
ĺ			~	7:	•	3	3	3	ء د	9	2	3	. c	2 3	3	•	Š	ŗ.	3 3	• •	•	•	n a	, ~	C C C C C C C C C C C C C C C C C C C	ŗ	•	3	2 4	3	16.42	.	•	• •	3	3	C . C	` ?	. ~.	3
		5	٥	ø -			_	4	n =	٠-	•	5 653	650 01	92.4	107 10	107 1	102	101	2 2	706	907 90	100	00 / 00 02 / 03	5 703		202 50	55 703	20.		104.1	1001	201	200	5005			C			
		2	→	7		•		7 Y		,	٥	79 7	ŏ i	7	×	٥	×	-	4	4	;		9 4 9 4	-	7	-	7	× ,		. .	X				\ \	_	7	1	1 7	× .
		-	1040	5	1000	5	5			5 5		5	LOAU	5 5	3	5	5	• •		5	5	5		5	7 4 2 4 2 4 2 4 2 4 2	1000	1040	3		10407	5			1.040	5	3	740		LUAU	•
	٠	7 70°	0 2 0	4) 4	١ •1	•	4	030	9 -	٠-	3	3	7 5 6	, ,	3	3	3	9 5		051	950	450	5 C	0,70	7 5 5	0.5	9		2 4 4 5	۵	242	000	•	790	•	•	0.7 %	•	0.75	0/0

TOTAL PROPERTY STATES AND STATES OF THE STAT

													•																												
7 & A	0	E 0 1		4 - 0 0 0 × 1	• • • • • • • • • • • • • • • • • • •	1 0 7		1 0 A)			1		E C 1			ı					ł	~ . > : * :	- 1	00	>		~ ~ ~ > > 1 X		T 0 > 3	- 1			1		- 1			1
2 9 9 5	9	SECTO UNIF				1		GLUB UNIF		1177 go 5	4170 GO 5		GLUB UNIF			61.00 UV.						#120 pc.15				170 G1130		GLUB UNIF						ATAD ACTO	PLOG DOLD				6104 UNIT		
	5	0.1	9	7 2) -	70	90	27	50	<u> </u>		. 0	91	20	٠,	90	~ €	70		0.7	71	V 4	0 1	20	9 3	3	1 4	90	3 1	9 3	0.7	5 0	90	~ ×		_	0.2	0.4	→ J	200	-
		3	J	, 3	• •	. 3		•	•	•	•	• •	10.01		•	•			10.01	•	•	•	20	•	200	•		•	•	•		•	10	9 1	• •		•	9	10.01	١,	7
2 · · · ·	3	==		7 -		50	10	7	9 :	2 4		9	1.5	3	00	7	>	9	-	9	7	20	7	3	9 5		. 6	30	7 1	9 0	3	9 0	0	~ *	9			\$	~ 4) }	
	0	3	3 :			7.	٥,	3	0	ē 4	9	2	2		• •	9	0 4 3 -		0.1	2	• :	2 5	2	Đ	21.63			2	10 1	9	. •	•	3 :	2 1	9 5	•	٠	•	•	• =	٠.
		\$	٠, د	2 2		.0		9		2	• •	3	3	3	3 (•	> 0	. 0	.0	•	0 0	•		; •	400 00 00 00 00 00 00 00 00 00 00 00 00	, ,	` 2	2	23	2 2		2	3 : C :	2 2	20	001	0.1	3 c	9 5	9 0	2
	15	4 040 J	5	2 4 7	LUAU 1	ַ חַאַּט בינאַט	3 40	יישר.		3 :	5	240	740	340	40	.	3 3	5 5	_	5	3 ·	10.00 10.00	740	340	LOAU A	9.0) A U	5 ,	٠ ا	1040	3	5	ر ا ا	5 5	LO10 X	2	5	U 4 U	: c	5 5	5
	E NU.	970		•		Ð	£.	£.	£ 3	Ç (•	3	•	•	700	> 0	0 ~ 7 7	• •	3	001	0 :	5 O C	104	501		, ,	601	~		2 = =	-	~		-	9 1 1 6	v	ν	144	\$? ? ? ? ?	125	126

~1. ~1.								! !													1 1 1 1			! !													
	DATE 10/05/76					•					•																										
	105.0 FEET	7 50	3 O >	9 :	2002	~ · · · · · · · · · · · · · · · · · · ·	W N >>> 3	1	э:	V ~ 0 > 2		9	V 0	,	ł	N 0 0 2 3 1	· -	Э.	3	v nv	9	o	V N 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	9	~ · ·	0	N 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	> > > >	•	W 0 5 1	> > > >) >	> :	u ~ :	>	V ^ = > = = = = = = = = = = = = = = = = =	7 0 7
4 L 4 0	FATIGUE ANALYSIS - HLW	5 6 6 7	SCOB UNITE	1	SLUB UNIF			3	2		20		7 7 5 2			# T	17.0 A019	GLUB UNIF			CNIF			1		1	は T Z つ T つ こ 1	GLUB UNIF	#1 HO	60.00 mm	#170 BCJ9		#1x0 9019	33			
~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	PLATFURMS .	55	3 0 ·		90	7 10	0 3	07	~	-	03	20	3 0	20	70	→ 0	0.2	† 0		3		70	4 4	-			7) H								20	*	70
ø	- ACHE	3 4 5	16,22	370	2.04	•	23	~	00.	200	7.	7.74	•	70.0	20	•	4.65	. 65	3 T		0	2	7.26	45	ָרְילָ קיי	7	•	-	2.	5 .2	7 5	-		10	97	7.31	7.51-
	NAW.	٠,0	9	- 	0 0 0		C 0	8	N	-	60	50	7 3	0 3	ر ر	~ }	50	40	-	y -	·	\$0	t t		~ ?	50	000	50	90	5	* ~	8	3 7	u	70	3	0.5
	3	0.5	16.22	27.0	10.62	3		11	9	5 3	3	0		Ş	Š.	v٦	100	2	9 1	•	5	ے ' •	5.5	.51	10.00	7	000		.31	<u> </u>	70	. 62	0.		7.		2
		05.	4061006		515 651 513 651	15 6	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	14 05	51 00	ν ν υ •υ	90 10	010	0 C C C C C C C C C C C C C C C C C C C	11 66	11 60	200	15 00	13 66	79 10	20 10	22 70	22 70	622 7U3	42 70	100 0000000000000000000000000000000000	05 62	25 70 25 70	65 70	25 70	65.70	2 2 2	45 70	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	9 6	20 00	, , ,	7 7
		15	_	N 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	≺ ≻	4 2 3 4 2	- -	- O40	7 040	7 040	A	7 040		. ×	 - -	× +		► 1 Э	را داد	- -	AU AU	P 0 40	- 0401	7 040	4 × ×	7 0	X > 040	7 040	A UAU		4 ×	1 040	7 040	· -	7 040	< ≻	7 040
))	120	٠ د اح	131			1	~ 1		9	ا ـــا		3	5:	0 ~	9	.	2.1	٠~	_	3 1	000	_	0 >	;	^	-	.	ر ا	• ~	10	> :	. ~	~	174	175

SECONDARY CONTRACTOR DESCRIPTION OF THE PROPERTY OF THE PROPER

HOLE COUNTY BOOKS CONTRACTOR

												•													•																
MLM 105.0 FEET			7 0 AE	_			~ O ^ I	7	V 0	> >	IV C 2	>	0		> <)	9	3	э:	V 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	,	3	0	N 0)	Э	3	_		Э		- 1))	0	N:	ချ်	V \	1 ° ° ° > 1	20 71
FATIGUE ANALYSIS - M	5 6 6 7		GLÜB UNIF			i					1					PINIE CONTRACTOR					1 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1		3			2		פרוסם מודעו		2 2	2	N 0	5		2 2	3	2	2		2 2	
ACMK PLATFURMS . F	5 7 7		0 3	51.		0	.	0		74- 03	2.	د دد			o d			ŝ	•	76- 02		. ~		Q		2	~	~ (vn	-21	72- 03	N.	76.	ŭń	'n	2/		6.5		12 02	
	C			1 7	^		° -	2 :	· ·	9	116	10.	•			10	10	16	1 10.			3	2 10,	.01	10.	10	2 10.	•	* * *		\$ 10.	•	•	• • •	• •	1 10.			2 0	•	1 22.
0.0	5 - 0	7.31-	. 5		.02	•	3	3			5	9	ہ ج د د	2 3		000	0	00	00.	90.0		3	12	6.72	10./2-	7.5	3.44	3	•	0.72	6.7	. 72	. t	7.5	0	3	-00-0	10 S	ŭ,	3.44	٥. د
	05.	3	, _ = ~	7 77	772	- -	~ ' 5	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	, r	. ~	<u>.</u> .	_		, ,		. ~	~	~	7 70	, i		· .	₽	T :	909	: 5	τ :- >	₽: •: •:	7 10	9 10 10 10 10 10 10 10 10 10 10 10 10 10	500	6 S O	10 1 10 1 10 1	0 # 0 # 0 =	3000	UB 80	9	0 i	o c	00 90	01 60
	15	- ·		UAU 4	7 040	7 070	v :	-	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7		ר א השנה	5	اد			2	5	5	¥ .04	5 :	* A D	5	Š	DAU .	LU40 X 7	UAU Y	7 040	313	- ^ - A) A	V 040	3 40	N 0 1	5 :	4 040	LUAU 7 7	5	٠ •		5	UAU T
	INE NU.	1177	221	1130	1147	1162	5411	1106		1167	1146	1134		7011	701	100	1145	1140	1197	9511	007	1201	1202	₹0 ?	1001	1200	1001	1.200 1.200 1.300	1010	1211	1212	-			•	~	~ ′	น า	vv	•	~

						•						•	•																													
105.		~ O A=	٩		•	0	0	N 0 / 3	> <	7 V	40	9	9	0	>	1	ə	3	O > 3	5 5		3	3	اد	V 00	, ,	0	0	V .		,	9			V ^ > C > I	> =) · ⊃	· >	. э	i	0	~ C 23
FATIGUE ANALYSIS - ML			51.00 UNIF				GLUB UNIF			2 2		GEOR UNIF		イアつ		3			0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	# Two mode			77	1		GEOR UNITE				1470 BC 3										1		GLUB UNIF
PLATFURMS -	5	-		• -	•	-			~• •	• -		-			-	-	0.2	20		y -	٠.	-	2 0	-	9		-	~ 4 (.	• •	• ~	-	,		-	• ••	•) -4	•	-	-4	
- ACHR	50	22.70-	•	9 5	7	~	7:7	5 2	• •		1	6.00	6.0	2.80	ż	00.7	4.87	17.87	10.07	10.7	, ,	000	. 67	•	14.07	2	4.67	4.07	*	2 -	7.41	~	24.1	3 :			7	2.23	1,11		1.11	-17
U.S. NAVY	5	٥.	00	• 3	3	0	90.	٥ •	•		4		3	3	•00	0.0	0	0 - 2	87		• •	000	0 -00	00.	.00	. 27	7.	-74-	•	2 2	3	S	200) •		2 2		9	30.	3	=	1.11-
-		803	3 405		806	800	308	400	0 4	2 2	700	305	SO N	808	805	0.5	903	MOD :	903	200	n 0 0	906	401	100		100	901 3	F)		7 7	906	906	400	500	2007 2007	1002	1002	1042	1005	1005	1005 2	۰ د
-	0	96 + 0	2 S	200	38 7 0	25 × 2	2 4	2 7 2			7	40	7 0	7 2) P	2 3	- 4 - 2	⊅ ► `	20,1		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	U 2 80	э ж	30 i	,) £	מים אַ ס	D) ; } - ×)	20 1	ō:	× .	•		2	20	7 90	05 7 0	200	Э
	NE NU. 1.	\$0 L	1227 - 40	2	30 0	31 L	32 L	35 - -	, ,		37 - 1	9	•			, L	, , ,	ا ع	היי) - 1	בי בי			. r	2 . 2 .) t	1255 LU	הא	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7		90	31 L	הל	33		9 9 9) 	90	99	70 1	71 -	72 L

With the second	5	10/05/76																																		
		J F										•																								
		105.0 FEET	0 2		> >	00	1	0	3	ə 0	, э	•	9	9	2))	9	u u = = = = = = = = = = = = = = = = = = =	:	9 9	• ၁	3 (0 0	0	3	> >	o :	o c >!>	> o) 	ə :	~! ~! > >		5 c	داد داد	• •
	4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	ATIGUE ANALYSIS - MLM	50505	MINIO COLO	L I NO	A	1 N	L L 7	HTMD	E E	TINO.	F 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 7 7 7	25	F170	L I N D	UNIL	. u.	L I	4 4 2 2 3 3	1 K	#IZO	4 4 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	UNIF	#120 1120	7 7	LT NO	1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		UNLF	#170		- L		ST NO	
	Z 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	PLAIFURNS . FA	5 2 N		-	~ ~		-94		~	-	 •	0.2	0.5		., •	-		0.7	11			o	25	0 0	50	2:	9 0	3 -	17	5 0	20	11	14	וע	20
	•	NAVY - ACAR P	5 3 4	3 3	1 14.07=			::	F . C .	14.07	13		36.04	2 34.	7	u v	7 C	36.0	1.5	1	4,1	1 4 1		7	~ . ~ .	5 2 2	0.6	3	7	9	0.5	~ ~	7.1	7.1	3.55	1 5.55
		2 .0.0	2 2	3 3	26.15	~ ·	0000	21.11	•	0.00	4.07	2.5	0000	5	5		0 3		÷.	• • • • • • • • • • • • • • • • • • • •	-75,	•	100	3	• •		•00	000	30	0.4	70.	၁ ၁	000	-00	000	•
			0.05	06100	0140	0019	01105	201105	001000	001406	900100	201625	1001100	1002100	1601100	0011001	1004100	1000	0.0	 	90	9.79	909 624	621	523	943	929	979	979	520	020	0 0	626	424	955	653
药			INE NU. 15.	25	77 - 104	1276 LUAU A	3407 34	86 104	401 . 58	34 LUAU	LOAU) ; -	NO LUAU	90 1040	1291 LUAD X	45 LUAU	We LOAU		47 LUA		U 40 J 00	2 :	7 LUAU	UAU LUAU	0 4 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0407 - 10	רטיים.	70	11 1040	12 1040	13 1040	1514 LOAD A	16 1040	17 LOAU	14 1.140	5

BIRD TOPET DATA

(3)		10/05/76																																						
		PAGE							•																															
•			900			- 2	1 0	1 -	• •	0 1	.	- -	3	-	ı,	_		1		. !							0	0:	3	 	1	7 0			.		• •	10	•	•
	_	3	~ 6		> >	> 1	*	3	* 3	7	> :	> > 3 3	3	3	3	> : 3	> ? R 1	3	*	3	> > E E	3	3	> > *	3	>) I I	3	3	S 3	> > : 1	*	>	>) I 3	*	> : I	3	* *	>	>	
	UATA	50 to 50 to				DINO D						20 2			- 1	1 NO 1		77	7 2			3			1	1		770					2 2	3	2			12.5	B UVIF	2
\$	_ _	8× 14×4	100		8019 8019	0.19	079		ב פ פ	9	3	3	9	6,719	3	2013 1013 1013 1013 1013 1013 1013 1013			9	3	9000	9		ה ה ה	9079			80.19		019	(P)	ت و ا					6100	95	8079	-
	2 ~	FATIGUE																																						
	Z Z	2000	=3 (7	,	32	28	#1	25	53	9	₽ :	3 Y	3		80		7 1	g	20		0 7	20	37 :	7 ~	22	50-	20	0 . 0 .	2 3	g	90	7 6	~ ~ 0 -	70	7.		: ~	27	0.2	
	a).	a 2	37 0	:	2 2		9	٥	9		0	- -		0	0	•	> 0		=	-		3	3 3	9 3	7	3 3	2	7 :	7 4	1 7	0	9 6	2 2	2	0 3		7 7	ŧ	3	
			, n		9 9		•	1		0	å.	0 6		•	•	• •			10.	-		17					3	ਤ ੰ	1	, 4	3	3 3	• 1	3 -	3 4	; ;	.	3	3	4
;		2	M 3		8 ±			200	3.	2		- 7				-			90	-12		-	37 f	9 •	24		25	0	17	200	3	9 5	9 -	67		7 7	0	13	22	
			N 0		000			V		2	9	2 5		٠.	2	.	2 3		3	<u>ب</u>	•		00.	• •		• •	, 3	3	•			.	90	, ,	9	•	, ,		7 .	=
			- 5	: ;	651	į.		- 1					1		4		0 4	9	6	7		6	4	0 0	. 6	0 0	•	•	0 4		٥	0 4	0 6	9	\$	0 4	•	8	8	2
			- 5		513	-	•	 -	•	~	-	-	2	2	3	.	٠,	'n	-	~ .	⊸ 0	o	Ĉ i	9 4	10	ē 0	9	 .	-	•	~		-	-			613	0	-	-
100	•		1		LUAU 4	5	5	4 4	LUAU	5	F 0401	5 5	1040	5	3	7 0401	5	5	LUAU T	2 0401		5		1010	י טער	1040 Z	3	5:			5	5		5	5:		5	5	רְיַטְאַטַן יַּ יַיַּטְאָטַן	
			N NO.	1	1422	•	~ '	1460	, ~	\sim	3 4 5 0	7	~	•	ჟ.	0571	. ~	•	3	J :	1645	3	3 :	7 7	277	1 1 2 2	2	1452	n s		s	7 3	~ ~	•		0 0	TEOF	0	•	¢

	~
	_
	⋖
	٥
ì	-
	3
	œ.
	Z
	-
	z
	•
	Œ
	_
	•
	٠,

15. NAVY = ACHR PLAIFURMS = FAIIGUE ANALTSIS = PLAIFURMS = FAIIGUE ANALTSIS = PLAIFURMS = FAIIGUE ANALTSIS = PLAIFURMS = FAIIGUE ANALTSIS = PLAIFURMS = FAIIGUE ANALTSIS = PLAIFURMS = FAIIGUE ANALTSIS = PLAIFURMS = FAIIGUE ANALTSIS = PLAIFURMS = FAIIGUE ANALTSIS = PLAIFURMS = FAIIGUE ANALTSIS = PLAIFURMS = FAIIGUE ANALTSIS = PLAIFURMS = FAIIGUE ANALTSIS = PLAIFURMS = PLAIFU	* * * * * * * * * * * * * * * * * * *	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		A	20 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2			PAGE 1
1,				A	1	ANAL S S S S S S S S S S S S S S S S S S S		
				20000000000000000000000000000000000000	00 00 00 00 00 00 00 00 00 00 00 00 00		• >>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>	
					0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>	
					100 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>	
					1		>>>>>>>>>>	
CLAD							>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>	
				3 C C C C C C C C C C C C C C C C C C C	20 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	l	> > > > > > > > > >	
	######################################				2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>	
CLUE CACE COS CACE CACE CACE CACE CACE COS CACE CAC	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4				100 000 000 000 000 000 000 000 000 000		> > > > > > > > > > > > > > > > > > > >	
1 1 1 1 1 1 1 1 1 1	4 × × × × × × × × × × × × × × × × × × ×				100 000 000 000 000 000 000 000 000 000			
Color Colo	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4				100 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			
Color Colo	W - 1 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2				10000000000000000000000000000000000000			
Color Colo	# 2 4 7 7 7 7 7 7 7 7 7				00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		i : 1	
Court Cour	2	2	00000000000000000000000000000000000000		18 00 00 00 00 00 00 00 00 00 00 00 00 00		1 1	
CLUB	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	2	10000000000000000000000000000000000000		00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		1 1	
CLUE X SUS	4	20 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2022222		0 3 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4		. > > > >	
	MA C C C C C C C C C C C C C C C C C C	03 62 03 62	000000		0 0 3 0 0 3 0 0 0 0 0 0 0 0 0 0 0 0 0 0		. > > > > >	
	2 LCAD 2 S	u3 02	222222		003 7 4 60 60 60 60 60 60 60 60 60 60 60 60 60	4	>>>	
	3	•	22222	1000	03 04 04 06		>>	
		20 50	2200	101	04 04 06 10		> >	
LUAD	1 LUAU K 6 L	03.62	200	1.01	07 04 06 10		> >	
	3 LUAU 4 8	20 20	• •		0.6 0.6 1.0		>	
		אר איני איני	•		10	4 14 1		
	4 _ 1 _ 1	, r , r	=	~	2	- î	> '.	
			٠~				> :	
		2 2	•	_	7 4			
LUAU X 865 706 14.02 04 7.31 04 6600 UNIF XV 625 706 14.02 04 7.31 09 6600 UNIF XV 625 706 14.02 04 7.31 09 6600 UNIF XV 625 706 14.02 04 7.31 09 6600 UNIF XV 625 706 14.02 04 10.12 09 6600 UNIF XV 626 924 10.12 10.12 09 6600 UNIF XV 626 924 10.12 0 10.12 09 6600 UNIF XV 626 701 UNIF XV 626 701 UNIF XV 626 701 UNIF XV 626 701 UNIF XV 626 701 UNIF XV 626 701 UNIF XV 626 701 UNIF XV 626 701 UNIF XV 626 701 UNIF XV 626 701 UNIF XV 626 701 UNIF XV 626 701 UNIF XV 626 701 UNIF XV 626 701 UNIF XV 626 701 UNIF XV 626 701 UNIF XV 626 701 UNIF XV 626 701 UNIF XV 626 701 UNIF XV 702 703 UNIF XV 626 703 UNIF XV 703 103 UNIF XV 703 103 UNIF XV 703 103 UNIF XV 703 103 UNIF X	1 1040 / 6	25.70	. ~		0	ŧ	- 1	
	B LUAU A B	25 70	4	~	* 15 C			-
	9 LUAU 7 6	25 70	3		, L			
LUAU	טֿ בט≱ט ב ֿס	25.70	. 3	7.5	60		 - ->	
\$\text{Lunu } \text{Sup} & \text{Cunu } \text{Sup} & \text{Cunu } \text{Sup} & \text{Cunu } \text{Sup} & \text{Cunu } \text{Sup} & \text{Cunu } \text{Sup} & \text{Cunu } \text{Sup} & \text{Cunu } \text{Sup} & \text{Cunu } \text{Sup} & \text{Cunu } \text{Sup} & \text{Cunu } \text{Sup} & \text{Cunu } \text{Sup} & \text{Cunu } \text{Sup} & \text{Cunu } \text{Sup} & \text{Cunu } \text{Sup} & \text{Cunu } \text{Sup} &	1 LU40 x 5	20 90	٦.	101	10			
Cuan	2 LUAU 1 5	29 40	2	10.1	90			
Cuan Subsect Color Col	5 LUAU 2 5	00 05	э Э	10.1	-		>	
CLUAD X O. C.	S K OVOL S	2 9 90		10.1	? c		>	
	C	96.52	3	2	07		>	
	ביים אחם מיים	70 0 T	: :	7.0				
CLAND & CASA 701 0.000 04 10.47 04 64.00 UNIF NV CLUAD & CASA 701 10.47 14 10.47 15 16 16 16 16 16 16 16 16 16 16 16 16 16		7 F	•) :) :	7			
LUAD Z 702 703 0.00 04 10.47 10 66.00 UNIF NV CLUAD Z 702 703 0.00 09 10.47 10 66.00 UNIF NV CLUAD Z 702 703 0.00 09 10.47 04 66.00 UNIF NV CLUAD Z 702 703 0.00 09 10.70 09 66.00 UNIF NV CLUAD Z 702 703 0.00 09 10.70 09 66.00 UNIF NV CLUAD Z 702 703 0.00 09 10.70 09 66.00 UNIF NV CLUAD Z 702 703 0.00 09 10.70 09 66.00 UNIF NV CLUAD Z 703 703 0.00 09 7.34 02 66.00 UNIF NV CLUAD Z 703 705 0.00 09 7.34 02 66.00 UNIF NV CLUAD Z 703 705 0.00 09 7.34 02 66.00 UNIF NV CLUAD Z 703 705 0.00 09 7.34 02 66.00 UNIF NV CLUAD Z 703 705 0.00 09 7.34 02 66.00 UNIF NV CLUAD Z 703 705 0.00 00 7.34 0.0) (C	6 G		12	- 1	10 74	
LUAD Z DES 701 10.97 15 10.97 11 66108 UNIF NV CLUAD Z DES 701 10.97 10.97 11 66108 UNIF NV CLUAD Z DES 701 10.97 04 66108 UNIF NV CLUAD Z 702 703 0.00 09 10.70 09 66108 UNIF NV CLUAD Z 702 703 0.00 07 10.70 09 66108 UNIF NV CLUAD Z 702 703 0.00 1 10.70 09 66108 UNIF NV CLUAD Z 703 705 0.00 1 10.70 02 66108 UNIF NV CLUAD Z 703 705 0.00 0 7.34 0.00 02 66108 UNIF NV CLUAD Z 703 705 0.00 0 7.34 0.00 02 66108 UNIF NV CLUAD Z 703 705 0.00 0 7.34 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0		70		2 2	37 :			
LUAD & 624 701 10,47= 04 10,47= 04 6608 UNIF NV GLOB UNIF	1 1040 1 6	70 70			.		> :	
3 LUAD 7 701 702 0.00 09 16.75 09 GLUB UNIF NV GLUBU LA 7 702 703 0.00 09 16.75 09 GLUB UNIF NV GLUBU Z 702 703 0.00 09 16.75 09 GLUB UNIF NV GLUBU Z 702 703 0.00 1 16.75 02 GLUB UNIF NV GLUBU Z 702 703 0.00 1 16.75 02 GLUB UNIF NV GLUB UN	2 LUAU 2 6	70 70		2	11	,	- İ:	
LUAD Z 701 702 7,50 11,26 1 1 GC00 UNIF TV GC100 UNIF TV G	5 LUAU 7 7	70		2 2	3 1	3 3		
Color Colo	LUAU 7		2 5	0/07	•			
5 CLAPU Z 702 703 0.000 1 10.700 02 6[15 UNIF E CLAPU Z 702 702 0.000 03 4.340 02 6[15 UNIF E CLAPU Z 703 705 0.000 03 4.340 02 6[15 UNIF E CLAPU Z 703 705 0.380 02 4.340 1		- 0	Ų:	11.60		- 1	- (
LUAU Z 705 705 0.00 05 4.58 02 02 02 02 ELIB UNIF EL ELIAU Z 705 705 9.38 02 4.58 1	LOBU 7 7) \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	9 3	0/.01	> 1			
LUAU Z 705 705 9,380 02 4,580 2	7 0407	2		9/07	7 0		→ · > :	
	LUAU Z 7	2 7 2 7) X	7 7	-		2	
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	· / (14)	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \		7.7	~ .	5	~ · ·	

Telegraph Consider

وجير ا

10/05/76						•					-	•																											
UA1E								-																															
5.0 FEET	30	1 0	3	1 0	0 1	~ •	~ ~		-				. 0	→		 	-		**	3	•	0_1		• •	0 1	- 1 .	9		0 1		• •	1 0	1 0	-	 		1 0		
AL # 10	7	3			- 1			1	>	4			1	> 3	- :			1				i	> > 3 3		1		2 2		- 1							3		> ? # 1	. >
ANALYSIS -	50	GLUB UNIF	SLUB UNIF		GE JA UNIF			20		2 3	2 2	2 2	GLUB UNIF	2 2	2			GLUB UNIF		100 001	200	SLUD DOLF		2 2	115	7	6008 ON F	22	70			NO.	20					GLUB UNIF	2
PLATFURMS - FATIGUE	5 5 7		70	••		3 6		-	20		3	.	10	9	90	9 4	9	90	\$0		13		·	•	1		0.5	% 0	0.5	N	, v	50		60	30			ν :	
- ACAR	W.	6.5	8.75	4.7	4.7			7	2.7	•		7	2.9	~	•	•			~	•	-	7.0	•	``	~	7.0		5	S.			٤.٧	2.7	7	. ~	1.40	1.4	.,	2
× × ×	70		90			. t		-	90	١.			~	.) 1	.			ا م				۱		٦.	1	-	اً د	v -	۰.۰			<u>.</u>				ָ מי	
	2 2	, N.	0000	•	•	၁ ေ	•	~	3	ુ:	2 5	2	2	0	٠ •	•		4.5	3 :	7 0	3	2		``	. 3	7°	3 3 7 3	0))	•	• •) •	.	•	• •	S	3	•	•
	1.5.	706	704	-	-		•			-	-	. ~	. ~	~	_	-	•		-	~ -	•	_	2 -	0	-	0 '	30.0	_	_	·		-	3 :	•	•	-	-	<u> </u>	•
	- 3	50	15	=	3 3	a :	, ^ > >	2	2	\ 3	V 4	3	5		- -	- - -		5	<u>۔</u> ح	- ·	m	S	-n =	7 ~	5	<u>س</u> .	90	9	9	0 1	0	์ร	5 5	v 1	, m	5	5	- - - -	. 1
		5		5	J 40	2 :	5 5	3	345) :	4 >	340	2 4 2	3	3	5 5) 	.5	3		340	, O 4 D	▼ •	7	X 040	٠ ١	֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֡֓֓֓֓֓֡֓֡	3 40	7	5 5	2 2	UAU	3 :		2	040	3	5 5	3
	N. 1	. د. د د		25 L	77.	ر د د د د		7 97	50	00		55 L	34 L	Σ		J -	34.	1 24		2 2	1 3	45	J -		7	2 ; 2 ;	יין אין		34 L	7. L		70 1	7 . 7 .		. ל	35		ν 6 -	7

## ## ## ## ## ## ## ## ## ## ## ## ##	DATE 10/05/76																																							
- A - A - A - A - A - A - A - A - A - A	GUE ANALYSIS - MLW 105.0 FEET	6 6 7 7 8	Z .	A 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	L	AM STAN	> X X X X X X X X X X X X X X X X X X X	117	3	1 0 AR 4740 0019	A# 4140	># (4T%)	A#		L 20	UN15	> : * :	A 3	# N	UNIF HV	A	A 1	3	. H. T. O	AM 4770	6 COS 10 12 12 12 12 12 12 12 12 12 12 12 12 12	* * LTZ	AN PARTY		U. 1. F	V	2	A 3		A3 4770	TINO	V		4170	GLUB UNIF NY 0 1
2 Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z	. NAVY - ACHR PLATFURMS - FATIGUE	3 3 4 4 5 50555.	•	1011	4 22.60	2 22.80 0	0 VV VV	2 14,87	10 1	74.67	0 19.87 0	3 19.67		7 5	19,87	9.67	0 19.0 19.0	2 2	· -	19.67	14.67	2 14.67	29.61	2 19.67- 0	5 19.67 0	0 14.67	5 5	4 19,87 0	7.67. D	27.42	27.4	4.6	77	3 27.41 0	2 27.41 0	2/.4	27.42	2 27.41 0	1 27.41	03 27,42 05
		1 1 2 2	00.0 908 808 7 0	2 6 6 5 6 4 1 1 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	U X 8U2 905 U.O	0 7 802 303		0 X 601 903 0.0	200 100 A 0	001 402 CO. 2010 A. 20	U 7 801 903 19.8	8° 7 301 303 14°8	7 A	06 108 7 0	0 x 803 905 0.0	0 4 803 406 0.0	0		1 803 406 1	U x 805 906 54.7	7.5M 000 H0W X 0	7. 400 400 X 00 X 00 X 00 X 00 X 00 X 00		U & 806 901 0.0	J X 805 901 19.8	2	7. 48 104 008 X 0	44.78 34.78	7.92 100 400 7.00 F.00	0 206 106 7 0	0.0 206 206 10	00.0 208 903		0 1 40F 0 000	0 4 401 404 - 0.0	0.0 404 404 X 0	0.0 406 006		0.0 406 306 7 0	10 Y 404 405 0.00
	<u> </u>	LINE NO. 1.	1509 1	12/1	1572 L	1573 L		1576 6	1/51	1579 1	1550	1551	אינו	1004	1585 L	1586	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	98.5	1540 1	1541 LU	7.51	 	1595	1596 LU	1597 Lu	275	1000	1001		1001	1007	1000	-	1604 -	1010 1	1611	1012		1615 LJ	1017 104

CONTRACTOR CONTRACTOR

ASSIST BONNING TRESSOCIAL SIGNINGS DECORAGE (PARENES DOPENIAL PERSONAL

10/05/76 PAGE DATE U.S. NAVY - ACAR PLATFURMS - FATIGUE ANALYSIS - MLM 105.0 FEET > > > I >>> >>>>>> F I S 20000 20000 20000 20000 E NO 1 N N F120 **■ ?** ₹ O 1 NO FIND ムイマン 71VU F ... 3 i vo 3 120 1 NO ママン 9079 8019 SCOB 00 ~ ~ ~ 0 0 0 03 50 0 80.41 4,07 40.00 # C 3 2 2 3 2 2 0 2 2 0 14.07 4.07 14.08 14.08 0000 9011002 9011002 9011002 9011002 9011002 9051002 9051002 9051002 9061005 9061000 9011000 9011000 9011004 9031002 7001 1000 9051002 4011004 9091906 4011004 081002 00150 LUAU LUAU LUAU LUAU しゅつし 340 1040 0401 1040 2407 1040 100 340 このない 1040 L (A U 1040 707 2407 こるり UAU 2401 J. J. LUAU 1000 1040 3 しるり こるりょ 407 J 4 J しょいし 654 654 654 9 000 474 3 9

BULLIONAL PERSONS SEE FRANCES OF THE

OATA
► ⊃ a z ¬
2 4 2 - 0

(>

									•																											
0 > 3	i	_	-				- :			1		- 1			1	_			- 1		i					i					1		- 1			
			1			2 2	3			3																							- 1			#120 AC19
.07	67	4.07	20.0	20.0	20.00	1 V	2.04	40.7	7 T T T T T T T T T T T T T T T T T T T	50.	.65	90	e 5	Š	-56	0,5	0.0	50.	No.	40	20.	30.) J	.04	3 3	0.4	70.	30.	3 2	20.	70.	.35	.55	. ~	~	÷.
# C7 =	6,15	6.15. 0.00	00	50.	000		00	9 3		7.05	7.85	27.0	100	000	03:		15.	.51	100		20.	7 0		.00	3 5	20	00.	9	200	7 7	770	000	000	.35	. 55	.35.
LUAU & 906100	LUAU Y VUBIOU	UAU & 406100	UAU Y 1002100	UAU 7 1002100	040 4 0001100	UAU A 1004190	UAU Y 1004100	140 x 1002100	UAU 7 1004100	UAU A 301 40	UAU 7 501 40	UAD X 503 40		UAU 7 401 50	UAU X 405 SU	140 X 404 Y 040	UAV K # 008 SU	UP 7 400 50	04.0 4 404.050	O + O + O + O + O + O + O + O + O + O +	UAU X 501 60	04 105 F 040	UAU 7 5045 60	040 2 503 60	040 X 505 60	UAU Z 503 60	UAU X 506 60	UAU 7 508 60		UAU Y 506 60	UAU 4 500 00	24 X 040	0 109 7 040	UAU X 601 6	AU 7 601 6	9 109 7 09
	LUAD & 9061004 14.07 1 14.07 1 600 UNIF	UAU Z 9061004 14,07- 1 14,07- 1 6608 UNIF WY UND A VUGIOU4 28,15 02 14,07 02 6618 UNIF WY UND Y VUGIOU4 28,15 03 14,07 03	040 & 9061004 14,07- 1 14,07- 1 GLUB UNIF MY 040 A 9061004 28,15 04 14,07 02 GLUB UNIF MY 040 Y 9061004 28,15 04 14,07 03 GLUB UNIF MY 040 Y 9061004 28,15- 1 14,07- 03 GLUB UNIF MY 040 Y 9061004 28,15- 1 14,07- 03	040 2 9061004 14,07- 1 14,07- 1 600 02 600 001F MY 0401004 28,15 02 14,07 02 600 001F MY 0401004 28,15- 1 14,07- 1 600 001F MY 001004 28,15- 1 14,07- 1 600 001F MY 001000 03 52,04 03 600 001F MY 0010000 03 12,04 03 600 001F MY 00100000 03 10,00 03 10,00 03 600 001F MY	UAU Z 9001004 14,07* 1 14,07* 1 6608 UNIF NV UAU X 9001004 28,15 05 14,07 03 6608 UNIF NV UAU Z 9001004 26,15* 1 14,07* 1 6608 UNIF NV UAU Z 10011002 0,00 03 52,04 03 6608 UNIF NV UAU Z 10021003 16,02 03 16,02 03 6608 UNIF NV	CAU & 9001000 14,07 1 14,07 1 14,07 1 6600 001 1 14,07 1 14,07 1 6600 001 1 14,07 1 14,07 1 6600 001	CAU & QUESTOUR 14,07 14,07 14,07	UAU Z 900010004 14,07 1 14,07 1 10000 10000 10000 10000	UAD Z 90010004 14,07 1 14,07 1 1000 <t< td=""><td>UAD Z 90000000 14,07 1 UAD Z 9000000 28,15 02 600 001 02 UAD Z 900000 14,07 03 600 001 0</td><td>UAD Z 90001000 14,07 1 UAD Z 400000 14,07 1 UAD Z 14,07 03 6000 UAD Z 14,07 03 6000 UAD Z 1000 03 600 UAD Z 1000 03 600<</td><td>UAD Z 90000000 14,07 1 UAD Z 9000000 28,15 02 14,07 03 6000 UNIF NY UAD Z 900000 23,14,07 03 6000 UNIF NY UAD Z 1001000 03 6000 UNIF NY UAD Z 1001000 03 6000 UNIF NY UAD Z 1001000 03 600 UNIF NY UAD Z 100000 03 600 UNIF NY UAD Z 100000 03 600 UNIF NY UAD Z 100000</td><td>UAD Z 9000000 14,07 1 UAD Z 900000 14,07 03 6000 00 UAD Z 900000 14,07 03 6000 00 00 UAD Z 100000 14,07 03 600 00</td></t<> <td>UAD Z 9000000 14.07 1 UAD Z 9000000 14.07 03 6000 00 UAD Z 9000000 14.07 03 6000 00 00 UAD Z 1000000 03 14.07 03 6000 0</td> <td>UAD Z 9061004 14,07 1 14,07 1 14,07 1 14,07 03 600 UNIF 14,00 03 600 UNIF 14,00 UNIF 14,00<</td> <td>UAD Z 4001000 114,07 1 UAD Z 4001000 28,15 03,14,07 1 UAD Z 4001000 28,15 03,14,07 03 UAD Z 4001000 28,15 03,14,07 03 UAD Z 1001000 03,14,07 03 600 UAD Z 114,07 03 600 03 UAD Z 03,00 03 600 03 UAD Z 000 03 600 03 600 UAD Z 1001000 03 600 03 600 UAD Z 1001000 03 03 600 03 UAD Z 1001000 03 03 600 03 600 UAD Z 1001000 03 03 600 03 600 03 600 UAD Z 100200 03 03 600 03 600 03 600 03 600 03 600 03 600 03 03 600 03 03 03 03 03 <t< td=""><td> 14.07 1 14.07 1 1 1 1 1 1 1 1 1 </td><td> 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 1 1 1 1 1 1 1 1 </td><td> </td><td> 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 1 14.07 1 1 1 1 1 1 1 1 1 </td><td> 14,07</td><td> 14.07</td><td> 14.07</td><td> 14,07 14,07 1 1 1 1 1 1 1 1 1 </td><td> 14 14 15 17 17 18 18 18 18 18 18</td><td> 1</td><td> 14 14 15 15 15 15 15 15</td><td> </td><td> </td><td> 10 10 10 10 10 10 10 10</td><td> 10 10 10 10 10 10 10 10</td><td> </td><td> </td><td> No. 100.00</td><td> </td><td> 1</td></t<></td>	UAD Z 90000000 14,07 1 UAD Z 9000000 28,15 02 600 001 02 UAD Z 900000 14,07 03 600 001 0	UAD Z 90001000 14,07 1 UAD Z 400000 14,07 1 UAD Z 14,07 03 6000 UAD Z 14,07 03 6000 UAD Z 1000 03 600 UAD Z 1000 03 600<	UAD Z 90000000 14,07 1 UAD Z 9000000 28,15 02 14,07 03 6000 UNIF NY UAD Z 900000 23,14,07 03 6000 UNIF NY UAD Z 1001000 03 6000 UNIF NY UAD Z 1001000 03 6000 UNIF NY UAD Z 1001000 03 600 UNIF NY UAD Z 100000 03 600 UNIF NY UAD Z 100000 03 600 UNIF NY UAD Z 100000	UAD Z 9000000 14,07 1 UAD Z 900000 14,07 03 6000 00 UAD Z 900000 14,07 03 6000 00 00 UAD Z 100000 14,07 03 600 00	UAD Z 9000000 14.07 1 UAD Z 9000000 14.07 03 6000 00 UAD Z 9000000 14.07 03 6000 00 00 UAD Z 1000000 03 14.07 03 6000 0	UAD Z 9061004 14,07 1 14,07 1 14,07 1 14,07 03 600 UNIF 14,00 03 600 UNIF 14,00 UNIF 14,00<	UAD Z 4001000 114,07 1 UAD Z 4001000 28,15 03,14,07 1 UAD Z 4001000 28,15 03,14,07 03 UAD Z 4001000 28,15 03,14,07 03 UAD Z 1001000 03,14,07 03 600 UAD Z 114,07 03 600 03 UAD Z 03,00 03 600 03 UAD Z 000 03 600 03 600 UAD Z 1001000 03 600 03 600 UAD Z 1001000 03 03 600 03 UAD Z 1001000 03 03 600 03 600 UAD Z 1001000 03 03 600 03 600 03 600 UAD Z 100200 03 03 600 03 600 03 600 03 600 03 600 03 600 03 03 600 03 03 03 03 03 <t< td=""><td> 14.07 1 14.07 1 1 1 1 1 1 1 1 1 </td><td> 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 1 1 1 1 1 1 1 1 </td><td> </td><td> 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 1 14.07 1 1 1 1 1 1 1 1 1 </td><td> 14,07</td><td> 14.07</td><td> 14.07</td><td> 14,07 14,07 1 1 1 1 1 1 1 1 1 </td><td> 14 14 15 17 17 18 18 18 18 18 18</td><td> 1</td><td> 14 14 15 15 15 15 15 15</td><td> </td><td> </td><td> 10 10 10 10 10 10 10 10</td><td> 10 10 10 10 10 10 10 10</td><td> </td><td> </td><td> No. 100.00</td><td> </td><td> 1</td></t<>	14.07 1 14.07 1 1 1 1 1 1 1 1 1	14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 1 1 1 1 1 1 1 1		14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 14.07 1 1 14.07 1 1 1 1 1 1 1 1 1	14,07	14.07	14.07	14,07 14,07 1 1 1 1 1 1 1 1 1	14 14 15 17 17 18 18 18 18 18 18	1	14 14 15 15 15 15 15 15			10 10 10 10 10 10 10 10	10 10 10 10 10 10 10 10			No. 100.00		1

PAGE UATE - MLH 105.0 FEET 4120 ANALYBIB FATIGUE - ACAR PLATFURDS 2 2 3 3 4 >> < Z e sin e tra e la o tra e de se e la colo en el en el en el en el en el en el en el en el en el en el en el en e China el en el el el el el el el el en el en el en el en el en el en el en el en el en el en el en el en el en .0.0 653 653 653 551 LUAU LUAU LUAU 1040 1040 1040 L 0 & 0 ž. LINE

10/05/76 - ACAR PLATFURMS - FATIGUE ANALYGIS - MLM 105.0 FEET U.S. NAVY よった 40110011 40110001 40110001 40110001 4051003 4051003 3333 1000 2407 しつもい トリタン 1001 LINE

	.			-								
	- :		.05	90	3	4.3	× × × × × × × × × × × × × × × × × × ×	.050.	7	\$		
	5	. 0	8.0	2.5	10				[•••		
1	^ ^ C C	3 3		20	ġ Đ	03		- 1	2 2			
ŏ ö	-	1003	21.63	9	200	0						
•	3 0	33		- 3	> ~	60			2 2			
•	0	00	2	17	9.0	15	-	GLUB UNIF		-		
: ح	9	5	3	5	9.0	70						!
	9 4	3 :	2	> 4	,	2 .		6LOB UNIT	> :	⊶ .		
	2 0	5	ý Y	n 7	4 7	7 0			> >			
z	_		•		•			,	i	ł		
.	<u>~</u> :	150	٠,	9 :	> 60°	90			> : E	N (•	
ا ا	_	Λ.		3	ç .				> :	2		
		Λ.		o :	Ŝ	, c			> : * :	~ 1		
	-	n 1	•	<u> </u>	, :	•				v 1		
		D (•	ا			2	9		
		2 4		•		•				-		
	•	•		9		0						
	۵	ø	Ċ	0.5	2.				>	_		
.	Δ	Ð	90.	\$	17.	0	_			-		
,	Δ.	e.	5	20	7.					_		
	D -	D 4	200	, ,		> 0			> > E 1			
. >-			000	0	, 0 . C	A. 6	_		_	4 ~		
l	-	0	.17	-	.0.			Į.	i	1		
	-	٥	.17	0 3	5	•				2		
- 1	-	ε	75.	0	6/6	0			- 1	- 1		
	~4 '	£:	~.	<u>ب</u>	`.	0					•	
< >	~ ~	o :) c	→	5	ć		# NO 9019		N 6		
	4 1	o :	2 7	5	'n) (
	200	> =		9		0 ~		61.00 0045 51.00 00 0045	> >			
· >-	· N	. ~		0	. 7							
_ 7	~	\rightarrow	S		45				ı			
	~	=	Ž	03	25	0	_	GLUB UNIF	> 1			
ĺ	\sim	0	v	Ş	.23	40			0 >#			
	~	3	, .	>	\$5	0						
	າ	2	4 4	9	\$	0						
- 1	~ ∙	Э	, t	3	5	0				. !		
9	~ '	つ :	4	\ \ \ \ \ \	3	9 :						
	₩.	90/	0/ 71	u :	'n.	0 0		z .	- > :	~ .		
i	4 1	> :) (2	֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	> 3 E 3	i		
0 4) (•	D *	֝֞֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֓֓֓֡֓֓֓֡֓֡	7		2 :				
	> :	v	0	1 •	- 20.1	1 0	_			-		
	<u>-</u>	v	• •	3	è :	3		2	_ _':			Î
	v	Э .	• ·	0	?	9	_		> *	u (
Đ	٦	:			•							

- ACHR PLATFURMS - FATIGUE ANALYBIS - MLH 105.0 FEET GLUB UNIF GLUB UNIF GLUB UNIF GLUB UNIF UNIF TINO THE STATE OF THE S SCION CALL 9019 9079 2 6 5 5 U.S. NAVY NATHURENTENANTENENTARE 000 0000 -00.0 -00.0 00000 -00.0 -00.0 -00.0 -00.0 LUAU しいるい Ş 40000

C.S. NAVY = ACMX PLATFURMS = 10.5
NG ကို ကို သိသိသိသိသိ သိသိသိသိသိသိသိသိသိသိသိသိသိ

ACCIDENT PROGRESSION SOSSOON SOSSOON SOSSOON SOSSOON

											•																			•										
 	2071	9	V ~ ~ X	N 2	M 0 &	N 0 A	2 0 X	9	u ~ .	0	1 O VI	2 0 A	W n	• =	N 0 >E	0	1 0 V	3 (V ^ 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		>	-		9	0		9	>		> =	• • • • • • • • • • • • • • • • • • •	2 O Z	_	~ O > I	> =	V (2)	0	•	W 0 2	~ ~ ×
5 6 6 7	GLUB UNIF								2 2		2 2					Š										61.00 books	1			4120 BUND							i			GL!10 U^1F
4 5 5	13	70		13	25	3	97	7	; <u>-</u>	92	9	72	# 3 -	2 2 2	0.4	12	23	= ;	101	10	1.2	200	? -		50	10	0.5	13	23	3 M	12	03		* * C	n 0	17	30	10	0.0	15
3 4	2.70-	7.	7.74	77	ž	•	-	•				•	•					1 . T			£ 3.	3.		. 4	. E &	C C	4	44.	4.5	2 2		3.	4.6	•		2 5	20	10.01	٥.	•
.08	-	3		7	2	•	•	•		-0	-0				0	1 •0) ·		9	11.	2	-0	2											•
55	26 3.		100	53 6.	53 6.	53 2.	3,	o :		5		•		20	50	01 0.	01	• ·		01 18.	0 80	. C.	•		63		03 -10.	90	00	99		9.	16.	90	01 00	010	01 10	01 10	01 21.	7
5	9	900		623	623	663	470	0 7	; <u>-</u>	451	27.0	929	0 4	55.5	653	701	701		102	5	•	202	5 6	5 5	50%	4 7 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	50/	702	•	0 4	9 9	0	9 :	907	G -	2 2	100		5	-
''U. 1		, C	5 CO S	L .	₩ 01	٠ .	VO .		د. د	1 LUA	40.	4 T		, L	1 LUA	401 e	4 L L L L	J.	, C.	\$ C.A	407	س	4 C C	L .	د ح	040 T 040	. ~.	3 LUA	# LOA	7 .	, ~	401 B	401.	٠ - د د د د د د	40.		407	7	40.1	37 LUAU

-
_
4
٥
_
>
o −
Z
-
_
z
~
3
•
⊢

					•						•	•																													
7 6	9	0	• •	0	2	9	3	Э	5 C	> =	> 3	, э	>	% O X	- 1	0	9	ر د)	>	> 3	9	>	3	•	i					1	1 0 A	>	>	> >	- >	. >				~ >×
5 6 6 7	1				2													4							₩ Z O																
2 S	15	7 5	3 -	20	90	13	₽0	ə !			:5	£0	90	7	0.2	80	3 1	0.7	2 6	4 4	1.5	2 0	0 66	13	90			17	7 2	2 - 2 -	92		88	7	4 50	20] == a	1		72	~
50	30	0 5	9	9	.0	.0.	9.		0 4			5	. 8	9	0.01	7.44	7 . C	77.7	7 . T		22	2	42.	.43	, K	2	. u.S	3	<u>ء</u> :	ָר עַר כיי פי	. 15	٦.	.15	4 :	ָ הַ הַ	• •	9	\$2.	2.5		•
7 0	1.7	300	·	2	90	, ,	3	= :	÷ •	3 =	: -	9	60	~	50	10 ·	Λ :	3	9 3	y x	3	0.2	90	1.5	70	17	26	~	9 -	- 1	92	7 0	82								
05	3	0 0	8	. 0	1.63	1.63	1.03	غ •	9 5		8		1.03	1.03	1.03	00.0	3	ن د •	3			99	.23	27	22.	. 5	95.0	0.56	200			•	3 1	7.5	5 Y		3	٠, د	~	.	2
.05	0.3 90	90	06 50	03 90	03 40	06 50	0 t 10	\$ 0 0 0 0 0	0 4		9 9	9 00	06 90	06 00	00 00	0110		0 2 1 0 0	00 15 0			06190	00140	00190	06100 7	c	01 40	01 10	3		03 60	01 20	200	0 % % 0		25 50	2 %	05 50	05 50	0	` -
	-	, 	· -	7	*	~ '	7	< >	- >	; • •	· -	~	ا د.	>	7 7		- : 2	× .	- ·	4 4	· >	7 0	۲ ۲	- '	, ,	,	2	2	5 :	ב כ	3	د	3	۔ د			3	3	٠ د	3 2	
1.	. د.	ر ا	ע ו	د			ه. ا	. د	_ ر	د. (د ،	د	•	4 LO	<u>د</u> ا	. د	. د	ا	۔ د	J		3 101	<u>.</u>	. د			د	ب	۔ د		ı	د	. د	. د		, ,	7	3))
	1505050505050	150050505050505050505005050	150550505055055050505050505	1500	1505505505505505505550555055555055.	1505505050505505505505505550555055.	LUAD Y RUS 903 0.00	LUAD Y RUS 903 0.00	LUAD Y RUS 903 0.00	LUAD Y RUS 903 0.00	LUAD Y RUS 9013 U.00- 17 10.81- 15 GLUB UNIF NY C CLUBU UNIF NY C CLUB UNIF NY C C CLUB UNIF NY C C CLUB UNIF NY C C CLUB UNIF NY C C CLUB UNIF NY C C CLUB UNIF NY C C CLUB UNIF NY C C CLUB UNIF NY C C CLUB UNIF NY C C CLUB UNIF NY C C C C C C C C C C C C C C C C C C	LUAD Y RUS 903 10.00	LUAD Y RUS 903 10.00	1	1	1	1							1										11.5 1 2 2 3 3 4 4 5 5 6 7 7 7 7 7 7 7 7 7	1	1	1	1	1		1

FATIGUE ANALYSIS EAST COAST AIR COMBAT MANEUVERING RANGE OFFSHORE KITTY H. (U) CREST ENGINEERING INC TULSA OK SEP 76 27-771-100 CHES/NAVFAC-FP0-7616 N62477-76-C-0179 F/G 13/13 3/6 AD-A165 651 UNCLASSIFIED NL:



MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-A

STATES STATES STATES STATES STATES STATES STATES STATES STATES STATES STATES

10/05/76 - MLH 105.0 FEET ANALYSIS FATIGUE • ACHR PLATFURMS NU. 1...5....6....5....6....5....6....5.... • **7 Y Y** .8.0 0000 LINE

- MLM 105.0 PEET UN I - FATIGUE ANALYSIS 0....5....0....5....0....5....0....5....0....6...1 - ACHR PLATFURES 000000 U.S. NAVY 200 Š 2185 2150 2150 2150 LINE <u>তাৰ সালাপতি পালাকাৰ লাকাৰ প্ৰচাৰ কাৰণ কাৰণ কাৰণ কাৰণে কাৰণ কাৰণে কাৰণে কাৰণে কাৰণে কাৰণে কাৰণে কাৰণে কৰিছে আছি</u> পুনুষ্ঠি মুখ্যুম্পুট্যুষ্ট্যুষ্ট্ৰী সুষ্ঠাৰী সংগ্ৰহ্মিট্ৰেই কৈ সিংগ্ৰাম্থিক সংগ্ৰাম্থিক সিংগ্ৰাম্থিক স্থায় কৰি

W

								1					
						en	F & X	- - - -	A T A O				
		-)	8.	IVY - ACHR	PLATE	URMS - FATIGUE AL	ANALYSIS - 1	ML# 10	S.O FEET	DATE 10/05/76	
-	\$		0	50	50	3	4 4	5 5 6 00	50.	7	20		
	340	~ ~	M 1	00.0	90	6.0	00	3 3	LOW UNIF	> 2 2 2	-		
	240		05 706		30	55.4	200	5 6	#INO 8019	2 3			
	3 2	آ ،	מות	12,51	5 6	0.0	2	5 G		2 3			·
-	34.		-	0	2.5	10.4	9 5	5 5		> 3 # 1			
ּבֿ נֿ	2 2	. ř			:	10.0	2 2	3 3					· ¦
	3 4 5		# 5	0	9 -	16.7	17	ड इ		> 3 E 3	7 .		
_	3	. ~			0.2	18.7) M	5 5		. 3	1 0		
	340		· ~ ·		0	3	3	3		2	-		
	2 2	د و	v v	07.7	2 -	16.7	9 9	5 G		> > R	- -	•	
_	3	7	· N	0	10	10.7	10	15	7	>			
	2 2		~ =	3 9	0 7	17.0	5	.	COR COLF	> > 1 1	→ -		
	JAU.	7	· .	0	0	18.		5		3	- 0		
	3 3	× ×		000	₽ 3 N N	10.0	17	៤ ថ	LUB UNIT	> > E E	→ -		
	040	7	٠.,	3	0	10.7	90	3 i	1	3	0		
	2 2	< h		10.7	v =			<u>ق</u> و	COB UNIF	> > # #	 	:	
· 🗓 .			. وس	10.7	ĕ:	16.7	20	: ق	•	> 3	3		
د د	ב נ	(-		30.0	 	10.7	2 -	9 3 	LOG CAIF	> > E Z			
. ت	3		. 🛶 ،	33.4	ő	10.7	07	5	١.	3	0		
	2 2	< ×	7 M	• •	- M	10.7	* 5 N		COR CAIR	> > I I	 		
. ت	· 2	<u>, , , , , , , , , , , , , , , , , , , </u>	· •		0	100	03	: وَ	2	>	2		
	2 2	· ř	n •	10.7	Š	10.	7. to	<u>ق</u> ق	LOB UNIF	> > I I	 		
ر تــزا			-	10.7	10	16.7	90	3		3			
	2 2	× ×	~ ~	3.50	5 K	10.7	9 0	3	LOG CALF	> > I I			
_	حاد	1	~	35.4	30	10.7	10	9	3	> 3			
۔ د) Y	× -	•	• •	0 6	50.1	M 4		2 2	> 3 3 3	 .		
	7.040		م ہ		5	50.1	0	5 5	1	> 3	0 0		
	3 :	æ : 	 .	000	Ξ.	24.1	3 (. ड े		>			
_	داد	E 10	- ~	3	7	766.1	2 2	5		> >	-		
-:	.	3 0 :	N	00.0	ŏ .	22.7	10			*	• • • • • • • • • • • • • • • • • • •		
. , -	دا د	2 6	· 1	•	0	- اد	20	ق د ا	CO CALE	> 3	-		
. 1		10		11.40	2	11.40		ٔ ق		· >	4		
۔ د	2 4	* '=	- -	0 3	-	<u>ر</u> م	27	ة و ا		≥ 13			
		•	4						3		-		

S T R A N I N P C C C C C C C C C C C C C C C C C C	1.3. MAY - ACM PLATFURMS - FAILGUE ANALYSIS - MLM 105.0 FEE CLUB UNIF WAY DILL OF THE CLUB UNIF	10.3, MAY - KEMP PLATFORMS - FATIGUE ANNEXES - NLT 103.0 FEE 10.3, MAY - KEMP PLATFORMS - FATIGUE ANNEXES - NLT 103.0 FEE 10.3, MAY - KEMP PLATFORMS - FATIGUE ANNEXES - NLT 103.0 FEE 10.4, MAY - KEMP PLATFORMS - FATIGUE ANNEXES - NLT 103.0 FEE 10.5, MAY - KEMP PLATFORMS - FATIGUE ANNEXES - NLT 103.0 FEE 10.5, MAY - KEMP PLATFORMS - FATIGUE ANNEXES - NLT 103.0 FEE 10.5, MAY - KEMP PLATFORMS - FATIGUE ANNEXES - NLT 103.0 FEE 10.5, MAY - KEMP PLATFORMS - NLT 1	PAGE 87	-											•														•					•									
0.5. NAVY - ACMY PLATFURMS - FATIGUE ANALYSIS - ML 12. 22. 80 13. 22. 80 14. 22. 80 15. 22. 80 16. 22. 80 17. 22. 80 18. 22. 80 19. 22. 80 10	0.5. NAVY - ACRY PLATFURMS - FAITGUE ANALYSIS - R. 5. NAVY - ACRY PLATFURMS - FAITGUE ANALYSIS - R. 5. NAVY - ACRY PLATFURMS - FAITGUE ANALYSIS - R. 5. NAVY - ACRY PLATFURMS - FAITGUE ANALYSIS - R. 6. CLUG UNIT F CLUG	3 T R A N I N P C C C C C C C C C C C C C C C C C C		105.0 FEE			- 1	_			_			1		i	- -	> >	١,	· >	>	> :	> >			- 1		- 1			1		- !		ı,	l		1					
	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	8 T R A N L S. S. S. S. S. S. S. S. S. S. S. S. S.	4	ANALYSIS - ML	50		- 1		,							- :												NO.	2 2						3	2	2 Z	2	2	3			
	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.00	2 	ATFURES .	5 5 55	12	20	~ ?:o				13	10	17	07	0.3	3	0 4	2	50	0.2	70	· ~	50	0.5	700		13	14	* 7	=	3 6	2	70	70	- ;	2.0) - T		60	S.	•	
			•	- ACRE	3	۵.۶	2 1 V 1	3	7.7	D 1	2		0 5	. 2	47	D :	5	0 1			æ,	20, 7	20	D	20	0 3	2		79.0	0 0	20	70.0		4.07	7.42	7.42	/ . 42 / . 42	7.47	1.42	7.4	7.4	7.5	
		**************************************		.0.	2			•	• 0	→ 0		-			•	0				3.	0	6	•	3	0 0		. 0				1	• • •			0		- -		•	0	0	•	

	-
	4
,	=
	3
	2
	2
	0
	•

A CONTRACTOR OF THE STATE OF TH 11 NO 8019 61.18 10.00 ,LUB ,110 2076 1040 3

PAGE DATE FL# 105.0 PEE1 >>>> • ANAL 7818 333 33333 GLUB 610 610 610 610 610 610 610 610 FATIGUE PLAIFURAS 3 3 3 3 3 2 201 3000 651 653 653 653 653 653 651 651 546 551 2000 LCAU CAU LUAU LC & C LUAU LUAU 2458 1.

9	1 0 4				1		10 1	# • • • • • • • • • • • • • • • • • • •				- 1			- 1			ļ				1 0 7	→ · > :		~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~		7 0 1				, , , , , , , , , , , , , , , , , , ,							
•)))))))))))))))))))		0 0		1	7 7 7 X	~ ·))))		7 7 7 8		- 1			- 1			7 3 22)		1 0 AV		N	~ . > ? } !		7 > A		0 >1	7 O A	> :))) > 3	
505		SECON DATE	FLUG UN15					ATRO BOJS				- 1	1780 BOUD					•		41VO 9019			9100 001E		610b U21f		1									GLUB UNIF		
2	36		33	6.5		5		2 4	9	34	56		> 4						0 :		5.5	30	۲ <u>۱</u>	25	4 0	37	52	100	20	75	90	~ ~ ~ ~ ~	90	92	0 1	25	2 2	1
5.00	97.6	7 3	. 7	3	•		3:	0 4 5 5 C 4	. 7		3	3 :	0 4 2 7	. 3	97	4			3 :	3		3:	9 1	200	•		•	9 9	, 50	Ð	•		. 2	10			• •	•
7 3	45	-	36	73	-	7	\$ 1	9 5	2.5		•		* £	2 2	2				.	17) (4)	3	> 1	\$ \$	9 0	7	2	9 9	25	77	2) 1	90	32	300	200		
2 2 2 0	00.0		3	3	7		•	2 5	•	3	÷:	3 1	•	•	9 3	3	3	` Ŧ	.	3 3	?	.	• •	10.01	2. 4	9:1	ے د ا	• •	9	9.0	Ð:4 ⊃ -		•	9.	2 3	20	: :	
-	1 2 2					0 :		0 P	5		っ	2 2	> =	•	, ,		0	2	\$. 20 :	> =	•		- C	2.5	0 0 0 0	901	3	9 6	9	9	o :	9 M 2 C 2 C	9	9 :	\$ 0 0 \$ 0 0		9	
-0	707							7 2 2			3	2	o a	, ,	90	Š	Э	5	ō:	0 5	•				2 D	801	၁ :	2 C	•		ာ် ဒ	6 C	5	Э:	3 5	0 0		
\$	Z 0 A U	7 040	4 040	3		X 1		4 >		א טאט	7 040	7 0 0	4 >	7 240	× 240	7 040	7 040	X 041	P :	4 040	7 340	7 040	4 >	- 4.	> 4 0 4 0 4 0 4	UAU 4	. A .	7 040	A UAU	7 040	7 040	× > 0 V O	7 040	A OAU	- \ 040 040	0 4 0 0 4 0 4 0 4 0	. P	

						•						•																													
05.0 FEET	• 0		0 1	~ . • •	 	-		, 0	-	• •		~	1 0	 	• -	3		0 1				10	- 1	u ^		i		,			1		- 1		. .			2 0	2 0	N 11	
MLH 10	7	*	MX	> : E 1	> > E E	2	>	A S	2 3		3	> : E	3		3	>	>	3	> : *	>) E i	*	*	3	· 1	* *	3	> R	2	. 3		3	> 3	*	> : E :	> > I I	> R	*	> X	>	> > E 1	
•	50.	4140	- 1		1 N N	1	Š				2			1 to 2				Z		2 2 2		UNIF	. !	200		1	200	- 1	2 2				- 1	5	2 2					1 1 N	7
ATIGUE ANALYSI	50	B019	2015			8019	6LUB	6009		9019	90.19	8079	2019		9019	90.19	6100	80 19	8015	80 0	9119	8019			8C-19	9(719	8019	90.19			9079	9079	9019	8013		9(1)9	9079	BU 19	9079		199
TFURMS . FA	5.0																																								
PLATF	30	90	3	? .	- O	15	36	15	D 7	1 19	25	70	3:	- 6	2 0	40	9	2	I	0 - V 1	27	\$0	4	9 -	9	10	;	<u>ر</u>	- 8		10	9	05	5	0 0	0.50	50	8	;	> -	<u> </u>
- ACAR	3.00	Ð	10.01		9	2		20 7	9 4	5	٥.	•	•		5		\$	2	10:	•	2 2	•	1	•		۲.	9	3	2 2	``	7	.74	2.	9	•	7	2	3.	\$		5
	3.0.0	0.7	20	À :	9	17	э М	17)		2	†	2	9 6	25	200	0	2	7	0 1 > -	31	60	6.0	3 2	. 6	3	(50	• •	, ,	90	90	0.7	50	9 7	20	\$0	0	- 1	} -	 -
n.)	2 2		0)))	9	-	1:0	9	•	9 9	2	3.0	0 1	•	000	, ,	· •	9	9 : 3 :	•		•			ŧ	'n	٥	• :	2 3	• •	3	00.	3	Š	j q	90	7.	•	5	9 ×	
	1 1	9	=			77.0	0110	0150		2 2	3	3			3	7	3	7	→		1	=	1	70 71 70 71	1 3	14 65	51 66	51 60		000	01 60	99 29	99 29	9	11 00	12 60	15 60	13.00	22 70)) () ()	20 70
	ζ	!	UAU X	s :	. .	3	2	3 ::			1 040	٠ د	4	7 7 7 7	_		7 040	A UAL	LOAU .	7 040	1	7 040	ن عاد	< > 0 < 0 < 0 < 0 < 0 < 0 < 0 < 0 < 0 <	2	: >	2	a 15	> 2	1 2 4 2	7 040	2	7 040	a :	. .	7 040	2	2	X 040	7 2 2 2	
	N.U. 1.	5	2501_10			ر د	9	را			1 =	. د د د	1	 		_	•	•	> :	~ ^	3 2	3	ر در	o ~	- 30	2		ا ا				. S		2 3 2 3		:	اد ب	1,5	구 . 명한	. 4	1.1.1

Agend Heresona Heresonal branch austrance of the Control Processon and Frances Branch Frances Control Frances

0.5. MAY = ACHR PLAITURNS = FAITURE MART 1915
25 70 1 1 2 2 3 3 4 4 5 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
LOS. NAVY = ACHR PLATFURIS = 1

0/09/76 U.S. NAVY . ACMM PLATFURMS . FATIGUE ANALYSIS . MLM 105.0 FEET 0...5...0...5...0 7177 7177 1770 1125 PIND. AT NO 41 NO IN IN N 1 1 7.VO 7,0 1720 177 T NO # Z > I N 1 2 3 222 1770 N N 2 3 3 3 77 ž GL08 GL08 9019 - 3 N N N N N N N N 0 0 0 0 0 2000 0 2000 0 000 200 -00.0 8 C C C 1040 340 740. LINE NU. 910 050 5640 2013 4192 010

ALAU TUTAL NAXHO

Access to the second of the se

													•																													
	7 6	э	3	0	>	S	> :	> 3	> =) >	>	>	اه اح	o (o :	> :		. >	5	3 .		• • •	· >	o :	V ()	3	Э.	ء اح د اح	> = > >	· >	0	э >	o ¦: > ::	> = > >	, _{>}	: >		3	V N	· >	5
	5556	GLUB UNIF			LIVE BOILS	- 1	MIND 9019									STOR COLO						4100 NOTS						GEOR UNIT	ATAC SCIENT		AINO ROJO		SECH UNIF	4 NO 9019		2 2		FLUB CNIN	2			
	S	-		? 0	? 0			•	-	• • <u>•</u>	70	20		30			3 -	7 ~	· •	60	 4 ,	7 6	.		2 0	~ ·~	0.2	-		• 70	;	0.6	•	4			0.4	-	100		-	20
	5	14.87	õ	. 07	•	ò :		0 1	5		.07	. 87	.07	5			• 3	0 0	7.42	1,42	5.73	` ·	, E	41	3.71	• •	5.1	5.73	~			7.42	.42		1.1	-	1:11	100	3.4	42,25	6.25	2,43
	7 3	-	-	0	3 .	- '. 	y 6	? -	• -	. 50	9	_	V	40	y .		3 3			0.3	•	7			9.		70		-		,	70		م! و			6.0	⊶ .	7	, -		20
	2 2	39,73	30.	•	+ 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0	•	0 6			0.0	•	00.0	60.0		•		7 3	3	3	00.0	10.0	; = ; =	9	•		5.71	13.71-	7			30.	03	.	• •		~	7.0	9 5		00.	•
	. 0 5	7	08 0	07 50	906 K09))) ()				30 40	æ Ç	→ (or :	2 6 2 6 3 6	o :		200	01 60	US 40		ν - •)	01 40	3 :		2	906 306 306	2 0	200	05 20	00 00	35 30		0110	00110	0110	0110		4051002	03100	00150
!	15	3 0	₹	2	5	3) :			• 🤈	340	340	340	٠ •	3 :	• •		כנ	740	J 4 ∪	٠ ا	9	0 4 0	3	5 :		3	٥ . د د	3 :2	5 5	3	240	3) \ \ \ \ \ \	5	340	3 :	240	· -	3	240
ĺ	NE NO. 1	-	D 7 0	7 1 0	.		200	7 1		0,0	150	50		00	700	.			0 0 0	100	0 0)) ()	7.0	219	5 7 5		0/0	7.	0 3	ב ב ב		299	635	t t	1 0	100	000	O :	200	2692	545	720

				9.0	· NAV	- ACMR	PLATF		ATIGUE ANALYSI	•	MLH 105	. O FEET	0 A C	10/02/76	
LINE NU	۱۰ ، ۵۰۰۰	10000	%	2 2 .05.	50	5	5 S	5 5	505	7	7	•			; }
2646	40.1	0	2	٦.		14.07-			90 1 9	PINO	> 3	_			
0 0	1000	200	2 9	0000	-	~	3 2		9015	A I N		~ ~			ļ
2	101	9	• •		. ~	5			8019	. L.		_			
2	LUA	3	100	4. C		2	9		6119	J NO	Į.				;
2:	4 01.	3	202	٥. د د	7 0	.07			9019	UN LF					
2 3			9 5	24.15	→ ?	•				M 14 14 14 14 14 14 14 14 14 14 14 14 14	> : * :	~ 1			
2		7	200	•		> -					1				ł
2	1	>	200			23	50		6019	1 N T N T					
2	104	3	•	2		44.25-			9:19	CNIF					
-	 	3	100		_	6.63	-		9119	13					•
2	101	•	100	•	0.5	14.07-	9		9019	E I NO				•	
2	5	2	O O	00	95	77.	9		8119	UNIF	- 1	- 1			1
7	L O	3	301		70	4.07	70		61.0b	UNIF					
7	10A	3	3	5	70	.01	03		9079	#I NO					
7	LUA	0	100	4.07		4.07	-		CLUM	UNIF					i
7.	10 A	3	100	. 15	70		60		GLUB	4TNO					i
7	2	•	100	9.1	?	4.07	03		8 6 6	S I NO					
7	L. L.	Э	100	9+15	-	3	-		60.08	I NO	- 1	- 1			ļ
2:	Š.	20.	11002	00	4 :	2	S		8075	47 Z				:	
: :	5 :	701	001	3		20°	0		2019	L .					
7 7	- 	0 :		9 3	3	3 3 3 3	200		50.0	2 2 2	> 3 3 3	ŧ			1
: ;	<u></u>	2 0	9 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	•	4 3) i	u 5								
. 5			2 0	•	2) C	* 6		90.36	1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2					
					2) = 1	3			7 2	-	-			1
7	ָר יַ בַּרְי	100	9		-	2			6LUB	. L.) } : 3				
7	1	3	100	, ,	0	2.04	20		6 LUB	- IN					
7.	1. LUA	3	3	. 12	2	7	3		90.09	SALE CALE	>				i
2	1 2	9	8	. 12	7	5.	15		9079	PLNU.	>				
72	L.)	929 9		90	20	07		60.08	4120				•	
7	2	3	Ş	. 71	2	.37	2		90.19	JIN0	i	1			!
72	7	62	65	~	35	~	31		9019	MINO.	O > R				
7.5	2	9	\$. 58	<u>.</u>	. 7.1	15		80 7 9	#INO				!	
7.5	2	9	t t	. 38	26	۲.	26		9(19	FINO					1
7.5	1.0A	9	ů	. 33	90		70		8019	F 120					
2	1 1	4	Ç	ŝ	2	90	2		9079	₩ 1 ×⊃					
73	LUA	V	0		35	9.08	35		9079	UNIF	1				
7.5	201	9	6	3	0	•	9		8019	FIND					
7.5	101	\$	70	3	1.1	7	-		6100	AT NO					
7.5	LUA	65	7.0	٦.	33	07.	31		60.08	CNIF	1				1
7.5	LUA	65	70	3	2	2	16		9119	#1×0					
7.5	د	7 656	902 9		7	7.10-	36		9019	# T 7 0) >	N			
7 4	2	65	70		90	2	S		8019	UNIF	1	i .			
7.4	LUA	•	7	3	D	7.10	17		60.08	JINO.					
7.	LUA	65	3 703	3	24	1	27		61.08	LINO.					
7.4	V 1 1	•	7			•	; 				:				!
	֭֭֭֭֭֭֭֭֭֭֭֭֭֡֝	٦	•	?	2	0 .	S		2 2 2 2 3		> *	~			

THE STATE STATES OF THE STATES

STATE STATES CHARGE

F 2 2 2.1

3

A T A C >=0

			•					•										•			\			
		. 217	20,000		50°00°05	2.0.1	20,000	11.120	20,000		21,248	20,000	10 103	20,000		20.000								
0701744		716			1.580		1.580		1.580	1	21,248			1.580		1.580		5.281 20.000		3,261 20,000		20,000		
		281	.700		007.	1.644	700	056.4	. 700		13,480	00/•	7.4 4.	700	28.721	700		3.281 2.940		3.461	9	075		
	3	9	.430		1.150	4 C	450	959	007.		11,273	208.	15 070		0.40.45	.500		2,418		1.160	•	1.160		
			.270		0 0 0 0 0 0 0 0	2.107	240	4.742	.320		516.6	. 580	100 01		21,066	380		1.718		1.716	_	044		
		.129	.120		110	50	140	19091	. 190	t	990'8	0/2	11.007		17.995	. 270		1,513		1.313	3	000		
	000 000	/017	0.50		9000	1.244	070	3,021	.120		7.634	022	40 714		16.225	.220		. 967		. 467	3	270		
	00000	200	0000	14,00	000	20.00	0.000	34.00	0000	00.83	00000	2000	00.00	0000	102,00	0000	102,10	000.0	136.00	0000	0 :			
	DEPTH (FI) B FUNCE (AZIN) DEFL (IN)	DEFIN (FT) B	(NI)	UEPTH (P.1) B	UEFL (14)	FINCE (KIN)	UEFL (1N)	UEPIG (PI) B		UEPTH (FT) B	UKCE (N/IN)	UEFL (11N)	DEFIX (*1.) B	UEFL (IN)	UEPIN (PI) B			PUNCE (K/IN) DEFL (IN)	DEPTH (PI) B	25	-	DEFL (IN)		



PILE JUINT NO. 1011

(11) = 0.000																												
(**!) = 0.00	3 L x 105 0		. 237	20.000		2.274		5.831		11.120	20.000		21.248	000.02		30.102	20,000		45,155	20,000						; ;		
(11) = 0.000 0.000 (111) = 0.000 (112) 0.000 0.000 (112) 0.000 0.000 0.000 (112) 0.000 0.000 0.020 0.0			.237	1,580		2.274		5.631		11,120	1,580		21.248	1,580		30,102	1.580		45,153	1,580		3.281	60.000		3.281	20,000		
(11) = 0.000 0.000 (111) = 0.000 0.000 (112)			188	100		1,440	1	3.644		0.450	100		15.280	00/*		16.014	00/		28,421	00/		5.641	006*2		3. CA1	200.7		
(11) = 0.000 0.000 (111) = 0.000 0.000 (112)	7		. 109	05 7		1,150		2.445 .450		5.659	007.		11.275	905.		15,970	500		23,954	.500		2,418	1.150		2,414	1.160		
(11)			,155	012.		906.		7 2 5 4 7		4.142	. 520		4.413	0 45.		14,043	946		21,064	280		1.710	064.		1.718	470		
(11)	•		, 129	.120	1	.110		1,001		3.595	140		8.464	012.		11,447	0/2.		17.445	062.		1.515	.140		1,515	140		
	,	20.000	.107	050	1	, 560 0 50		1.244		5.021	120		1.054	• 220		10.718	455.		16,225	,420		190.	\$40.		196.	\$70.		
	I	0000	000°0	0.000	14.00	0000.0	24.00	000000	54.00	0.000	0000	00.00	04.0.0	0.000	94.00	0.000	000.0	104.00	0.000	00000	102.10	0.000	00000	150.00	00000	0.000	400,000	
Ses ors ses ors ses ors ses ors ses ors ses ors ses ors ses ors ses ors ses ors ses ors ses ors ses ors ses or ses		CEFT (12)	CEPTA (*1) H	(-1)	5	:: :::	GFI			\(\frac{1}{2}\)	7.0	1	PURCE (1/1-1)	C : 3	UEPTH (FT) HTT	PURCE (AZIN)	(12)	a (14)	(*1/*)	(+1)	H (1-1)	1175 (1714) ADMIN	7 7	# (14)	(4/17)	1	H (14)	

3 .19295776_

PAGE

PILE JUINT NO. 1012

ではないのは、日本やななななど、自己ないのではない。

U.S. NAVY - ACHR PLATFONMS - FATIGUE ANALYSIS - MLH 105,0 FEET 20,000 20,000 20,000 5.631 30,102 20,000 20,000 20,000 1.580 1.560 11.580 21,248 1,560 3.261 1.580 2.274 3.281 20,000 13.280 16.614 28,421 188 3.644 00/ 3.481 3.481 1.440 3.491 11.273 15.970 23,954 1.180 1.140 2.418 2.895 1.136 . 440 430 5.659 9,913 14.043 21.064 1.718 1.716 1,716 906. 2.347 240 253 9.742 1,513 1,681 11.997 17.495 .011 190 8.468 1.515 1021 3,093 16.223 10.718 .967 20.000 365 1.24¢ 7.634 .967 167 020 3.021 102.00 0000 000 000 0000 00000 00000 00000 0.000 000000 0000 DEPIN (FI) B PUMCE (K/IN) DEFL (IN) PUNCE (N/IN)
UEFL (IN) DEPTH (PT) # PUNCE (H/1N) DEFL (1N) PLHCE (W/IN)
VEPL (IN) PUNCE (N/IN) FUNCE (K/IN) UEPL (IN) #114 (+11 a vince (+/14) a vert (14) CK/IN) UEPTH (F1) # FUNCE (N/IN) FUNCE (N/1N) DEFL (1N) PURCE (K/1N) DEFL (1N) DEPTH (F1) (TN) PUNCE UEPL

(2) 10/05/76 PAGE LUAD CUMDITION NU. 1

CYCLE NU. 1

U.S. NAVY - ACHH PLAY

Participal Commen

Juny 1		しょつようの		AT NUNE INEAK	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	DISPLACEMENTS AT SUPPORTS (IN-KAU)	REGUL ANT DISP DIFFERENCE (IN, KAD) DI	PERCEIENTS PERCENTS PFRENCE	
11000. 11000.	1. 121. 1.	JULNI NO.		SCHPURTS (KIPS)	01745 00000 00000 00000 00000				
	10000. 100000. 10000. 10000. 10000. 10000. 10000. 10000. 10000. 10000. 100000. 10000. 10000. 10000. 10000. 10000. 10000. 10000. 10000. 100000. 10000. 10000. 10000. 10000. 10000. 10000. 10000. 10000. 100000. 10000. 10000. 10000. 10000. 10000. 10000. 10000. 10000. 100000. 10000. 10000. 10000. 10000. 10000. 10000. 10000. 10000. 100000. 100	1010	- A 1	27.0845	100 L 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-,01419			
1 1000 0 0 0000 0 0000 0 0000 0 0000 0 0000		1010	, 	. 3611	00000	95000 -			
0000 0000 0000 0000 0000 0000 0000 0000 0000	10000		·			02000			
	1		• 4	7000 and	10000	•			
10000 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		200		N 7 7 7 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9		•			
10000 100000 100000 100000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 100000 10000 10000 10000 100000 10000 10000 10000 10000 10000 100000 100000 10000	1000 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	;	•		04.640				
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1	1011		5.6140	21.22	.00723			
4 0000 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	101		-6.0428	01302	-,01223			
00000° 00000°	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1011	~	40.3269	4/900	00674			
10000°	10000° 1000° 7557° 6 10000° 1000° 1000° 7557° 6 10000° 1000° 1000° 7557° 6 10000° 1000° 1000° 7557° 6 10000° 1000° 1000° 1000° 7557° 6 10000° 1000° 1000° 100° 7557° 6 10000° 1000° 1000° 100° 7557° 6 10000° 1000° 1000° 100° 7557° 6 10000° 1000° 1000° 100° 7557° 6 10000° 1000° 100° 100° 7557° 6 10000° 1000° 1000° 100° 7557° 6 10000° 1000° 100° 100° 7557° 6 10000° 1000° 1000° 100° 7557° 6 10000° 1000° 100° 100° 100° 7557° 6 10000° 1000° 100° 100° 100° 100° 100°	1011	3	-609.2828	.000	\$0000			
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	10000° 10000° 10000° 10000° 10000° 10000° 10000° 10000° 1000	1101	_	-301,3982	80000	00005			
2	2	1011	•	7547.8	.0000	10000		•	
2	200000	7101	-	0434	47.400	0.440			
012 3 -41 -150 -00000 -012 3 -000000 -012 3 -000000 -012 3 -000000 -012 3 -000000 -012 3 -000000 -012 3 -000000 -012 3 -00000000 -012 3 -0000000 -012 3 -00000000 -012 3 -00000000 -012 3 -00000000 -012 3 -00000000 -012 3 -00000000 -012 3 -00000000 -012 3 -00000000 -012 3 -00000000 -012 3 -00000000 -012 3 -00000000 -012 3 -00000000 -012 3 -000000000 -012 3 -000000000 -012 3 -0000000000 -012 3 -00000000000000000000000000000000000	100000	7101	• •	7000 M	7 4 3 7 6				
5	5 - 561.9430 - 000018 - 00000 0 00000 0 00000 0 00000 0 000000	7101	۰, د	24.0°.		0 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			
5 -255,5883 0 00000 0 4729 0 00001	5.555.584.3 6.0000, 6.4729 6.0000, 6.4729	1		0270 149	* 000	0000			
9,4729	9,4729	7.01	r ur	4429 4500 4429 4500					
		7.57	•	00000000000000000000000000000000000000	90000	N 0000			

PAGE PILE-STRUCTURE
NESULTANT DISPLACEMENTS
DIFFERENCE PERCENT
(IN-RAD) DIFFERENCE 0000 .0005 0000 0000 .0002 0000 .0000 00000 Z . ACHN PLATFORMS . FAILGUE ANALYSIS . MLM 105,0 FLET J • ¥ DISPLACEMENTS AT SUPPORTS W 00000 00000 00000 00000 00000 000643 01188 00000 01153 LINIHADA DISPLACEMENTS AT SUPPUNTS - 02585 00000 1100 0000 00000 00000 00000 •.0000 SIN, KAU) 97000 .02041 STRUCTURE ACTIONS AT NONLINEAR SUPPORTS 1 J z D INIPSE IN-HIPS 1.6255 35.3692 38.5440 -229.0070 -142.7447 8.8891 -5,5698 3.5565 5.9238 194,7521 194,7521 -27,9564 9,7974 -7.4078 Z U.S. NAVY • z « Œ FKEEDUM DEGMEE NUNL INCAN JUINT NU. 22222 LUAD CUNDITION NU. CYCLE NU.

SOCIAL PASSASSINATION AND SECURIOR SECU

のとついしくどばしい しょつむしつの よくばんべいてつとしとくないの

SANDONE AND SERVICE SANDONE STATES SANDON

PAGE PILE STRUCTURE
MESULIANT DISPLACEMENTS
DIFFERENCE PERCENT OIFFERENCE C.S. NAVY - ACAK PLATFUNTS - FAIRCUE ANALYSIS - ALK 105.0 PER DISPLACEMENTS AT SUPPORTS 00035 00000 60000 .0000 (IN, RAU) .01928 00000 00000 -100842 .00471 -,01500 190004 .0000 00000 01503 0000 STRUCTURE DISPLACEMENTS AT SUPPORTS *** 00000 600000 -,01519 INCHAU 47010 00000 -,00844 01200 -.00471 -. 00660 10000 .00001 .00017 .00467 STRUCTURE ACTIONS
AT NUNLINEAR (KIPS, IN-AIVS) 4.5521 -26.2117 160.9160 107.7853 -5.1591 .. 7571 178.5200 27,4916 5.5844 4618.05 -27.6644 -2,5473 -2,2659 -157,3005 -6.6068 -. 1004 SUPPORTS FKEEDUM DEGMEE SUPPURT JUINT NO. 1012 1011 10000 1016 1012 5 LOAD CUNDITION NO.

PILE-STRUCTURE MESULTANT DISPLACEMENTS DIFFERENCE PERCENT -0000 0000 .0000 .0000 (IN, KAD) DIPFEHENCE 40010 ₹000€ -0000 0000 0000 00000 0000 ANALYSIS - MLW 105,0 FEET 1 1 E M A 1 1 U OISPLACEMENTS AT SUPPINTS 00000 .01502 -,00909 00000 00000 (IN, KAD) .01928 60000 ***** ..000010000 0000 ----U.S. NAVY - ACM PLATFUMMS - PAITCUE DISPLACE LATE AT SCRPCATS 000000 000000 000000 00000 - 00 H44 00000 67610 -. 01519 (INTRAU) ..004/1 4 0 0 0 a. -.00860 ¥ STRUCTURE ACTIONS (ガネ! ヒーこ! ・のネ! ヒ) -27 -5409 -174 5299 -2.2676 -4.4854 -27.9921 -157.1762 -65.7315 128.540 188.2112 161.0546 107.8546 AT NUNLINEAN 5.5849 -. 1011 BUTTELIATOR -4. BU7. FREEDUM いとられたれ 1010 200 1011 22222 LUAD CUNUITION NO.

ITEXATI **1** 4 2 -z 9

PAGE DATE REGULIANT DISPLACEMENTS
UNFERENCE PERCENT (IN, MAD)_OIFFERENCE U.S. NAVY . ACHH PLATFORMS . FATIGUE ANALYSIS . MLM 105.0 FEET DISPLACEMENTS AT SUPPORTS 01907 97000 .03627 000298 -,00029 .00017 -.07917 (IN, KAD) .0000 .00057 10000 00027 DISPLACEMENTS
AT SUPPLINTS 000010 05570 000010 .01952 .00028 -.07745 -. 00036 03450 (IN, KAU) 10000 0000 STRUCTURE ACTIONS AT NUNLINEAR (AIPS, LASKIPS) -751.7468 -457.5946 26.3078 4,1732 66,6457 716,2845 10.9868 -18.2455 114.2753 9.0081 -45.4409 -116.4710 660.7744 -123,4424 30,7496 BUFFINATS FHELDUM DEGMEE SUNTEUR I JOINT NO. 1010 2000 1014 LUAD CUMDITIUM MU.
CYCLE NU. 1

PAGE PILE-SIRUCIURE REGULIANT DISPLACEMENTS CIFFERENCE PERCENT 1000 .0000 .0000 (IN, MAD) DIFFERENCE 1000 2100 0000 0000 0000 0000 1 - E R A - L C R U.S. NAVY - ACHN PLATFURMS - FAITGUE ANALYSIS - MLW 105.0 FEET DISPLACEMENTS AT SUPPORTS 03580 00001 03590 000293 .0000 - 00056 -,07820 (IN/HAD) 000059 .00017 00067 00003 DISPLACEMENTS AT SUPPLIFIE -. 07854 -. 90227 - 90070 04589 .01954 -,000056 .0000 (INDIAN) **₹0000**• 82000° \$1000° 0000 00000 ¥ 出た 17 コと 17 とく 17 一の STRUCIONE ACTIONS AT NINLINEAR (BYIN-KIPS) 10.9755 118.5685 114.5695 -748.5696 18,4469 -22,3472 741.4414 -12.1000 9615,000 4.1748 -405.4894 -129.3601 30,9159 SUPPORTS PKEEDUM NUNE INPAR UUTPURT JULYI NU. 2000 2000

BECTERT PROFILE WELTSTER WINNESSE U.S. NAVY - ACMY PLATFORMS - FATIGUE ANALYSIS - MLM 105.0 FEET CYCLE NU. 1

VUNLINEAR	DEGMEE	9 N C	の1800108円	PILE	PILE-STRUCTURE
- ED7700	0.6 ENF 6 0.34	AT NUNLIMEAN SUPPORTS	DIGETACE SERVICE AND DESCRIPTION AND DESCRIPTI	DISPLACEMENTS	AMOULTANT CLODIACENTO
		8)	(IN, KAU)	(IN. HAU)	CINCADO DIFFERENCE
1010	-4	15,4015	.05236	.05119	
1010	~	0000	.00115	67130	
1010	7	-5,2592	89000	88000	
2101	3	-51.2115	.00001	00001	
1010	s	-506.044Z	45000°	.00043	
1010	•	10,0634	.00001	10000	•
1011	-	-7,7412	02472	#5570°•	
1011	~	15.1446	.04154	.04112	
1011	~	5000 601	01137	01137	
1011	ŧ	621,1908		00018	
1017	5	355,7946	00011	00011	
1011	٥	-14,3453	1.0000.	.00001	•
101	-	-6.4731	•.02386	-,02432	
101	~	-13,3465	87570	04210	
1012	-7	03.3640	.01001	.01001	
1012	3	-549,4516	-00010	\$1000°	
1012	∽	152,6299	00011	00011	
1012	٥	-12,7191		10000	

CYCLE NU. 2

-5

PAGE 8 UATE 10/05/76

AVY - ACHA PLATPURMS - FAIICUE ANALYSIS - MLM 105,0 FEET

**************************************	DEGMEE	STACTION ACTIONS	STRUCTURE	PILE	PILE+STRUCTUR	1 1
- CZ 1237	C C C C C C C C C C C C C C C C C C C	AT NUNCTERAL	DIGHTACKITACIO	DISPLACEMENTS	REGULTANT DIGHLACE	1 KE 2 1 W
		(SdIvevi'sdiv)	(INN HAL)	(INTRO)	(IN, MAD) DIFFERENCE	ENCE
1010		15,4495	77150.	,05176		
1010	7	7500	00111	00151	0000	0000
1010	~	-5.2580	82000	99000		
1010	*	-51.4716	00001	- 00001		
1010	ζ,	->04.4125		00003	0000	0000
1010	٥	10,7799	10000	.00001		•
1011		e7.7458	- 02459	02466		
1011	~	15.0642	.04116	04112	0000	0000
101	~	-08.0253	01135	01135		•
1011	7	609.744Z	- 0001B	- 0001B		
1011	^	350.4583	00011	00011	0000	0000
101	٥	-10.2847	.00001	00001		•
1014	-	-6,5121	02373	-,02458		
1014	~	-13.3452	-042b7	04238	0000	20002
1012	~	63,5512	• 01000	01000		
1014	3	-505.6641	61000	61000		
101	^	148.8055	1.00011	-,00011	0000	2000
1016	٥	-12.6716	.00001	00001		

LOAD CONDITION NO.

CONTROL OF THE PROPERTY OF THE

		A TO COMPANY WITH THE PARTY OF	- 1	- 1		10/08/76	
			THURSH OF TAILGUE ANALYBIG	•	ML# 105.0 FEET		
SCS N TO SO S	DEGREE	GINUCTURE ACTIONS	SINUCIUNE	PILE	PILESSIAUCTURE		
120 E 2 T 2 T 2 T 2 T 2 T 2 T 2 T 2 T 2 T 2		A CONTRACTOR		DISPLACEMENTS	HEBULTANT DISPLACEMENTS		
		(Alta, Inen Ipa)	A	DINCEPECATION IN	CINETACO PERCENT		
3 3 3 3	•						-
2121	→ へ	11/20800	P.10H79	22420			
0101	- - - -	9076	4/200.	96500			
0101	1		69000 ·	69000°			<u></u> -
0101	,	/rss*nc2	\$0000	M0000.			
0101		500°0001	02000	00100			
	•	0289.92	£0000 -	• 00005		***	
1101		22.7964	0.1510	76.400			
1011	~	438.9512	1000	95500			<u>-</u>
101	**	207.185	50001				, -
1011	*			00240			<u>-</u> -
1101	2	4001.095	* F000 *	2/000			- <u>-</u> -
1011	٥	30,000	# 60000 •	17000			<u>-</u>
			00000	90000	•		_~_
7101	-	19,6417	.07642	10116			~~
7101	~	36,3472	18651				N
1014	•	-276,5864		2001			~
1014	7	1235,0340	0000	77000			۸.
1016	'n	-230.00to	85000	43000			Ņ.,
1016	٥	82.8500	60000	00000			À.
							~ _^
							i.
							. *
							. '
							: 4
				•			*
							R
							×
							£ 2
						1	2
							8
					1	•	= 3
							, ,
							- 3
	٠						\$ 5
							\$
							2
					•		٤ :
							. 2
		!				•	43
							3 1
						•	8 X
							5

- x 0 A 2 2 3 ************

with the property in the second of the property of the propert

1 TERATION

10/05/76 PAGE

U.S. NAVY - ACHN PLATFUAMS - FAITGUE AVALTOSS - MLM 105,0 FEET

CYCLE NO. 2

PILE-STRUCTURE RESOLTANT DISPLACEMENTS OIFFEMENCE PERCENT .0322 .0234 5080 .0277 (IN, MAD) DIFFERENCE0041 6970. 0000 9700 0000 0000 PILE DISPLACE 4E418 AT SUPPURTS 000035 .08860 00000 08503 .00058 .04505 60000 04000 .00002 .00003 (INTRO) -.14314 59500°-0000 OLGPEACHTENTG AT GUTTENTS 1.00305 95000 .15676 79000 (UANINI) -.00006 040000 -.00003 -.04462 04000 \$0000 50000 60000 STRUCTURE ACTIONS (ALTS, INSKIPS) AT NUNLINEAH -59,5467 19,0270 202,2395 -1159,9070 -473.4465 -47.0597 5.36H4 269,9106 -2058,3245 -279,2965 1806.1550 65.4624 U/84 2131,0507 -44.9014 64.5618 のしないろうつの FRELDUM DEGHER さいとしまいた あまり ひことがいい ひことがしまし 2010 200 1001 7101

11 10/05/76 PAGE PILE-SIRUCTURE RESULTANT DISPLACEMENTS DIFFEMENCE PERCENT DIFFERENCE (CAN NAS) U.S. NAVY . ACHN PLATFUNMS . PATTEUE ANALYSIS . MLW 105,0 FEET PILE DISPLACEMENTS AT SUPPUNTS .05908 00024 000013 92000 -,00112 -,00000 ...03203 (IN.RAU) .0699B 62000 20000 .03483 01505 -.05847 -,00002 ----STRUCTURE DISPLACEMENTS AT SUPPLINTS .07576 -. 00038 -.00112 (UNAHAL) .09319 •• 00000 ..0/040 -. 00019 .00038 ₹0000 -.04166 -.04369 -01509 20000-00000 70000-STRUCTURE ACTIONS AT NUNLINEAR (BILES, LATA I PS) -122,3092 1320,0854 23,1543 -.6524 -4.6858 -20,6522 -11,1010 -44.3682 -10.3546 426.9785 16,4012 20.4425 84.96.69 -20.7793 -1200,4617 z SUPPORTS FREEDUM DEGMEE SUPPORT JOINT NO. 10101 1012 1010 1010 1000 1011 1011 CYCLE NU. 1

10/05/76 PAGE UATE HESULIANT DISPLACEMENTS .0062 .0076 .0124 .0131 DIFFERENCE PERCENT DIPFLHENCE \$000 (TAN AND) 0000 5000. 0000 1 1 E R A 1 L C R U.S. NAVY - ACMM PLATFORMS - FAITGUE ANALYSIS - HEW 105.0 FEET UISPLACEMENTS AT SUPPLIKTS -,00112 -,00016 -.06476 \$0000° .03653 65790 -,01657 -,00002 -.03945 01480 67000 (IN, KAU) 94000 F-00067 0000 - 2 - 2 - -DISPLACEMENTS AT SUPPURTS -,05792 -.01657 . U / HB9 -.00112 55000 -.00016 9000 -.00018 STRUCTURE (THINAD) 06000 50000 20950 .06430 17000 50000-.01460 ≥0000° n ¥ STRUCTURE ACTIONS (BULNEYINGTING) 1110-4145 1220-0081 17-56-56 20.6627 -48.0514 1027.4579 531.4617 40.5526 48.6843 452.8452 AT NUNLINEAR 43,6276 -.6/05 -11,5004 -10,6284 -18.5631 -19.7530 BLECHTON FRELOUA DEGNEE #07 FC10 YOUR INEAN 0101 222 2010 1016 1016 1011 1011

ITERAT

LUAD CUNUITIUN NU.

>

PAGE PILE-STRUCTURE RESULTANT DISPLACEMENTS UIFFERENCE PERCENT DIFFERENCE (IN, MAD) U.S. NAVY - ACHN PLATFUNDS - PATICUE ANALYSIS - MLM 105,0 FERT PILE DISPLACEMENTS AT SUPPURTS 00204 00204 000008 00008 -,55236 -,11018 000150 57379 00145 (IN, RAU) 00223 34690 00240 DIBPLACEMENTS BLECTTOR LA . 32070 . 0020d . 51559 .11018 .00018 (IN, HAU) 241046 00007 -.00140 18515 901142 00003 87100 .00043 .00018 70000 (RIPS, INSKIPS) 1,4525 660.1000 45,1099 600,6295 171,6652 -621,7436 52,4445 -2170.0545 48.1010 -666,9934 -115.4674 3469.3738 -64,5501 -45.5347 2963,7591 19509.2491 172.4537 のしというようのの FREEDUM DEGMEE NONC INEAR שניים ואוחר 2000 22000 2222 101

OTHER STREET STREETS

CVCLE NU. 3

W.

15/05/76

PAGE

z

.0183 .0233 .0196 FESTRUCTURE
RESULTANT DISPLACEMENT
UIFFERENCE PERCENT CIN, MAD) DIFFERENCE 1020 0570 10136 0000 \$600. 0000 .0127 0000 U.S. NAVY . ACHA PLATPUNAS . FAITEUL ANALYSIS & MLM 105,0 PERT DISPLACEMENTS AT SUPPORTS 000045 - 56861 000000 46253 00178 (IN, HAD) 90200 46803 11680 11231 00108 20956 DISTINCTURE DISTINCTURES SAT SOFFCRIS - 56247 45469 97000° \$0100. -,000217 40135 (IN.KAU) 90200 10000 25564 .11600 61000 11251 20100 STRUCTURE ACTIONS (NIFE, IN-KIPS) -6339.5365 -3410.7216 165.5101 5972,8340 AI NUNLINEAR 544.7543 43,7036 14,3060 PPP0 - 1404 672.8815 -110,5251 -57,4500 23.3414 -40.1442 45.5430 -699,7620 1,424 BUTHUHADE FREEDUM DEGHEL MOVE INCAN JULIA MU. しているという 20000 101 1012 2121

* ***** • •

7547 A. N. C. C. A. N. A.

10/05/76 PAGE UATE .0612 (IN. MAD) DIFFEHENCE *090* .0757 PILE-STRUCTURE MESULTANT DISPLACEMENT *090 UIFFEMENCE .0070. .0376 ANALYSIS - HLW 105.0 FEET DISPLACEMENTS AT SUPPUNTS 44562 11255 11255 00152 00092 -.61756 -,00008 .26062 00158 .00208 90000 (INVKAU) 00011 C.S. NAVY . AGMR PLATFURMS . PANISCIP DIOYING TANDO 00208 45116 000049 .45804 (IN, MAU) -.54749 F. 000812 04165 80100 10001 .,11661 -.001/1 *********** DESCRIPTION OF THE STATE OF ST (SAIVELIER IFS) -5943, 9022 102,6740 555.4071 6900.81#2 -78.1782 56,5588 -41,5110 672,9946 -116.4844 12,4514 5465,0620 1,3550 88,2063 48.0005 849. 7848 103,456 FREEJUM DEGNEE POLLINGS VOTFORT JUL 14100 22 1010 1011 LUAU CUNUITION NU.

CYCLE NO. 1

U.S. NAVY - ACAN PLATFOANS - FAITGUE ANALYSIS - MLM 105.0 FEET

NUNLINEAR	DEGMEE	STRUCTURE ACTIONS	STRUCTURE	PILE	
1204100	90 90	AT NUNLINEAR	DISPLACEMENTS	DISPLACEMENTS	ANGULLIANT CLOSTACES
•		(RIPS, INSTERS)	(INTRAD)	(IN, KAD)	
0101	-	30,7440	.15200	62780	
010	2	- 4493	\$ 000 \$	00137	
010	•	-11,3946	04100	00140	-
010	3	-125,7549		00000	
010	3 0	-2190,2923	\$C000	.00031	
010	9	45,2521	\$0000	.00003	
1101	-	-15,5876	-,07044	-,04259	
110	~	26,7571	.16513	0/421	
011	~	-129,8285	04107	02167	
1011	3	2267,9731	-,00043	- 00065	
011	5	1141,3244	00025	00014	
1011	٥	673.4449	20000-	-,00002	•
210	-	-14,1310	07124	-,04268	
210	~	-68.6199	12753	-,07321	
1012	~	112.4480	.01885	.01885	
016	3	-2263,4750	24000 ·	97000	
1014	^	842.7118	00027	00015	
017		a > 1. h 7 1.0	C0000	C0000	

PAGE

EVELE NO.	•		STREET AND A VANCOR		STATE OF STATE AND LIVE OF	105.0 6667	DATE	10/05/76	i i
			•						
	NUNE INEAR	DEGHEE	STRUCTUME ACTIONS	STRUCTURE	PILE	PILE-STRUCTURE	RUCTURE		i
	בב האטט בב האטט	FKEEOUM	AT NOT INCHARAGE WORKS WITH CALCATOR WALKER CALCATOR CALC	0 10 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	DISTERENTS AT SCHOOLSTS (IN. AAC)	AFGULTANT DI DIFFERENCE (IN, RAD)	SPLACEMENTS PERCENT DIFFERENCE		i
	5	-	31,6586	.10735	.11462				!
	1010	~	\$100°	07000	-,00217	6900	7700		į
	<u>۔</u>	~	-11.5549	00140	-,00190				İ
	5	3 .	-128.4784	100001	10000				
		•	1334,4151	4000	05000	0000	0640		•
	2	•	75 77 77	£0000°	50000				
	1011	-	-15.9947	42120	0.05456				
	1911	~	28.1075	20000	97560	2500	7050		1
	101	-	#### #################################	90120	60100		•		
	101	. 3	1406,0045	95000**	65000				
	1191	5	741,7848	57000·	00023	0000	.0578		,
	1011	٥	-41.5137	-,00002	20000-				
	510)		334 8 1	- 06307	06.740				1
		• •		- TWO	00.000	•	1 1		
	9101	u -	7/50000	0/040**	303A0*	0900	£/£0.		
	3101		5075-01	• 01769	A2010.				1
	7101	3 7 i	1620.1641	8000°	11000	•			
	9101	Λ.	0 V V C 0 C C C C C C C C C C C C C C C	\$2000°	CV000.	0000	9190.		
	1016	•	-21.1591	20000 ·	20000				1
	٠								
									ļ !
									1
							٠		
		-						,	
									İ
									!
							•		٠
									!
									!
						•			

ł

1 -1

1

1

1 . 1. 1

Γ



	UEPLEGT10N			DEFLECTION	:		DEFLECTION	
FILE	NUMBE TO	deau fac	PILE	PURMAL ID	BENDING		NUMBAL TO	BENDIVE
エーラスコー	7116		LE SG TE	7117 7117	とのでしている。	183671	PILE	ACSENT COLOR
1	LINCHESS	(Satvent)	1 2 1	- (Inches)	CRATYONT		(INCHES)	CRAINENTY
00.	9620.	-225.11	76.09	0000.	•,33	137.68	0000	00.
2	6220	-45.00	70.07	0000		134.41	0000	00.
00.	5610.	129.87	12,49	0000	1.07	101.43	0000.	00.
むっ・	.0170	290.14	75.02	0000.	1.27	145.96	0000.	00
=	1910.	454,30	17,05	0000	1.27	145.99	0000	900
3	5110.	560.55	79.08	0000	71.1	146.02	. 0000	90
2.17		074.00	81.10	0000			0000	0
21.2	3	707.54	65.13	0000	.73	152.07	0000	00
6.22	1500.	714.95	45.16	0000	.53	154.10	0000	30
8	.0035	695,67	A7.19	0000	.35	150,13	0000	20.
	661101	71.94	60.04	9999	Ř	44.	999	•
27.77	2000		77.0		•	61.061		200
77 77	7000	No • C 7 C	7,000		744	Tena!	0000	200
77.47		7 C P C P C P C P C P C P C P C P C P C	73.67		9 00	12.201		9 9
3		200	2000		V = 0	72.401		
		3636	66.14	0000	300	100.60	0000	000
50.41	10001	247,745	66.35	0000	• 05	166.29	0000	00.
3	, 000 v	1/8,17	101.58	0000	50.	170.52	0000	26.
54.47	1000.	118.95	103.41	0000	10.	172.35	0000	00.
	000.	7.0	105.44	0000	*O*•	174.37	0000	00.
25.	•0000	53.52	107.45	0000	• 03	170,40		00.
Ž	*000°	•	109.49	2202.	70*-	176.43	0000	00
46.55	#000 *	-12,97	111,52	0000	ಿ	180.46	0000	00
10.77	\$000°	-24.53	115.55	0000	-0.T	182.49	0300	20.
10.	?	-50.57	115.57	0000	10.1	184.51	0000	20.
90	1000.	-51.95	117.00	0000	••01	180,54	0000	00.
50.05	1000.	-30.51	119.63	0000.	00*•	180.57	0000	20.
_ ; ~	0000	-67.20	121.06	0000	00.	190.60	0000	00
54.15	3	-22.90	125.08	0707	, ,	192.62	0000	70.
_	3	-18.27	•	00000	00.	194.05	0000	20.
2	00000	-13.90	•	0000	000	196.68	0000	7000
.85	00000	36.30	129.77	0000	00.	198.71	0000	90.
64.00	0000	3		0000	0	200.73	0000	000
20.40	0000		155.62	0700	20.	402.76	0000	3
;	0000	11.71	145.85	0000	00			

The state of the s

**

	111. 0000	C.O. NAVY - ACKN PLATFI	TRANK - AFTECK BUSEAUT	X 1 0	105.0 FEET		
UEFLECTION			OEFLECTION			DEFLECTION	
DE JANKON		477.4	NURMAL TIL	BENDING	9116	NUNAAL TO	BENDING
(INCHES)	(SALM-VI)	(FT)	(INCARS)	(INEKIPS)	(FT)	(INCHES)	MUMENT (TNOKING)
0550.		300	9399	03.	137.88	0000	90.
# 0 N O .	•	10.47	0000	3	139.41	0000	33
.01/8	62.11	72.44	0000	6.	141.43	0000	30
.0155	74	75.02	0000	-	143.96	0000	7
.0129		77.05	0000	_	145.99	0000	000
.0104		79.08	0000	101	168.00	0000	00
5 900 0	502.07	A1.10	0000	59	150.04	000	9
\$400.		83.13	0000	90	152.07	0000	00
1400.	432.57	45.16	0000	27.	154.10	0000	9
.0032	616.51	87.19	0000	1,32	156.13	•• 0000	00
1700	575.10	55.48	0000	02.	51.45.	0000-	20
	515.45	91.24	2202	2.5	40.		200
7000.	245.80	93.27	0000	50.	162.21	0000	20.
0000-	370.75	95.30	0000	10	164.24	0000	00
4000	246.43	97.53	0000	03	166.26	0000	000
£000.	220.67	94.55	0000	3 0	168,29	0000	00.
	104.20	101.38	0000	30.	170.32	0000	00
1000.	110.84	105.41	0000	70.	174.35	00:00	_
	67,13	•	0000.	£0.	174.37	0000.	00.
\$000.	32,99	107.46	0000	•,03	176.40	.0000	000-
5000	7.73	104.49	0000.	₹0°-	176.43	0000	30.
*****		111.52	0000	20.	140.45	0000	20 -
\$ 000 ·		115.55	0000	70.	186.49	0000	20.0
2000	-46.2	115.57	0000		3	3	00.
1000	90.42	117.60	0000	• 01	186.54	1000.	1000
1000-		119.03	6000.	00.	188.57	0000	3 0 •
6000.	į		0000	70.	140.00	0000	00
7973.			•	90.	192.02		3
000	• -	125.71	0000	00.	194.65	0000	00.
0 n c • •	-12.57	127.74	0000.	20.	140.08	000ñ•	00
0000.		124.17	0000	00.	198.71	0000	20.4
coco.	:	151.79	0000	000	200.73	0000	77
333.		133.02	0000	?°	202.15	0000	20 4
4. 4. 4. 4	•						

A SING B A A A P D

10/05/76 33333 30. 2 2 2 2 300 33333 22022 0000 0000 00000 0000 00000 000 0000 00000 0000 0000 0000 0000 0000 (INCHES) 157.08 1184.91 141.93 145.46 150.02 150.02 150.04 156.15 160.18 162.21 164.24 166.24 178.43 180.46 182.49 184.51 174.35 188.57 190.60 194.65 194.65 166.29 200.73 80.54 - MLH 105,0 FEET BENDING BUMENT (IN-KIPS) 27. 2 6 6 5 % 00000 00000 8888 U.O. NAVY . ACHR PLATFORM . FAITCUE ANALYGIG DEFLECTION NUPRAL 10 PILE 00000 00000 00000 00000 0000 PENGTH CFT 70.47 72.49 75.02 77.05 111.55 1115.57 1115.57 119.03 121.06 125.08 125.71 131.79 131.79 133.82 155.85 44.08 81.10 85.18 CSGI XON! 262.95 1000.05 106.57 24.04 4.67 24,34 150,21 273,36 20.70 20.70 10.24 597,26 564.24 247.67 247.08 364.73 653.11 BENDING 6.67 MUMBAT 01100 .000. 0100. 4000. 1000. V000. *000* 50.41 54.47 54.47 59.50 56.77 56.77 56.77 22444 40.55



(;;<u>)</u>

						1331 00001		
فد	UE+LECTIUM			DEFLECTION			DEFLECTION	
1	COMMAL TO	GENOLNG	PILE	NURHAL TO	BENDING	PILE	NURMAL TU	BEND146
	(14CHES)	(IN-KIPS)	(FT)	(INCHES)	(IN-KIPS)	(F1)	(INCHES)	(INSKIN)
	.0193	-178.90	34.80	0000	•.26	137.68	0000	00
	.0171	64.24-	70.47	0		180.01	000	00
ı	*****	67.41	72.49	0000		141,93	0000	00
	.0127	204.70	75.02	0000	75.	143.96	0000	0
- 1	0100	1	77.05	2700	70.	145.49	0000	000
	0000	415.58	74.08	0000	ξφ.	148.02	0000	00
	9000	22.122	-	0000	7	5	000	90
1	2500.	565.45	85.13	0000	\$4.	152.07	0000	2
	8 5 00.	535.13	⁻:	0000	24.	154.10	0000	99
	.0020	518.55	-	0000.	929	156.13	3303	00
	4.00	00.140	00.00	0000	4.	11.1		
	200		97.10		2 2			
1	\$ 000.	370.07	93.27	0000	20	162.21	0000	
	.0001		05.50	0000		104.24	0000	
		244.25	97.33	0000	••03	166.26	0000	00
	5000-	185.88	94,55	0000	*00	168.29	0000	00
	<0000-	153.90	101,58	0000-		170.52	0000	
1	9700.	04.00	7.5	0000	•	172.35	0000	00.
	5000-	53.50	*	0000.	٠.	174.57	-	00.
i		Š	107.46	0000	02	170.40	5	00
	1000.	4.79	3	0000.	₹0.	176.43	0707.	20.
- 1	\$ 000°	-0.30	į	0000.	-,01	180.45	3	3
	*000°	i	115.55	3	10.	186.44	0000	•
	202.	-5.27-	'n	0000.		;	9700	3:0
		-43.72		0000	20.	70.057	0000	3 5 6
	10.0.	-44.75	•	3707	00.	140.57	0000	•
	0)0).	15	171.00	0,0,0	30 ·	٠	\sim	3,0
	? ? .	-17.14	^	0000	00.	•	•	73.
	() () •	04.07.	1725.71	00000	20.	19.05	-	3
	C000.	-10.55	•	0,0,0,	3 0.	140.00		33
	0000	-7.30	124.77	0,000	00.	196,71	0300.	3
	coon.		151,79	000	0	£ 000 \$	000	_
		1						
)))		155.02	0000	30	202.16	00000	22.0

BENDING MOMENT (IN-KIPB) 93393 00000 33030 3 3 3 PAGE DAJE DEFLECTION NURMAL TO 00000 00000 000000 0000 0000 303 .0000 0000 (INCHES) 180.46 PILE LENGTH (FT) 137.68 134.93 141.93 143.46 100 100 100 100 100 100 100 100 156.15 160.18 164.21 164.24 166.20 190.00 190.00 194.62 194.65 196.71 200.73 202.76 170.32 172.35 174.57 78.43 MLH 105.0 FEET 31.00 BENDING AUMENT (INEKIPS) 2222 00.00 2000 20000 0000 - ACHY PLATFORMS - FATIGUE ANALYSIS DEFLECTION NUMBER 10 000000 00000 00000 FILE (INCHES) 00000 0000 0000 101 44 105 44 105 44 107 44 PILE 70.47 104.49 111.52 115.55 114.05 121.06 123.06 125.71 124,77 131,79 135,82 135,85 89.22 91.22 93.20 93.50 -210.65 -82.96 59.89 154.27 170.30 123.54 55.56 50.71 115.30 119.61 20.20 113.20 12.21 20.20 20.20 386.40 354.10 278.17 -6.70 -2.50 -2.50 (Set xeel) BENDING 430.54 222.54 NOTIFE TO NOTIFE CONTINE 4000. 0000 00000 0000 01174 41000 .0001 .0000 .0004 -.0002 0000. PILE JUINT NO. 1011 LENGTH (F1) 50.47 56.44 56.44 56.47 20.28 20.55 20.55 20.50 06.03 02.00 04.00 0 0 1 0 C 12.17 40.55 56.75 56.75 56.75 56.75 44.50

	Æ.				•		1	
	~		z ∢ x ⊷	P 11 F	#0 \- >			PAGE 6
		9	- ACMN PLATE		ANALYSIS - PLW	105.0 FEET		
	CEFEETIUM			DEFLECTION			DEFLECTION	
148 19 19 19 19 19 19 19 1	0 4 1 4 1 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	3 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	2 C C C C C C C C C C C C C C C C C C C	NURHAL TO	DE LONG	3116	NURMAL TO	SENONAL PROPERTY.
14.65	(SACHES)		(FT)		(IN-KIPS)	(FT)	-	(INOKIPS)
10	.0170	148.3	90.4	9999	•	137.66	0000	36.
14, 25	.0155	-26.4	70.47	0000	98,	16.651	0000	00
144, 95 75, 12 144,	. 0155	40.5	72.49	0000	.73	141.43	0000	90.
100.77	\$0115	296.05	?	0000	9 9	145.44		200
444.97 444.97 460.77 460.72 477.19 47.1	•		,					
47.34 46.34 47.34 48.35 48.462 48.463 48	£/00.	501.77	2 -	0000	77	140.02	0000	3
14 15 15 15 15 15 15 15	7,00	400.77	: =	0000	50	152.07	0000	33
# 12, 54 # 12, 65 # 1, 62 # 1, 62 # 1, 62 # 1, 62 # 1, 62 # 1, 62 # 1, 62 # 1, 62 # 1, 62 # 1, 62 # 1, 62 # 1, 62 # 1, 62 # 1, 62 # 1, 63 #	4600.	72.42	: ∹	0000	95.	154.10	0000	
12,92	5200°	4/2.34	-	00000	454	150.13	0000	20.
340,46 91,24 -0000 002 1064,24 245,71 95,47 -0000 -01 1064,24 277,46 97,43 -0000 -03 176,42 107,91 99,45 -0000 -03 176,42 100,72 101,44 -0000 -03 176,43 47,40 107,40 -0000 -03 176,43 47,40 107,40 -0000 -03 176,44 47,40 1000 -000 176,44 -10,10 -000 -001 186,54 -10,10 -000 -001 186,54 -10,10 -001 186,54 -10,10 -001 186,54 -10,10 -001 190,04 -10,10 -001 186,54 -10,10 -001 186,54 -10,10 -001 190,04 -10,10 -001 190,04 -10,10 -001 190,04 -10,10 -001 190,04 -10,10 -001 190,04 -10,10	.0013	457.95	89.48		7	156.15	•	30
107.91 95.27 100.00 100.21 100.22 10	1000°	340.45	91.24	0000.	20	160,16	0000	30.
107,000	\$000	535.71	95.67	0000.	70.	162.21	0000	20.
107.91	1000.	277.88	95.30	0000	10.	164.24	•	00
120.72	\$000	76.022	97.35	0000	50.0	166.24	•	00.
120.72	*000	6	99.55	0000	* 0.	166,29	0000**	00.
3.86 109.46 .000002 176.43 174.37 111.52 .000002 176.43 176	\$000°	2 2	101.38	0000	103	170.52	0000	30.
3.86	6000	FC • 00	70.00		7 6	1/6.33) ·
0000 -002 178.43 0000 -01 180.46 0000 -01 182.49 0001 -01 184.51 0001 -001 184.51 0001 -000 186.54 0001 -000 186.57 0000 -15.54 180.00 0000 -15.54 182.65 120.71 186.65 196.65 0000 -15.54 186.57 0000 -15.55 182.71 000 0000 186.77 000 196.67 0000 -200.73 -200.73 0000 -25.54 000 000	1000	- ~	107.46	0000	• •	176.40	• •	20
00002	.000	3.40	104.49	0000	≥0°-	78.4	0000	00.
115.55 .0000 .001 184.51 1001 .000 .001 184.51 1001 .000 .000 186.54 1001 .000 .000 194.55 1000 .000 .000 194.65 1000 .000 194.65 .000 1000 .000 194.65 .000 1000 .000 194.65 .000 1000 .000 194.77 .000 .000 1000 .000 .000 .000 .000 1000 .000 .000 .000 .000 1000 .000 .000 .000 .000 1000 .000 .000 .000 .000 1000 .000 .000 .000 .000 1000 .000 .000 .000 .000 1000 .000 .000 .000 .000 1000 .000 .000 .000 .000 1000 .000 .000 .000 .000 1000	.0003	TH. H.	111.52	0000	100-	180.46	0000	00
117.57 .000	2000·	-16.70	115.55	0000	10.	182.49	U 900 *	70.
0000		100.76	115.57	0000	•	164.51	9909	0 0
0000 -20.71 119.65 .000 140.60 0000 -15.54 123.68 .000 194.65 0000 -12.34 123.71 .000 194.65 0000 -12.34 127.74 .000 194.65 0000 -6.64 129.77 .000 194.71 0000 -4.35 131.79 .000 200.73 000 -20.73 .000 202.76								•
0000	- C - C - C - C - C - C - C - C - C - C	-20.71	114.05	0000	0 : 0 •	186.57	0000	06.
0000 -12.34 125.71 .0000 .00 194.65 0000 -9.36 127.74 .0000 .00 198.71 0000 -6.64 129.77 .0000 .00 200.73 0000 -4.35 131.79 .0000 .00 202.73	0000	15.55	123.68	0000	•	190.00	0000	300
0000 -9.36 127.74 .0000 .00 198.71 .0000 .00 .00 .00 .00 .00 .00 .00 .00	0300	-12.34	125.71	0000		194.65	0000	
0000 =6.64 129.77000 .00 198.71 0000 =4.35 131.79000 .00 200.73 0000 =205.74	0000.	-9.30	127.74	0000	000	190,08	0000	20
0000 -4.35 131.79 0000 000 200.73 0000 -2.53 155.62 0000 000	0000.	••	129.17	0000	00.	198.71	0000	00.
0000 -2.55 155.62 0000 000 20.76	00000	4.3	131,79	0000	200	200.73	0000	200
137.00	0000	· .	155.62	0000	000	202.76	0000	00.

1	C110W L 10 LE 10		- ACAN PLANFO	UNHS - FAIICUE	SANALYSIG . HLR	105.0 FEE1		
				DEFLECTION			DEFLECTION	
		BENDING	PICE	NURMAL TU	BENDING	PILE	NURMAL TO	BENDING
	MES)	(\$d1x=N1)	(FT)	(INCHES)	TOUR NEW TOUR	(+1)	(INCHES)	(IN-KIPS)
	0783	-737.61	75.00	1000		157.68	01100	10.
	9	-194.22	70.97	0000	1002	139.91	0000	
	• >	532.44	72.49	0000	3,16	141.93	0000	00
	0515	970.40	75.02	0000	3,81	143,96	0000	20.
	0620	1272.77	77.05	0000	3,82	145.99	0000	00.
	0.540	1004.50	3	Ondo	77 2	CO. MD.1		ē
	0211	1959-61	01.18	0700	7.87	150.00	•	
	0212	2125.40	-	0000	2.23	152.07	0000	70
	0155	2167.AS	~	0000	-	154.10	0000	200
•	1010	2102,71	8/.19	0000	1.08	150.13	7007	00
•		•	:					
	700		27.69	0700	\$9°	158.15	6000°	90°
-	0000		71.64	0000	75	100.18	0000	00.
•	5100	1300	45.67		010	194.21	0000	00.
	5000		00.00		50. ■	104.68	0000	•
		0 0 0	1	0000	21.6	100.00	0000	70.
	0000	-	55.90	0000		168.00		6
	100	34.04.0	13	0000		170.52		
	0062	305.79	105.41	0000		172.55	0000	30
	0021	•	3	0000		174.57	0000	3
	0018	3	4	0000	60.	176.40	0000	000
•	4	***	3		1	44		
95.24	2100	-37.15	111.52	0977	40	180.45		
10	6000	-72.86	113.55	0000	70	182.49	0000	20
•	1000	-91.10	115,57	0000.	.03	184.51	0000	00
••	2	-46,25	117.00	0000	-,02	180,54	2000	90.
	1000	36.00	4	9300	•	7 7 7		
	9 9		•	0000				
54.75	0000	-69.55	125.08	0000	00	192.62	0000	00
•	9		~	0000	00	194.65	0000	200
•	3	•	127,14	0000	0.01	196,68	0000	
4	3	50	•	•	ć			
	7000	77.01	•			1/*0/1		9 9
	1000	11.55	. 2	0000		202.78		
91	0001	5.44	135.05	0000	0 1			•

ø
-
•
>
د
•
Z
•
w
J
-
-
•
- C - Z -
0. I

REPORT THE PROPERTY OF THE PRO

			UEFLECTION			DEFLECTION			DEFLECTION	
1.075531 (TACKIRS) (TT) (LINCHES) (TACKIRS) (T	1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	l	NUMMAL TU	BUNENT MUNENT	PILE	NURMAL IU	MUNENT	Pare Lessen	NURMAL TU PTLE	BENDING
1414 19	1	- 1	I CHES	(IN-KIPS)	(FT)	(INCHES)	(SATYANT)	(F1)	(INCHES)	(SAIN-NI)
141,00	111 2		.0703	-879.76	3. D.	0707		137.66	0000	10.
1411 99 17 17 18 18 18 18 18 18	14 14 15 15 15 15 15 15		0.0545	141.62	70.07	00000	1,655	159.41	0000	3.3
1414.19	1444 9 77,45 4000 3,10 144,49 144		8070.	6119	75.02	0000	3,35	143.96	0000	
1750.14	1799.14 199.00 190.00	- 1	2450.	1037.91	77.05	0000	3,40	145.99	0000	30
1578 18 18 18 18 18 18 18	17.00 19.0		.0520	1414,19	40.04	0000	3,10	146.02	0000	00
1756.15	128-14		\$450.	1049.18	81.10	0000	4,60	150.04	0000	
1256,04 1956,14 1956,15 1956	1756.04 1941.0 1941.1		.0145	18/1.37	65.13	0000	2,03	152.07	0000	20.
1578;12	179.24 19.4 19.4 19.6		9	10.4261	85.16	0000	23	154.10	0000	00
1158-15 1159-14 1159-15 1159-16 1159-16 1159-16 1159-16 1159-16 1159-16 1159-16 1159-16 1159-16 1159-16 1159-16 1159-16 1159-16 1159-16 1159-16 1159-17 1159-18 115	199.15	- 1	0010	1991.26	87.19	0000	1,00	156.13	0000	000
1559,22	1500, 24 91,64 9		4000.	1758.15	84,22	0000	10,	158.15	0000	•
1,500,10 95,27 1,000 1	1300-18		0500.	1579,22	91.64	0000	, 31	160,18	0000	
158.28 95.50 0000 03 166.24 156.25 156.	91197 25 99.50		71000	1506.10	95.27	0000.	010	162.21	0000	20.
698.27 99.35 ".0000 ".13 104.22 507.12 101.48 ".0000 ".13 170.42 208.29 105.44 ".0000 ".00 176.45 208.94 107.46 ".000 ".00 176.43 208.94 107.46 ".000 ".00 176.43 209.95 111.55 ".000 ".02 184.51 209.95 115.57 ".000 ".02 184.51 209.95 115.57 ".000 ".02 184.51 209.95 117.55 ".000 ".00 184.51 209.95 117.55 ".000 ".000 184.51 209.95 117.55 ".000 ".000 184.55 209.95 121.55 ".000 ".000 184.55 209.95 121.55 ".000 ".000 194.55 209.95 121.55 ".000 ".000 194.55 209.95 121.55 ".000 ".000 ".000 ".000 209.95 122.56 ".000 ".000 ".000	\$43.24		2000	1158.28	95.50	0000	. O.	164.24	0000	70.
100,000	1000 1000	- 1		411.53	2001			02.001	0000	•
100,000 100,	26.07 176.94 105.4 105.4 107.4		0017	696.27	9	00000	••13	166.29	••0000	90°•
108.44	15,94 105,44 .0000 176,45 176	- 1	0000	507.12	6	0000	•,13	170.52	0000	00
103.95	10.5.95		9 9	70°750	3 4		7. ·	176.35	0000	000
-27.90 -27.90 -113.55 -113.55 -1000 -104 -105 -113.55 -113.55 -1000 -104 -104 -105 -113.55 -113.55 -1000 -104 -105 -105 -106 -106 -106 -106 -106 -106 -106 -106	-27.90 -2		0016			0000	• 0	176.40	0000	
-67.90 -61.75 -6	-27.90 -11.52 -1	1	7100	70.47	57 50.	0000		100		
-61.75 113.55 .0000 -04 168.49 188.51 .0000 -03 188.51 188.51 17.60 .0000 -02 188.51 186.57 .0000 -02 188.51 186.57 .0000 -00 198.62 190.60 19	-85.57 113.55		1100.	06.75-	111.52	0000	50.	150.43		
10004 -79.59 115.57 .000003 184.51 1000402 186.54 117.60 .000002 186.54 186.54 100002 186.54 186.57 100001 186.57	0000	1	9000	-61,75	113.55	0000	*0	182.49	0000	30.
0004 -65.54 117.60 -0000 186.57 0004 -65.54 114.63 -000 190.60 0004 -65.04 121.66 -000 192.62 0004 -65.04 125.71 -000 194.65 0004 -50.73 127.74 -000 -01 196.71 0004 -56.57 1131.74 -000 -01 196.71 0004 -56.11 133.65 -000 -01 -01 -00.73 0004 -10.96 -133.65 -000 -01 -01 -02	11 12 13 14 15 15 15 15 15 15 15		\$000°	-79.59	115.57	0707	*0°	184,51	0000	00.
-82.57 119.03 .000001 198.57 190.00 190.00 190.00 190.00 192.02 190.00 192.02 190.00 192.02 190.00 190.01 190.02 190.0	-82.57 119.63 .000001 188.57 .0000 .000 .000 .000 .000 .000 .000	- 1	- 1	-85.34	11/.00	00000	20.0	:n	0000	00.
-54.55 121.66 .0000 .00 192.62 .0000 .00 192.62 .0000 .00 192.62 .0000 .00 192.65 .0000 .00 192.65 .0000 .01 196.71 .0000 .01 196.71 .0000 .01 196.71 .0000 .01 196.71 .0000 .01 196.71 .0000 .01 .01 .000.73 .0000 .01 .01 .000.73 .0000 .01 .01 .0000 .01 .01 .0000 .01 .01	-74.55 121.66 .0000 .00 190.60 .0000 .000 192.62 .0000 .000 192.62 .0000 .000 192.62 .0000 .001 196.65 .0000 .001 196.65 .0000 .001 196.66 .0000 .001 196.66 .0000 .001 196.66 .0000 .001 196.66 .0000 .001 202.76 .0000 .001 202.76 .0000 .001 202.76 .0000 .001 202.76 .0000 .001 202.76 .0000			-82.57	114.03	0700.	.0.	188.57	0000	00.
-54.00 125.06 .000 192.02 -50.73 125.71 .0000 .01 190.05 -38.55 129.77 .0000 .01 190.71 -18.41 131.79 .0000 .01 200.73 -10.90 135.62 .0000 .01 202.76	-5,00 125,00 100 00 192,02 0000 194,05 000	ı	0001	-74.55	121.66	0000	000	190.00	0000	200
-38.55 127.74	-36.65 123.71000001 196.680000 -27.71 129.77000001 196.710000 -18.41 131.79000001 200.730000 -10.96 133.82000001 202.760000 -5.32 135.85000001		0000.	66.5°0	125.08	0303	3	192.62	0000	000
-27.71 129.77	-27.71 129.77)	.36.55	127.74) ·	100.00 100.00		3 3 6 0 1
-5.32 10.00 000 10.00.73 10.00 000 001 10.00.73 10.00 001 20.73 10.00 001 20.73 10.00 001 20.73 10.00 001 20.22.76 10.00 001 20	-2,271 129,77	1		1 1						
10°0 0000 133°62 10°00 000 001 50°.76 0000 001 50°.76 0000 001	10°00°1 \$0°00°		1000	•	154.17	0000		148.71	000	3 ·
10° 0000° 50°55° 1000	10000 0000 0000 0000 0000 0000 0000 0000 0000	I	1000	• c	27.77	0000		2000-73	200	30
•			0000	\$	135.85	0000	. 01			•
								•		
		1								

111391940						1011011111	
FILE SURFAL TO	DARNOING	9116	NURAL	30000	PILE	NURMAL TO	SEND ING
r	_	LENGIN	r1.e	MUMENT	LENGTE		NUME'S T
(FT)(FT)		(67)	(Inches)	(IN-KIPS)	(FT)	(INCHES)	(SAI wewI)
		95.89	0000.	\$6.	137.88	9000	10.
\$00.		74.97	0000	1.50	139.91	0000	10
2550.	326.85	72.49	0000.	5,45	141.43	0000	30,
•		75.02	0707	3.51	143.96	0000	70°
.11		77.05	00000	3.51	145.49	0000	70.
	1537.1	97.56	0000	3.16	146.02	0000	00
		M1,10	0000	2,63	150,04	0000	20.
6,10.		H5.13	0000	2.04	152.07	0000	30.
•	_	45.10	0000	1.47	154.10	0000	20.
2500.		87.19	0000	96	156.13	0000	30.
20.28	1789.51	84.22	0000	95	61 - 851	0000	93
		27.10	0707				•
55000	2 13/5.18	95.27	0000	30	162.21	0000	3
•		95.50	0000	*0	164.24	0000	30
20.59	3 407.50	97.53	0000		166.26	0000	00.
\$0.41		94.45	0000	# "	168.29	0000	30.0
		101.58	0000	41.4	170.52	0000	36
34.47		103.41	0000	12	172.35	0000	25.
	198.45	107.44	0000	10	174.37	0000.	30°•
		107.46	0000	900	170.40	0000	000-
40.55		104.40	0000.	07	178.43	0000	20.
	1 -35.04	111.52	0000	20°	180.46	0000	00
•		115.55	0000	*0.	182.49	0000	20.
		115.57	0000	20.	184.51	0000	30.
#000°	30° 00°	117.00	00000	-,02	180.54	0000	300
50.00		119,63	0999	10.	188,57	0000	20.
•		121.06	0000	00**	190.00	0000	22.
		125.08	0000	70.	192.62	0000	70.
•	.20.	125.71	0202.	20.	194.65	0000	30.
1000.		127.74	0000	100	190.68	00000	000
1000.		124.17	0000	10.	198.71	0000	20.4
90.	1 -17.45	131.79	0000		200.73	0000	00
		135.02	00000	10.	202.76	6000	30.
.0001		135.85	0000	10.			
							1



Personne (Hiller and Charles Energy Expense (History Property Park)

The second secon

		UEPLECTI			DEFLECTION			DEFLECTION	
	1	PANADA 1	BENDING.	PILE	NURMAL TO	BENDING	PILE	NURBAL TO	BENDING
1941 1941	Z -	•	3	F NG I	PILE	M.)MENT	LENGIA	PILE	FORENT
19.5 19.5		•			LINCHEST	(Ballyant)		(TWCHES)	COATMONTS :
1000 1000	20.	6150.	-567.16	46.94	0000	30.	137.88	0000.	90.
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	3	0070	-191,36	70.97	0000	1.02	159.91	0000	200
1000 11 12 12 12 12 12 1	0 1		30°>0'	66.27	0000	2.07	£6.731	0000	3
1,242	2-	0000	00°10°	77.05		2,52	1 to . 40		9 3
1000	7	. (1)	10.76.94	30	0444	7 0	1		
11144 142.97 1124.19	_	.0105	1270.59	61.10		16-1	130.08		
1000	. 10	2010.	1394.77	H5.13	0000	1.46	152.07	0000	200
1744 1744	7 5	7/07	1467.90	85.16 87.10	0000	1.06	02.457	0700	3 0
1000 115.00 1000	!	•				1			
	22:	£ # 00 .	1594.01	84,42	0000	77.	154.15	0000	•
1000 1000	3	\$200.	2154.05	97.16	0000	72,	160.18	0000	22.
1000 124 101 102 101 102	25	•		7.00		2 6	106.21	0000	3 : 6 :
	3	• •	603.50	97.6			166.26		
1013 1014	!								
		V100.	500.00 500.00 500.00	\$7°55	0000		166.29	3000	30.0
	47	5100	246.03	103.41	0000	00	172.65	9999	
15.45 101.0	\$	71000	75.57	105.44	0000	.07	174.57	0000	
	. 52	100.	72,52	107.46	0000	• 00	170.40	0000	30.
	\$\$.	.00	15.43	67 601	0000	\$0.	178.43	000	00.0
	.58	8000.	-22,45	111,52	0000		180.46	0000	3
0000001 1000001 10000001 10000001 10000001 10000001 10000001 10000001 10000001 10000001 10000001 10000000 10000000 10000000 10000000 10000000 10000000 10000000 10000000 10000000 10000000 10000000 10000000 10000000000 10000000000000 100	·	9000	*47.11	115.55	0000	500	182.49	0000	20.
	9 6	3000.	154.65	115.57	0303	7 0•	184.51	0000	•
0002	!	•	n '		•		2001	200	
0001 -54.67 121.66 .0000 -000 194.62 .0000 .000 .000 194.62 .0000 .000 .000 .000 .000 .000 .000	70	₹000*•	60.00	114.03	0000	••01	188.57	0000	20.
-0000 -57.06 125.74 .0000 .00 194.65 .0000 .000 .000 .000 .000 .000 .000	2/	1000.	.54.67	121.06	0000	00.	190.00	0000	200
	.:		CV-040	163.00	0000	3	196.62	0000	•
.65 .0000 .000 .000 .000 .000 .000 .000		> >	-26.15	127.74			100.00	0000	3 3
	.05		-20.08	2	0 2 0 2	00	96.7	0000	00
	90	Э	15.27	3.	0000	10.	200.73	0000	٠.
00000		3	-7.82	%	2000	70.	•	0000	30.
	•		2.00	9	⇒	•			

		•						PAGE 11
11			S. NAVY . ACHR PLA	TFURMS .	ANALYSIS -	105.0 FEET		
Color Colo				OFFIECTION			DEFLECTION	
1		BENDE	-	NURNAL TU	BENDING	PILE	NURBAL TO	BENDING
1,12,15	3	(1 ×=×1)			(Salver!)	(67)	Z Z Z	(IN-NIPS)
1427 7547 7547 7547 7547 7547 7547 7547 7	o• oo•	-703.1	9.88	0000	1.0	37.	0000	0
1,127 127	30.	-352.A	70.4	0000		139.41	0000	70
1176 125.7	0.	23.9	4.27	0000	_	141.93	0000	23.
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	5° 5° 5° 5° 5° 5° 5° 5° 5° 5° 5° 5° 5° 5	356.9	75.0	0000	~ ~	46.54 46.54	0000	9 G
113								- ^^ -
1000 1000	0. 14	1 927.6	79.0	0000.	2,12	144.02	0000	>0
1000 1544 10 1000 100 100	2	1152.7	20.00	0000	1.79	150.04	0000	700
1000		1634,00			9 -	776.07		> :
1201.15	65	1260,5	87,1		•	150.13	0000	30
1000 12,247	00.	7.1071 24	A	•	2 17	91 191	5	
0000	00.	25 1002.6	2.16	3333	22.	1001		
	000	11 459.4	7.50	0000	90.	162.21	0000	90 •
	00.	00 282.0	45.5	0000	~ 0 ~	104.24	0000	90.
	00.0	630.6	9/.3	ခို	-004	160,26	3	00.
10013	•	011 48	64.3	9900**	00.	166.29	0000	00
	•	55	101.5	0707	60	170,52	0000	900
	7	510	3.50	0000	20 6	172.35	0000	00.
-, 0010			107			176.60		
11								
1000	, , , ,	0 7	J. +0-	0000	50.	N7.0/1	0000	30°
000	10.1	0.7	2.511	0707	0.03	182.49	0000	200
	70.0	•53°	115.5	0000	20.	184.51	0007	00
	90.0	.57.	117.0	00000	-01	186.54	0000	00.
75	0	.56.3	4 114.6	0000	10.	184.57	0000	0
754000 -43.34 123.64 .0000 .00 194.65 .0000 77 .0000 -35.01 125.71 .0000 78 .0000 -19.27 124.77 79 70 70 70 70 70 70 70 70 70 70 70 70 70 71 72 73 74 75 75 75 75 75 76 77 78 79 70	2,72	6.05-	3 121.6	0000	00	190.00	0000	00
	52.4	N . M 7 .	9*521	0000	30°	194.62	0000	20.
) · · · · · · · · · · · · · · · · · · ·	7.65.7	1 127.7		9 0	144.05		0.0
								•
86 .0000 -7.74 153.62 .0000 .00 202.76 .0000 .99	0. 22.	2.01.	7 124.7	0000	9	196.71	0 0	20.
.41 .0000 -3.82 135.85 .0000	99	7.7	133.8	0000	000	202.78	Э С	
	. 61	8.8	135.6	0000	00		,	•
						•		

16/05/76 HUMEN1 (1 N=K 1 P8) 22222 PALE DEFLECTION NURBAL 10 PILE 0000 000 .0000 . 0000 (INCHES) PILE LENGTH (FT) 150.08 150.08 156.07 154.10 157.68 154.91 161.93 165.46 156.15 160.18 164.21 164.24 108.29 170.52 172.55 174.57 176.45 186.46 186.59 186.51 196.00 194.00 194.05 198.71 200.73 202.76 - ACAK FLATFURIS - FAILFUR ANALYBIS - MLA 105.0 FRET (SAIVERI) 40000 00000 2000 00000 00000 3000 0000 00000 0000 (INCHES) PILE LENGTH (FT) 101.59 105.41 105.44 107.44 124.17 131.79 135.82 155.85 74.08 81.10 85.13 87.16 94.62 115.57 70.47 72.49 72.49 75.02 117.03 121.06 125.08 125.71 104.49 BENDÍNG HUMENT (INSKIPS) 157.62 143.80 155.22 -541.29 -220.21 127.08 450.30 1000.46 1511.52 250.34 250.38 250.38 143.34 16.74 16.02 14.03 16.33 16.03 -12.70 DEFLECTION NOWNAL TO FILE 1111 -.0004 00000 0000 0000 0000 10001 0175 4000 ..0010 9000 9 0 7 9 0 0 0 0 0 24.48 24.48 24.58 24.58 26.58 36.41 36.41 36.44 36.44 56.04 54.72 50.73 60.00 16.17

	!	
		® II ® I
23.3 25.5 25.5	Ö	LEANA
	i	1 1 2 4 1
	•	⊢
	:	
		٥.
		ION NO.

		C.U. NAVY	ACEX PLA	1091 V V V V V V V V V V V V V V V V V V V	. ANALYGIS . ALE	105,0 FEET		
:	VEFLEGT10N		: : : : : : : : : : : : : : : : : : : :	DEFLECTION	; ;		DEFLECTION	! ;
P.I.C.	NUMBEL TO	DENOTAG	116 116	NURMAL 10	BENDING	PILE	NURMAL TO	BENDINE
(FT)	(INCHES)	(9d1y=v1)	(FT)	CINCHES)	(Luerips)	CTT	PILE (INCHES)	MUMENT (IN-KIPS)
0	1932	-2124-12	20.00	1000	~	147.48	5000	•
2.03	1724	D4 6/6-		000	•	- 7		> =
4.00	.1523	144.40	72.49	1000	~	141.43	6000	30
£0.	1317		75.02	1000	8,17	143.96	0000	0
6.11	.1116	\$6,855	77,05	0000	A . A 4.	145.99	0000	10.
71.	#200°	5206,48	74.08	0000	8.37	148.02	0000	10.
14.17	0760.	4001,35	A1.10	0000	1.24	150.04	000	3
21.71	\$050.	4574.70	65,13	0000.	٦.	152.07	0000	00
6.42	6500.	4695.78	A5.16	0000	4.56	154.10	0000	00
6,65	.0315	4454.70	91.19	0000	3,04	150.13	0000	0.0
87.0	. 0211	47.57.48	89.48	0000	1.45	158-15	0000	30.
22.30	.0127	4355.61	91,64	0000	1.06	0.1		00
64.55	>0000	3425.90	95.67	0000.	77	٧.	0000	00
•	.0016	3245,51	л	0000		164.24	0000	00.
45.5	0016	2649.34	97,33	0000	121.	160,26	00000	00
50.41	1500	2013.42	99.35	0000	-,34	166.29	0300	0 (
54.44	7 700°-	1545.54	101,38	0000	-, 35	170,52	၁	2
34.41	1500.	1005.75	105.41	0000	-, 32	172.35	0000	00.
50.50	7700	647.51	105.44	0000.	67	174.37	0000.	0 ·
8.56	\$#60.	50H. H3	107.45	0000.	-,25	170.40	. 0000°€	00.
\$5.0	P. 00.59	154.20	07.701	00000	.16	178.43	0000	3
46.50	5500	-13,47	111.52	0000.	-	150.46	0000	0.0
10.11	5700.	-124.55	115.55	0000.	11	182.49	0000	00.
٥	- no19	-164.50	115.57	0000	\sim	164.51	0000	30
60.5	0015	-<15.33	117.00	0000	50	186.54	3000.	00.
50.05	£000.	-218.00	119.03	0000.	£0	188.57	0000°	00.
54.14	COO.	-202-20	٥	0000	01	190.00	0000	00
54.15	2000	-175.HO	125.08	0000	00	194.62	0000	000
	0000	-1160.37	7.	0000	1 0.	194.65	6000.	37.
00.		-112,77	121.14	0000	10.	196.68	0000	7 0
\$0.	.0001	-63.9U	124.17	0000	50.	198.71	0000.	20.
62.50	≥ 000°	50,74	151,79	0000		200.15	0000	00.
99.7	2000	-55,75	155.62	0000	• 20	404.76	0000	0000
	E 4.0.4	70 011	100					

PARTIE DESCRIPTION OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PARTIES

					JN CV	3		ST LONGE
# T L L L	- 4 - 4 - 4 - 4 - 4 - 4 - 4 - 4 - 4 - 4	ST TOTAL	# (UN)			T SC I	PILE	MUMENT
(£ 1)	(INCHES)	(\$d!x=\!)	(11)	(INCHES)	(IN=KIPS)	C+D	(INCHES)	(Salkenl)
00.0	51935	-2124.12	94.94	. 0001	-7,23	157.08	0000	10.
2.05		D4 6/5	10.47	.0001	. 30	139.91	•0000	100
97.1	1523	144.40	72.49	.0001	5.74	141.43	6000.	10.
80.0	11810	1244,71	75.02	1000	71.00	80°50°	0000	0
6.11	.1116	\$0,855	504//	0000	•	143.77		***
214	7760°	3206,48	74.08	0000	8.37	148.02	0000	10.
2.17	9770	4001,35	A1,10	0000	7.24	150.04	0000	000
71.7	\$050.	4514.70	45.13	00000	5.61	152.07	0000.	20.
27.5	6540.	1	H5.16	0000	4.56	154.10	0000	0
6,65	.0315	4434,70	N7.19	0000	3,04	156,13	0000.	750
8 Y 3	1150.	4727.48	55.68	0000	1,43	158.15	0000	00.
08.44	1770	4355	91.6	0000	1.06	160.18	0000	000
- 55.45	200m	3425.90	45.67	0000	•	162.21	0000.	00.
95.0	0100	3245,51	95,50	0000.	\$0.	164.24	0000"	00
95.0	0019	2649.34	97,33	0000		160,26	0000	000
3	1500	2073.42	99,35	0000	•,34	166.29	0000.	70.
34.44	M 700 -	1545.52	101,38	0000	•, 35	170,52	0000	00.
34.41	0051	1005.75	105.41	0000.	•, 32	172.55	0000	00.
06.0	プマロコ・	697,51	4	0000	12.	174.57	0000	•
50.05	\$#60.	\$88.43	107,46	0000		1/0.40	in on	0000
55.0	-,0059	154,20	67.601	0000	.16	178.43	0000	20.
46.50	-, 00.52	-13,h7	111.52	0000	7.0	130.46	0000	96
10.1	5200.	-164.35	113.55	0000	→ 1 → 0 •			
٥	\$ 100°		115.57	0000		20.13.	9900	
000	-,0015	-<16.33	11/00	0000	60	•		•
80.05	8000	-218.00	119.03	0000.	- .03	188.57	0000	000-
54.14	5000.	-202-20	121.66	0000	••01	190.00	0000	00
4.15	2000.	-175.40	125.08	0202.	00.	196.62	0000) •
11.0	0000.	-144.67	125.71	0000	To.	50.75	6000	•
00.0	1000	-112.77	127.74	0000	10.	1,0.03	0000	000
60.0	.0001	-88.0U	124.17	00000	.02	198.71	0000	3 °
62.06	2000	57.05	151.79	0000	70.	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	0000	200
90.4	Э	-55,75	155,62	0000		4/ 707	0000	00.0
0.41	2000	13.611	135.05	0000	>0.			

SH SH I A S S A S F S

ı

-

	2 7 7	7774	DEFLECTION			DEFLECTION	
Š	2 -2502.04 5 -1260.15 6 -177.04		NUKRAL TO	GENOING BIREYT	9 9 14 9 -	NURMAL TO	BENDING
		(FT)	(INCHES)	(1Nex IPS)	(+1)	(INCHES)	(SAI New I)
		75.20	.0001	• 6 B 1	157.48	0000	10.
		70.07	1000.	1.56	139.91	0000	10
		72.49	.0001	5,02	141.93	0000	0.0
	•	75.02	2000	7,26	145.96	0000	.01
	1436.13	50.77	0000	7,913	145.40	0000	10
		74.08	0000	7,52	146.02	0000	10.
		M1.10	0000	6,52	150.04	0000	3
		65,13	0000	S. S. S.	152.07	0000	99
	4394.2	7	0000	3,95	_	0000	30.
	4454.51	87.19	0000	2,75	150.13	0000	90
		64.42	0000	1.76	156.15	0000	30
		41.44	0000	9.	160.18	0000	
24.35		95.27	0000	77	162.21	0000	30
•		95.30	0707	70.	164.24	0000	00
24	4 2549.16	97.53	0000	•.10	166.26	0000	00.
	-	86.49	0000.	67	168.29	0000	00.
	1	101.58	0000.		170.32	0000	∍
	995	105.41	0000	67.	172,35	0000	90.
# :	637.5	27°507	0000	•• •	174.37	0000.	90°•
	35/.46	101.	0000	0>0	1/0.40	0000	20.
	145	104.49	0000.	• 10	178.43	0000	00.
		111.52	0000	-13	180,46	0000	00
	90.	115.55	0000	- 10	182.49	0000	20.
		115.57	0000.	10.	1851	6000°	00.
100.	6193	117.60	0000	500	186.54	0000	30.
\$0.00		114.63	0000	£0°-	188.57	0000	00 -
	-161.96	121.06	0000	01	190.00	0000	00
		125,08	0000.	000	192.02	0000	20.
•		155.71	0000	70.	194.65	0000	00.
1000	10.201	12/./4	0000.	,01	190.08	00000	00
		129,77	0000	10.	190,71	0000	00.
	15.	151.79	00000	20.5	200.73	0000	200
00.	•35.6	153.62	0000	÷0.	202.76	0000	70
1000.	•	135.65	0000.				

		•		2 4 2 10	. PILE A	BISTOR		•	
1.51 1.55	NU. 1012	پ						- 9	
				- ACHH PLAT		E .			
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,		ECTION			DEFLECTION			DEFLECTION	
175		יורב יורב			ACK 10 7 1 1 1	GENOTES SE			BESCHAE
17.5 17.5		97	(IN-KIPS)	(F.T.)	(INCHES)	(IN-KIPS)	GE 13	LINCHEST	(Sellen)
1975 1974		1751	-1550.66	40.50	1000		7	000	0
11873 1239 84 72,499 1000 1000 1254 1000 1000 1000 1000 1000 1000 1000 10		1505	195.95	70.07	.000	-	1591	0000	9
		.1375	234.84	74.49	1000	5,65	141.43	0000	9
1000 1500	v -	1977	1234,68	72.62	0000	7,69	145.46	0000	0
1986 1988		-			0000	041/	•	0000	•
1986 4.275 7 48.13 100.00 5.56 155.00 155	3	•	3058.45	9.	0000	7.65	140.02	0000	.01
	7	.0666	\$755.00	7:1	0000	6.56	150.04	0000	00
	>	. US18	4204.19	3.1	0000	5.24	152.07	0000	20
1000 1000	av .	Э	4525.17	1.	•	06°E	154.10	0000	20.
			4566.16	7.1	•	49.5	150.13	000	90.
100 100		.0105	4510.30	٧.	0000	1.69	158.15	0000	0
		0108	5934,50	٧.	0000	26	100.10	0000	30 °
0010 2918.50 99.30000001 1068.2400000018 1366.84 101.35000031 1068.2400000018 1366.84 101.36000022 176.3500000018 1366.84 100.44000022 176.3500000018 126.35 100.44000023 176.3500000018 126.34 111.52 1000013 186.4600000018 -26.94 111.52 1000001 186.4900000018 -26.94 111.52 1000001 186.57 100000018 -26.94 112.57 1000001 186.57 100000018 -16.24 12.46 100001 186.57 100000018 -16.24 12.46 1000001 186.57 100000018 -16.24 12.46 1000001 186.57 100000018 -16.24 12.46 1000001 186.57 100000018 -16.24 12.46 1000001 194.65 100000018 -16.24 12.46 1000001 194.65 100000018 -16.24 12.46 1000001 194.65 100000018 -16.24 12.46 1000001 194.65 100000018 -16.24 12.46 1000001 194.65 100000018 -16.24 12.46 1000001 194.65 100000018 -16.24 12.46 1000001 194.65 100000018 -16.24 12.46 1000001 194.65 100000018 -16.24 12.46 1000001 194.65 100000018 -16.24 12.46 1000001 194.65 10000		1500.	3453.58	٧.	0000	• 30	162.21	0000	00.
1000		• ·	2918.50	٦,	0000	0 ·	164.24	0000	00.
		200	2571.74	•	0000	12.	166,26	0000	00.
0044 1305,44 101,56004029 172,3500400041 991,88 105,44004029 176,4500400041 329,39 107,44004025 176,4000400041 329,39 111,52004017 176,400040004226,99 111,52004017 176,4000400042123,48 111,52004007 184,5100400042123,48 117,50004003 184,5100400042124,24 121,65004004 184,6500400042154,24 121,65004004 184,6500400042154,24 121,65004004 184,6500400042154,24 121,65004001 194,6500400041154,24 121,65004001 194,6500400041154,24 121,65004001 194,6500400041154,24 121,65004001 194,6500400041154,24 121,65004001 194,6500400041154,24 121,65004001 194,6500400041154,24 121,65004001 194,6500400041154,24 121,65004001 194,6500400041154,24 121,65004001 194,6500400041154,27004001 194,6500400041154,27004001 194,6500400041154,27004001 194,6500400041154,27004001 194,6500400041154,27004001 194,6500400041154,27004001 194,6500400041154,27004001 194,6500400041154,27004001 194,6500400041154,27004001 194,6500400041154,27004001 194,6500400041154,27004001 194,6500400041154,27004001 194,6500400041154,27004001 194,6500400041154,27004001 194,6500400041154,27004001 194,6500400041154,27004001 194,6500400041154,27004001 194,6500400041154,27004001 194,6500400041154,270040004000400041154,270040004000400041154,2700400040004000400041154,27004000400040004000400041154,270040			1446.95	64.55	0000	•,31	166.29	9000	00.
004/ 991.86 105.44000029 172.3500000041 120.94 109.44000017 170.4500000041 120.94 111.52000017 170.430000004220.94 111.52000017 170.430000004220.94 115.57000001 180.510000004220.64 115.57000001 180.540000004220.64 115.57000001 180.540000004220.64 115.57000001 194.570000004220.64 115.57000001 194.570000004220.64 123.56000001 194.570000004220.64 123.56000001 194.550000004220.64 123.56000001 194.550000004220.64 123.56000001 194.550000004220.64 123.56000001 194.550000004220.64 123.56000001 194.550000004220.64 123.56000001 194.550000004220.64 123.56000001 194.550000		****	1306,44	101.58	0000	55.	170,32	0000	00
0041 329.34 176.4001017 176.43000003 186.510000013 186.54000003 186.54000003 186.54000003 186.51000003 186.51000003 186.51000004 186.51000004 186.57000005 186.57000		1000	471.86	4.50	0000	62.	172.35	0000	00.
			4.00 K				174.57	0000	0 0
003> 120.94									
00225.99 111.52000015 180.460000		.0035	120.94	67 601	0000	17	176.43	9909	03.
0016 -176.20 115.57000007 184.51 .0000 0011 -200.41 117.6000004 184.51 .0000 0017 -200.24 121.66000001 192.620000 0004 -184.24 121.66000001 192.620000 0000 -150.24 125.71000001 196.690000 0001 -73.62 129.77000001 196.710000 0001 -73.62 129.77000001 196.710000			-56.99	111,52	0000	\$113	160.46	0000	00.
001		>>00.00 	165,46	115,55	0000	010	162.49	600 0	000
0007 -200.24 119.63 .000003 188.57 .0000 101. 190.60 101. 190.60 101. 190.60 101. 190.60 100.00 190.60		1100.	-1/0.A1	117.60	0000	000	180.54	0000	
		9	96 U16	14 311	0000	10	7 7 7 7	4 4 4	•
0000 -159.24 125.71 .000000 192.62 .0000 0000 -150.25 125.71 .0000 .01 194.65 .0000 0001 -73.62 129.77 .0000 .01 196.71 .0000 0002 -50.33 131.79 .0000 .01 204.75 .0000		7000	120000	121.06			09.061	0000	
0000 -150.25 125.71 .0000 .01 194.65 .0000 0001 -73.62 127.77 .0000 .01 196.71 .0000 0002 -50.33 131.79 .0000 .01 196.71 .0000		.0002	-159.24	123.08	0000	00.	192.62	0000	00
.0001 -73.82 124.77 .0000 .01 196.71 .0000 .01 .0000 .0000 .001 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000		0000	-130.25	17.521	0909	10.	194,65	0000	30.
.0000 -73.82 129.77 .0000 .01 196.71 .0000 .0002 -50.33 131.79 .0000 .02 204.73 .0000 .0002 -31.15 133.62 .0000	9	000	-100.95	127,74	0000	100	190.08	0000	000
.0002 -50,33 131,79 .0000 .02 204,73 .0000 .02 202,76 .0000	4	.000	-13.82	124.17	0000	.00	196.71	0900	99
.0000 -51.15 135.62 .0000 .02 202.76 .0000 .02 1000.		2000	-50,33	31,7	0000	20.	204.73	0000	000
	1 0 -	200	31.15	35.0	0000	~ 6	202.76	0000.	90°0

!
1
n.
1

	UEFLEGTJUN			DEFLECTION				
PILE	NUKHAL TU	BENDING	3-11-d	NURMAL 10	BROING		OF JAMON	5 10 N N S N S N S N S N S N S N S N S N S
LENGTE SANS		SCERPT CONTRACT				(14)	(INCHES)	(Set les)
00	6640.	-927.54	90.00	.000		00.761		
2.03	0110	-552.55	70.47	0000	1 600	129.04	0000	- 1 n d
•	0240.	205.51	12.49	0000	4 1 ° 6 '	5		
. c	0550.	730.77	15.02	0000	30°0	145.46		
=	### O .	1208.10	17.05	0000	3,68	145.99	0000	000
7	649.0	16/9/17	E3 - 52	0000	3,52	148.02	0000	200
2.17	10 N N N N N N N N N N N N N N N N N N N	26.0371	91.10	0000	2,95	150.04	0000	20.
61.4	0220	2137.15	83.13	0000	2,30	152.07	0700.	30°
6.42	.0102	2194.60	85.16	0000	1000	_	0000	99
6.25	0113	2139.09	87,19	0000	1,13	156.13	0000	20
				4	4	15.		
V	V	32°/77'	7 · 6		0 1		2000	
25.50	0.00	10.16.71	1000	0000		162.21	0000	20
2 4	7000				30 1	164.24	0000	00.
2 3		00.000	20.00			160.26	0000	00
		50.0501						
.4.	*100*	788.39	44.55	00000	• 15	168.29	0000	20.
37.	-,0042	571.54	101.38	0000	-, 15	170,52	0000	00
34.47	\$200.	385.91	103.41	0000	7.1	172.35	0000)) •
2	0041	253,95	105.44	0000	12	174.37		00
30.54	.0016	115,20	107.46	0000	600	176.40	0000	000
46.04	0016	27.34	104.49	0000	07	178.45	0000	30.
62.28		-33.37	111.52	0000	•00	180.46	0000	00
4.01	.0010	-71.34	115.55	0000	70.	182,49	0000	30.
70.0	1000-	-91.19	115.57	0000.		184.51	00000	•
00.	\$000.	-47.39	117.60	0000	5 0 -	186.54	0000	00.
20	£ 0.00°	00.50	119.03	0000	-,01	186.57	0000	00.
7	7000	C5.55-	121,06	0000	00.	190.60	0000	00.
54.75	1000	-71.55	125.08	0000	00.	192.62	0900	20.
11	0000	-57.46	125.71	0000	20.	104.65	2000.	20.
56.00		-43.70	127.74	0000	001	190.08	0000	00.
20.	1000	-51.27	129,77	0000	10.	146.71	0000	00.
05.00	1000	-20.72	151,79	0000	601	200.13	0000	00.
000	1000	=12.28	133.02	2202.	10.	405.76	0000	00.
	1000	10.5	135.65	0000	70.			

4110	NING ALL	A S A D I A C	4110	NET TO THE TANK THE		2	MIDNA: 40	200 100 100
F 10 1 1	716	RUMERT	1 5 5 6 1	7116	1010E	LESCIE	PILE	ACAR'S
(61)	(INCHES)	(Salvent)	(F7)	LINCHEST	(IN-KIPS)	(6.1)	(INCHES)	(IN-KIPS)
0	5010.	-1155.47	40.00	10000	-1.73	137.88	0000	10.
. 50	\$000		74.47	0000	7	139.91	0000	10
•	1950.	-<3.62	14.49	0000	2.75	141.93	0000	30.
0.0	0.500	501.84	75.02	0000	W. 40	143.95	00000	200
4	3 3 4 5	10001	9		, F	1 2 -	6	•
2,17	1		0 - 2		10°0	20.021		
01	.0212	1434.95	85.13	3000	2.19	152.07	0000	000
27.9	1010.	2011.47	65.10	0707.	1001	154.10	0000	
\$5.	0110	1979,22	87.19	0000	1.09	150.13	0000	00
۴۶.	1/00.	1869.72	89.22	0000	197	A	0000	
22.50	0,000	•	91.64	0000	58.	160.18		90
24.35	.0017	1460,11	93.27	0000	51.	162.21	0700	00
40.30	.0001	1222,12	95.30	0000.	- 05	164.24	0000	00.
. 59		463,36	97,33	0000	91.5	166.29	0000	90.
14.	4.0017	757.30	94,35	0000.	14	168,29	0000	00
34.44	0200.	553,68	101.38	0000	.14	170.52	.0000	00
74.55	1,000	578.24	105.41	0000	.13	174.35	0000	33°•
20.00		223070	107.50	0000		174.57	000	ີ
	,,,,,,	150.03				0.000	9000	00.
\$\$.	-, 0015	35.24	109.49	0000	07	176.43	0000	00.
8.50	0012	00.42-	111.52	0000	- 05	180.40	0000	100
	7000	0.00	115.55	0000	~ ^	185.49	0000	3 °
0.00	\$000	45.64	11/00		200	166.54		20
>	\$000.	-87.1%	119.63	0000-	• 01	186.57	0000	20.4
52.14	5000°	-7A,96	121.66	2200	00	140.00	0000	30.0
54.75	1707.	-67,41	123.68	0000	00.	192.62	0000	25.
56.17	0000	-54.51	125.71	0000	00•	194.65	0000	30.
2	0000	-41.75	127.74	0000	100	140,08	0000	90
.05	1000.	-50,13	129.17	0000	10.	196.71	0000	90.
96.29	1000.	-40.19	131.79	0000	101	400,73	0000	000
00.10	1000.	-12.17	155.62	0000	10.	202.16	0000	20.
16.	1000	6.0	135.45	0000	10.			

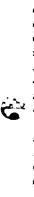
BENDING MUMENT SATER 22222 55233 3333 300 300 3 PAGE DEFLECTION NORMAL TO PILE 0000 00000 0000 0000 0000 0000 000000 00000 (INCHES) PILE LENGTH (FT) 141.93 146.02 150.04 152.07 154.10 156.15 160.18 162.21 164.24 166.26 156.29 170.32 172.35 174.37 188.57 190.60 194.62 194.68 182.49 184.51 200.73 137.68 78.43 U.S. NAVY . ACM PLATFUMS . FAITGUE ANALYSIS . MLM 105,0 FEET BENDING MUMENT (IN-KIPS) 50° 2000 40.10 200 0000 00000 00000 # 0 0 0 0 0 0 0 0 0 0 0 0 0 0 111158 111358 111555 P16 LENG1H (FT) 101.58 105.41 105.41 119.03 121.06 125.08 127.71 70 47 77 49 75 49 75 69 44.08 93.27 755.45 544.51 572.44 113.50 -974.74 -414.29 129.50 640.78 1104.05 1513.61 1864.45 2015.21 2074.71 30.01 119.00 111.90 (SdT xerT) 1697.15 1705.24 1476.16 1250.62 BENGING 29,13 10.00-NURAL TO PILE (INCRES) V 0000 11100 0000 0000 0000 0000 0000 .0758 .0500 .0347 .0150 0850 -.0015 PILE JUINT NU. 1012 LENGTH (FT) WWW. WWEEE 40.33 42.33 44.03 2011 56.15 56.15 56.15 10.00

		C. G. NAVY	- ACHK PLATE	TIKHS - FALLGUE	ANALYSIS - MLM	105.0 FEET		
	ULFLEGIION			DEFLECTION			DEFLECTION	
1 1	-	BENDING	9116	NUKHAL TU	BENDING	PILE	NURMAL TO	BENDING
	716	NOT NOT NOT NOT NOT NOT NOT NOT NOT NOT			ECEMENT.	1 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	PILE	NUMBAT
1	•	7catuant 7		Tricue 37	TOLI WOUTH	1111	LINCHESS	CENTRALI
00.0	0.000.	0	77.90	4000.	60.44	137.88	0000	70
2005	15156	-3457.90	70.07	.0003	-16.78	139.91	0000	50
\$ C Q	0197	_	12.49	£000°	3.41	141.93	0000	5 0
•	4024	1513.70	75.02	2 000°	15.42	143.46	0000	50.
11.0	. 1510	450 . 1	77.45	10001	21,21	145.99	0000	70.
0.14	8742.	6241,35	74.05	.000	22,61	148.02	0000	70.
2117	1725.	8481.52	81.10	0000	21.17	150.04	0000	10
4.14	***	10244.72	85,13	0000	18.13	152.07	0000	10
>,44	.1508	11541.61	62.16	0000	14.45	154.10	0000	70
3.25	1105	12447,04	R7.19	0000	10.71	156.13	0000	70
₹0°5	5600	12003.28	57.48	0000	7.36	158.15	. 0000	90
22,30	\$7500	14216.74	91.6	0000	. 3 . 0 . 0	100	0000	
24.35	.0351	11359,50	93,27	0000.	5,45	164.21	0000	00
9.50	.0179	10072,20	95,50	00000	693	104.64	0000	200
95.5	7500.	8560.01	97,33	0000	40.0	166,26	0000	00.
30.41	0032	7021.04	•	0000.	04.	166,29	0000	00.
777	1000.	5505.27	101.58	0000.	* B B 3	170,32	0000	20
77.75	9110.	4110.00	105.41	0000	- 83	172.55	0000	20.
).	0127	2888.99	105.44	•		174.57	0000	200
9.56	•	₹.	7.4	0000	79.0	170.40	0000	000
40.55	0113	1049.07	104.49	0000	24.	178.43	0000	00
2.28	8500.	42H.05	111.52	0000°	2244	180,45	0000	30
~ •	0000.	.15.9	113,55	0000	¥5.	182.49	0000	00.
٠	3	30B.4	115.57	00000	٦	4.5	0000	30°•
0	700	-4/7.41	117.60	0000	-19	186,54	0000	0000
>0.0¢	0032	-552.10	119,63	0000	.,13	186.57	0000	00.
2.12	.0021	-557.43	121.06	0000	90	190,60	0000	00
٠/٠	7100.	-510.44	123.08	9900	30.	194.62	0000	00.
2.11	•	8 7 7 °	155,71	0000	••01	194.65	0000.	?0.
20.00	. 0001	- 568.10	167,74	0000	101	190.68	0000	00.
\$0.0	₹000•	285.9	124,17	0000	50.	146.71	0000	00
5.05	#000°	5.60	~	0000	a 0.3	400.73	0000	20
0	3000	3	135.82	0000	70	202,76	0000	00.
	3000°	ć	'n	0000	70			



SISTICE ANDICE SANTS

	UEPLECTION			ָר היי	LECTION	• • • • • • • • • • • • • • • • • • •	DEFLECTION	
7 L L	NOWAAL TO	HENDING HE	PILE	NURMAL 111	SENDING.	PILE	NURMAL TU	BENDING
2	(INCHES)	(SdTy=vI)	(FT)	(INCHES)	(SdIX=71)	(F1)	(INCHES)	(SATY=NI)
0000	.5512	ナヘ・レナーレー	37.80	5000°	-45.25	157.68	0000	\$0.
20.5	4440	41.4554.	70.47	\$000.	-16,68	154.91	0000	50.
Ø :	. 4523	-1457.49	12.40	\$000°	5.46	141.45	0000	₹0 .
0.0°	1145.	ar 🗆	2	2000	13.92	145.46	0000	70.
11.	- 55055	5120.42	77.05	1000.	19.52	145.49	0000	70.
2 1 4	6050	5540,55	74.08	1000.	16.02	148.02	0000	70
17.	. 2551	1676.32	41.10	0000	4.7	0	•	
51.1	1306	לבסיר בט	F5.13	0000	15.46	152.07	0000	001
0.24	.1694	10409.25	45.16	0000	13,55	154.10	0000	3
10.25	.1145	11624.80	87.19	0000	10.09	150.15	0000.	00
82.05	7000	11407.44	52.48	0000	96.4	158-15	. 0000	30
<2.50	0750.	11565.52	91,24	0000	4.36	7	0000	3
۲۳۰۶۶	\$450	100/0.54	45.27	0000	2, 35	162.21	0000	00.
٠ \$٥	7	17.3	л	0000	26.	164.24	0000	00.
55.	5500.	8082.75	97.53	0000	••01	160.26	0000.	00.
50.41	0027	0966.90	94.35	0000.	5 C -	166.29	0000-	33
32.44	5/00°	5200.44	101.38	0000.	91.6	170.52	••0000	30
34.47	610/	5840.35	105.41	0000	•.76	172.55	0000	70.
56.50	•	2/41.20	105.44	0000	. .68	174.37	0000	00.
ا	0116	1774.00	101.46	0000	95.	176.40	0.000	00.
40.55	• 0100		104.49	0000.	64.	170.45	0000	00.
£2.	~x00.	420.31	111.52	0000	17.	140.46	00000	0.0
64.01	5/00.	50.	115.55	0000.	••32	156.44	0000.	no.
70.07	6500.	-474.35	115.57	00000	# Z - #	184.51	0000	ာ း
6 D • E	***************************************	\$\$.077=	117.60	0000.	• 18	186.54	0000	000
¥0.08	0051	-516-74	119.05	0000	-,12	140.57	0000	30.
56.16	0700.	7x - 21 S =	121.06	6000.	10	190.00	0000	0.0
54.15	1100.	-463.26	125.08	0000	70.	194.02	0000	00
	.00.		17.521	0000	10.	•	0000	00.
30.	1000.	15.55.	127,74	0000	• 01	196.64	0000	00.
50.0	2 000•	-269.35	124.17	0000	\$0 .	198.71	0000	00.
46.54	\$000.	1147.38	151.19	0000	£0.	200.73	0000	7.0
54.03	7000	-155.65	135.02	0000	• 0.5	405.76	0000	00.
-	0.000	44	11 17 -	0000	76			



Carter C									
		DEFLECTION			DEFLECTION			DEFLECTION	:
10 10 10 10 10 10 10 10	ָ רַג	DI JAMADA	SENCE NE	7176	NURMAL 1D	BENOING BENOING	716	-	BENDING
1900	E .	, ורני הייני	とのでは、	I S S S S S S S S S S S S S S S S S S S	716	TOWERS.	T SE SE SE SE SE SE SE SE SE SE SE SE SE		MUNENT
1970 1970		2012	Contract 1	- (11)	7636361	(Call seal)	71.47	n	- CONTHENTY
1500 1500	0000	_n	0.49.1	ar. Do	4000	05.13.	157.68	0000	70
1310	2.05	つかいす。	532.	70.47	0003	e13.70	139.91	0000	50
. 1310	4.00	7957	441.	72.49	£000.	4,93	141,93	0000	\$0.
1110	6. ca	3695.	1500.42	75.02	2000.	S	145.46	0000	£0.
1,000	11.0	.3310	416.	21.05	10001	0	145.99	0000	70.
1	9,40	6046	1201.77	70.08	1004	10.10	CO. ## 1		3
1000 17.50	717	0252	8517.71		0000		70.071		
11 12 12 12 12 12 12 12	7	.1671	10025-47	65.13	0000	17.20	152.07	0000	
	6.42	5077.	11280.92	85.16	0000	13.64	154.10	0000	
- 1124	6.45	.1100	40007	67,19	0000	10.05	156.13	0000	30
	;	1		i					
1174 1174 25 0 0100 24 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	, o . c	0020	Æ,	84.85	0000	6.85	156.15		•
			11764.58	91.64	0000	4.21	150.18	0000	000
**************************************	4.55	9150.	0196.	45.47	0000	2.20	164,21	0000	90.
	95.0	• 0150	4555.0¢	95.50	0000	97.	164.24	0000	90°•
**************************************	9.34	0700.	Đ	97,53	0000	••13	166,26	0000	00.
		=	14 1084	20		14 -	14.		•
	7	7000	76.34.5	101.58			170.67		
0119 174.370119 170.390119 170.390109 35.97	13.7	.0114	3360.07	105.41	0000	12.	172.35	0000	30
0119 1/01.99 109.49000062 176.45009333 182.49 111.52009024 182.49 184.45009024 184.45 115.57000024 184.45 115.57000017 186.59 184.510019017 186.59 184.510019017 186.57 186.570019017 186.57 194.650010017 186.57 194.650010017 186.57 194.650010017 186.57 194.650010017 186.57 194.650010017 186.57 194.650010017 186.57 194.650010017 186.57 194.650010017 186.57 194.650010017 186.57 194.650010017 185.65001001	0.50	0165	2004.05	107.44	0000	72	174.37	0000	00.
2.550093 557.06 111.52 .000033 180.45 180.45 180.0033 180.45 180.45 180.0033 180.45 180.45 180.0033 180.45 180.00324 180.55	9.52	0119	1701.99	107946	0000	-,62	176.40	0000	20.
0.004 357,04 111,52 9000 -33 180,46 0.007 -331,92 115,55 9000 -33 182,49 0.007 -331,92 115,55 9000 -33 182,49 0.008 -341,92 117,50 9000 -32 180,45 0.009 -341,92 117,50 9000 -32 184,51 0.009 -347,53 114,62 -0000 -01 196,50 0.009 -347,73 121,60 9000 -03 194,65 0.000 -347,73 127,74 9000 03 204,73 0.000 -347,73 135,42 9000 03 204,73 0.000 -000 -03 204,73 204,73 204,73 0.000 -000 -03 204,73 204,73 204,73 0.000 -000 -03 204,73 204,73 204,73 0.000 -000 -000 -000 -000 -000 0.000 -000 -000 -000 -000 0.000 <td>4</td> <td>1</td> <td>•</td> <td></td> <td>3</td> <td>;</td> <td>;</td> <td></td> <td>į</td>	4	1	•		3	;	;		į
0.00		0000	•			30 ° 0	75.07.1		
0.00 - 24.04 115.57 110.00 124.51 184.51	J J	2 an	20			27.61	CH CH .	1000	200
0.00 -0.00 -5.57.53 119.03 .0000 -1.2 186.54 190.00 121.00 -0.02 190.00	۰	2400	9117		0000	10 C - 1	2 2 2 2		
2.75 = .0019 -537.53 119.63 .0000 -012 188.57 199.60 2.76 = .0013 -443.84 123.66 .0000 -013 192.62 0.77 = .0014 -426.17 125.71 .0000 -013 196.65 0.00 = .000 -01 196.65 0.00 = .000 -01 196.65 0.000 -01 196.71 0.000	5000	474.1	117.00	0000	17	186.54	0000	000	
2.72 = .0019 = .536.84	9	0500.0	57150	9	0000	61.9	- S - S - S - S - S - S - S - S - S - S		
0.01 001 002 003 192.62 0.00 000 000 194.65 194.65 0.00 000 00 194.65 194.65 0.00 000 00 194.77 0.00 0.00 194.71 0.00 000 00 0.00 <	. ~ı	5100.	75.05S		0000	0.7	190.60	0000	300
6.00 000 00 194.65 6.00 000 00 194.65 6.00 000 00 124.77 6.00 000 00 00 6.00 000 00 00 6.00 00 00 00 6.00 00 00 00 7 000 00 00 6.00 00 00 00 6.00 00 00 00 6.00 00 00 00 7 00 00 00 7 00 00 00 8 00 00 00 9 00 00 00 8 00 00 00 9 00 00 00 9 00 00 00 9 00 00 00 9 00 00 00 9 00 00 00 9 00 00 00 9 00 00 00 9 00 00 00	3	1100.	-473°#4	3.0	0000	50.	192.62	2007	20
0.00 = .0000 = 347.73 127.74 .0000 .03 196.65 10.00 .03 196.71 .0000 .03 196.71 20.02 .03 200.73 200	٥	7000.1	-426.17	2:5	00000	20.	194.65	0000	20.
0.05 .0002 =266.59 124.77 .0000 .03 198.71 2.05 .0004 -195.50 131.79 .0000 .04 202.75 4.07 .0004 -152.45 135.62 .0000 .04 202.76 5.41 .0004 -81.17 135.65 .0000	10	0000	347	7:7	0000	0	196.68	0000	000
2000.73 4.000 .0004 -152.45 135.42 .0000 .04 206.76 6.0004 -61.17 135.45 .0000 .04	9	2000	10	2	0000	£0.	198.71	0000	90.
4.65 .0004 -152.45 135.82 .0000 .04 206.76 .0004 .04 206.76	5. ℃	7000.	S	131,79	0000	£0.	200.73	0000	30
0000 ° 00	,	7000	J	135.62	0000	70.	404.76	0000	00
	.	**************************************	•••	135.65	0000.	0		•	•

i

1

1

ŧ

ı

F

1

1

1

1 . 1

(

1

1, 3, NAVY = ACM PLATONING = PAITON EMAILS = MLW 103, PEEF 10/45/78 10/	10.3				•	• . ! # .			
1.3 ANVY = ACM PLATFOURNS = PLATFOLNG ANALYSIS = PLATFOLNG PREF DEFLECTION DEFL	1,			4 2 -	• • • • • • • • • • • • • • • • • • •	~			
	1			- ACHK PLA	SUNTE - PATION	•	105,0 FLE		ì
C C C C C C C C					DEFLECTION			DEFLECTION	
1			SEND LAG	P 1 C F	NURTAL TO	GENOLNG BORFFT	7 - 7 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	NUKAL TO	GENOLNE BORFET
11	11	į	30 T X = N T	(FT)	(1)Cres)	(14-K1P9)	(F1)	(INCHES)	(SALKAL)
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	1		€	70.00	.0001	-2.60	137.68	0000	70
77.75	72, 49 73, 40 74, 40 74, 40 74, 40 74, 40 74, 40 75, 40 76, 40 77, 40	- 1	-566.00	70.27	1000.	1,73	189.91	0000	100
77, 16	1,		00.07	66.27	0000	22.0	50.101	0000	~ ·
14.10 15.14 16.14 16	11 12 12 12 12 12 12 12		1501.05	77.05	0000	5.00	145.99	0000	00
95.13 95	1		£105.5£	• •	0000	•		. 0000	30
# # # # # # # # # # # # # # # # # # #	11,15		2404,28	~	0000	4,25	150.04	0000	20
1	1		4416.67	٦.	0000.	3,34	152.07	0000	90.
1	10		1.000	-: -	0000	57.	154.10	5000°	3 : o
7.2	71			:					2
1	1		28.945	٠,	0000	1.02	158.15	0000	
1	1		2711.66	71.64	0000	25.0	160.15	0000	200
44 94.55	41 99.45		1000	95.50	0000	30.	164.24		
77 101.36	77 101.36 0000 122 170.32 000 00 1 170.32 0000 00000 00000 00000 0000 00000 00000 00000 00000 00000 00000		1502.46	97,33	0000	• 10	166.26	0000	000
101.	77 101.56		156	٠,	0000.	~	166.29	0000**	•
105-44	100. 1005.44		644.77	101.58	0000	22	170.32	0000	00
10. 107.44 .0000 .114 170.45 .00000 .00000 .00000 .00000 .00	10 10 10 10 10 10 10 10		570.46	5 0	0000	•10	172.35	0000	200
111.52	113.55		Λ Λ	107.44	0000	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	174.57	00000	3 7 3 0 • 1
111.52	111,52		52,58	57.501	0000		176.43	6900	00 -
115.55	115.57000001 184.51000		-57.74	111.52	0000	90.	180.46	0000	20.
115.57	115.57		C0.56.	115.55	0040.	90.	142.49	2200	30.
46 119,63	40 119,63 .0000 .01 100.57 .0000 .0000 .000 .0000 .0000 .0000 .0000 .000 .0000 .000 .0000 .000 .0000 .0000 .000 .0000 .00		-156.86	115.57	000	70.1	104.11	0900	3 3 3 3 3 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
121.66 0000 124.62 0000 125.74 0000 001 146.62 0000 127.74 00000 001 146.71 0000 001 146.71 0000 001 146.71 0000 001 146.71 0000 001 146.71 0000 001 146.71 155.65 0000 001 166.66 001 167.74 185.65 0000 001 185.65 185.65 0000 001 185.65	121.00	1	*	14 000	4				
04 123.66	31 125.71		I	171.00	00000		04-104		
45.77 125.71	45.94 124.77	i	-105.04	123.08	0000	90	194.62	0000	200
45.96 124.77 .0000 .01 146.71 .0000	45.96 124.77 .0000 .01 146.71 .0000 .00 50.79 131.79 .0000 .01 200.73 .0000 .00 15.94 153.62 .0000 .01 202.76 .0000 .00		20	175.71	0000	10.	194.65	0000	20.
\$6.74 121.79 .0000 .01 140.71 .0000 \$6.74 131.79 .0000 .01 200.73 .0000 155.62 155.62 .0000 .01 202.76 .0000 -9.23 135.85 .0000	45.96 124.17 .0000 .01 146.71 .0000 .05.79 131.79 .0000 .01 200.13 .0000 .01 200.73 .0000 .01 200.73 .0000 .01 202.79 .0000		3	127.74	0000	10.6	140.06	00000	000
15.74 131.79	131,79 131,79 .0000 .01 204,79 .0000 .01 204,79 .0000 .01 204,79 .0000 .01 204,79 .0000		80.57.	124.17	0000	10.	146.71	0000	3 0 • •
14.54 155.62 .0000 .01 202.76 .0000	19,54 155,62 .0000 .01 204,76 .0000 .0.1 .0.23 135,85 .0000 .0.1		-50.79	131.79	0000	001	200.13	0000	00.
			~ I	155.02)))) •	100	407.70	0000	30.
		1							



	PILE NUMBAL 10 LENGTH PILE (FT) (INCHES) 137.86 .0000 134.91 .0000	
	to	00 PO 1 2 C
		(INeKIPS)
10000		10.
10000		0
0000. 0000.		10.
0000.		10.
1412.35 141	145.99	00
	0000** 20*981	30
	;	20
	; 	30.
		00.
**************************************		00
	91 HS1	111
		•
		90.
0015 1451.13 99.43 0000 0050 359.81 101.38 0050 359.81 105.41 0000 0050 357.00 105.41 0000 0050 357.00 105.41 0000 0050 357.00 109.49 0000 0015 05.54 115.54 100.00 0010 05.54 117.55 0000 0010 05.54 117.63 0000 0000 012.64 117.63 0000 0000 012.64 117.63 0000 0000 012.64 117.63 0000	164,24	000
0026		0.0
	168-29	00.
	•	00
105.45 104.45 105.05		200
100000		00.
	176.40	000
001765.20 1115.520000 001515.22 115.550000 0002167.41 117.000000 0004165.54 117.030000 000194.47 125.000000 000194.47 125.000000	178.43	90.
0010 -115.52 115.57 .0000 0010 -125.741 117.60 .0000 0014 -125.74 117.63 .0000 0014 -14.74 117.63 .0000 0014 -14.74 121.66 .0000 0016 -69.47 125.71 .0000		90
010 -115.24 117.60 .0000 0107 -125.74 117.63 .0000 0004 -114.74 121.06 .0000 0001 -94.47 125.06 .0000 0001 -80.06 125.71 .0000	•	20.1
0004 -125.74 117.63 .0000 0004 -114.74 121.06 .0000 0001 -47.74 125.86 .0000 0001 -80.08 125.81 .0000		30.
	186.54	00.
	186.57 .0000	9 C
		00
0000. 17.55. 10.00. 0000. 0000. 0000. 0000. 0000. 0000.		00.
0000.		00
	196.68	100
• 0000	146.71	00.
2.00 .0001 -50.27 151,79	200.73	00.
• 0000° 29.551 - 1000° 20.5	202.16 .0000	9 . .
• 0000• 55		

	PAGE	DATE
8 1		
A L Y 8		
F 2		
Z 4		
•		
	•	
	TOLITON NO.	1101
	21120	72 121

ANGEL STANDERS, REFERENCE LEGISLAGE SLOTERS UNISSELLED FINITALION

	DEFLECTION	**************************************	•	DATE TALLED	. AMALTULU I BER	10300 1661	OFFLECTION	
P.1.6	NUMBE 10	BENDING	9.0	NURNAL TO	BENDING	PILE	NURBAL 10	BENDINE
(+1)	(10CHES)	(Setten!)	CFT)	(INCHES)	(INSKIPS)	CF T)	(Inches)	1045N1 (1041P6)
2	.1076	-1041,41	70.00	1000	-3.01	137.68	0000	10.
3	コピケコ マ	-401.94	70.47	1000	1.26	6	0000	10
40.3	£ + £ 0 .	-150.41	12.99	0000	3.76	141.93	0000	10.
•	.0731	600.21	75.02	0000	26.4	143.96	0000	10.
=	/100.	1242,07	77.05	0000	5.15	145.49	•0000	00
77.	\$250°	1412.35	79.08	0000	4.77	146.02	0000	30
12.17	1000	2407.75	41,10	0000	4.06	150.04	0000	00
4.14	.0515	35.53</td <td>85.13</td> <td>0000</td> <td>3,21</td> <td>154.07</td> <td>0000</td> <td>30</td>	85.13	0000	3,21	154.07	0000	30
2	. 0255	24/3.15	62.10	C 2 2 2	2,38	154.10	0000	00
6.25	00100	Z248.00	87.19	0000	1.03	150.13	- 0000	00
9	90.0	10, 9564	27.04			31 751		
22.50		100 1/11 Y	77.10		• 3 • 0 • •	4-04-		900
44.35	0000	4154.77	95.27	0000	02	162.61	0000	30
26.36	5000	オティオテトロ	95.50	0000	200	164.20	0000	00
25.	. 0015	1451,15	97,53	0000	-14	160.46	0000	00
17	0025	1123.58	55.99	0000	97.	168.29	0000	90
52.44	B 000 -	825.77	101.38	0000	02.4	1	0000	20
34.47	0500.	509.61	105.41	0202	97.0	172.35	0000	30
\$6.50	*. UO 28	357.00	105.44	0000	•.16	174.37	0000	00
55.0	-,6065	164.88	107.46	0000	.,13	176.40	0000	00.
Ş	\$ \$00 °	92.62	104.49	9000	01.0	178.43	0000	00-
44.34	0017	\$2° 47	111.52	0000	200	97.71	0000	00
44.01	\$100.	-65,54	115,55	0000	90	186.49	0900	30
70.07	••010	-115,24	115.57	0000.	30 .	184.51	0000	30.
90	10000	-127,41	117.00	02000	••03	186.54	0000	900
50.	4000	-125.04	119.03	0000.	10.	186.57	0000	00.
54.14	>000.	-114.00	121.06	0000	01	190.00	0000	00.
54.15	1000.	73.EV	125.08	0000	30	192.62	0000	2
_	0000.	90.00	125.71	0000	10.	194.65	0000	06.
5.	1000	-61.66	127.74	0000	0.01	196.68	0000	00.
40.0	.0001	44.22-	124.77	0,000	10.	146.71	0000	90.
05.50	1000	-50.27	131,79	0000	100	400.73	0000	00
00.10	1000°	•	155.62	0000.	100	204.76	0000	22.
~	1000	17 9 E	3 X 3 Y -	0000	10			

WINTIES STRUCTS AND

E33352 Sec. 1997

1		U.S. NAV	U.S. NAVY . ACHR PLATE	FURMS - FAITFUE	ANALYSIS .	MLW 105.0 FEET		41.75.111
	URFLECTION			DEFLECTION			DEFLECTION	
PILE	NUMBAL TO	SENU 1.16	PICE	NUMBAL TO	BENDING	PILE	NURMAL 10	BENDING
(FT)	(1.6.063)	(Settent)	CF T)	CINCHESS	(INSKIPB)	CFT)	CINCHES	(INSKIPS)
3	. 1100	-1640.17	36.06	1000	.2.80	137.68	0000	10
2.05	プロウつ ·	-712,01	70.47	1000		186.651	0000	0
	9997	10.84	72.49	00000	5,47	141.43	0000	130
9.00	V470.	172.45	72.02	0000	5.11	143.46	0000	1°.
	, 00¢	1440.04	77.05	0000	5,30	145.99	0000	000
77.	0150.	4055.21	19.08	0000	99.7	146.02	0000	00
12.17	2100	2550.45	81.10	0000	4,14	100.00	0000	30
14:10	21500	2855.81	83.13	6000	3,27	152.07	0000	30.
97.0	. 0256	2417.18	62.16	0000.	2.41	154.10	0000	200
\$5.	0100	2957.06	8/.19	0000	1.04	156.13	0000	000
62.05	0717	2704.40	44.22	0000.	1,01	158.15	0000	90
42.50	2000.	2502.41	91.64	0000.	. ç ç	160.18	0000	•
. 35	1700.	4178.81	93.27	0000	91.	166.21	0000	20.
20.50	₹ 000.	1820.72	95.50	0000	£0.	164.24	0000	00.
27.	0015	1472.47	91.53	0000	-, 15	100.26	0000.	200
30.41	0025	1156.30	55.44	0000		168.29	0000	30°•
77	0.00.0	055.90	101.54	0000	21	170.32	0000	000
34.41	.0031	571,01	105.41	0000.	÷1.	172.55	0000	30.
30.00	**00°•	324.40	105.44	0000	_	174.37	0000	20.
56.56	•••••	164.54	107.40	0000	• 13	176.40	0000	00.
40.55	-,0022	57,13	67.401	0000	• 10	178.43	0000	00.
46.54	** CO13	-32.12	111.52	0,000	90 -	140.46	0000	700
44.01	7100.	91.70	113.55	0000	90.1	182.49	0000	00.
10.01	0100.	-120.51	115.57	0000	70.	184.51	0000	3 0.
60.00	.0007	•151.70	117,60	0000	• 03	186.54	0000	90.
>0.05	*****	-129.10	114.63	0000	.01	146.57	6000	96.
54.16	2000·	-117.40	121.06	0000	10.1	140.00	0000	20
54.15	1000	-100.45	123.08	0000	000	192.62	0000	200
50.17	2222.		125.71	0000	10.	104.05	0000	00.
20.0	1000	•62.51	121.74	0000	,01	190.08	0000	Du .
\$0.00	1000	-45.23	124.17	0900.	• 01	196.71	0000	00.
96.59	1000	-50.42	151.79	9900	10.	200,13	0000	30.
00.10	.0001	-18.45	155.62	0000	.01	204,16	0000	36.
- 3 44	. :	3 5	31 11 1	0000	ć			



/	TION IN INCHESS	/**********	/*********/	TIUN IN RADIANS-	3	/esskerakkuese/
₹	1	7	*	>	7	
0250	26500	0.000	10000	00000	00000	
.05664	n2n60*	00007	30000	٠,	10000	
******	.04256	-,00125	10000	0,000.	10000	
D1100	KOS00.	90000	20000	•	10000	
1100	03540	01000	10000	00000	10000	
	7 4 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	7 7 7 7 7	70000		20000	•
12550						
¥15C0.	04340	.00125	10000	00000	10000	
. 17174	.04051	\$0000	10000	00000	13020	
.051/4	.0440	21000	.0000	00000	10000	
\$2050.	\$0850	.00142	.0000	00000	₹0000	
0/850.	.04857	01000	.0000	00000	00000	•
+05 CD.	40440	•,00123	00000	00000	50000	
9 6050.	2/940.	.00142	10000	00000	20000	
****	.10100	01000.	.0000	-,00001	.00001	
\$7250	,04657	-,00123	10000	10000	20000	
04260.	6/860	.00142	00000	00000	20000	
でラフハン・	,10151	£0000°	10000	.00001		
.05476	.0220	-,00152	.00001	00000	20000	
10200	5.000	55000	10000	.0000	20000	
42500	90000	70000	.0000	00000	.00001	
61860	20/20	P2000.	.00001	00000	00000	
00000	1000°	01100	07000	00000	20000	
C/3C0.	. E-001.	# COO.	1000	1.0000	•• 00003	
2020	2000	E 0000		10000	20000	
04160	*0140	00100	00000	00000	20000°	
**************************************	10151	50000	.0000	.0000	.0000	
V42V0.	1,040.	.00156	10000	00001	20000	
サーバン・		.00173	00000	00000	20000	
- cutoc	.10100	\$7000*	10000	20000*	10000-	
.03446	84640.	. 00057	00000	2000°	20000	
\$0560.	101/1	01000	10000	100001	00001	
17750	. 04777	~* 000°	.00001	10000	20000	
0.0100	91270.	65000.	1.00001	00000	20000	
07050	10173	10000	.00001	10000	10000	
**************************************	,12217	21000	95000	00000	00000	
*4940.	6/240	05000	10000	10000-	90000	
C18C0.	.10101	90000	00000		20000	
£0440.	20801.	-,00252	00000	000000	57000.	
90550.	62960°	# 2 000	.00001	10000	£0000°	
1 7000.	.10412	\$2000°	10000	10000	£0000°	
04470.	X7050.	07500	00000	.0000	10000	
.05104	10460.	-,00056		00000	8000a	
\$4040.	10152	.00051	0001	00000	20000	
.02550	.04612	24000	00000	0000	0000	
040.00	.04718	0011/	00002	10000	10000	

	N N N N N N N N N N
--	---------------------------------------

3...

## 1000 0 0000 0000 0000 0000 0000 0000	אָט כּטּי	LUAD CUNDITION NO. 1	2 000	NAVY - ACOM PLATE	ONMS . FAITGUE	ANALYBIG - PLE 10	MLM 105,0 FEET	PAGE 10/05/76	
######################################	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	/	LECTION IN INCHES	7	*	TION IN RADIANS	7	/****EMARKS***/	; ;
79119 2000: 9000: 6000: 8500: 2720: 65110:	1011	.01157	45050	2000°	60000°	\$0000°	.00001	UBLIUUE	! !
		0.0110.	02142	# 000 # # 000 # # 000 # 1 # 000 # 1 # 000 # 1 # 000 # 1 # 000 # 1 # 000 # 1 # 000 # 1 # 000 # 00	60000 · •	90000°	. 00001	UNE THUE SEUBAL	
									·
								•	† †
	İ								
									: 1 !
									:
									1
	i								1
									1
									1
									:

S C L L L C X O Z **∢** DEFLECTIONS L × 1 0 7

Q.

	• n	₹ 4 •	4 HOST 44 B SETON	3 J 1	105.0 FEET	
A A A A A A A A A A A A A A A A A A A	***OKFLEGTION IN INCHEGE*	7	NOTIFE THE FEET OF STREET OF STREET	TIUN IN RADIANS	7	/ FEET SAK SOFE
- 50x50.	-068/1	#00000 ·	00001	00000	00000	
\rightarrow	0670	000	10000	00000	00001	
0050	C000.	*000	10000	00000		
07/40*I	# T x D C	2000°		00000	10000	
7490	.00705	7170	10000	00000	50000	
44.50	0690		# D C D D	07000	00000	
3595	10800	\$ # 0 n n .		00000	10000	
>	e4.700.	12000.	100001	00000	10000	
15×50	00915	20000	1.00001	00000	10000	
0.5357	F0100.	00017	00001	00000	00000	
U.57ul	00H00.	00121	1,0000	00000	10000.	
-1.516	401/0	5000a*	1.00001	00000	00000	•
6340¢	V7 202 .	16000	00000	00000	10000	
-,05/36-	00600.	-,00121	100001	00000	10000	
-,04051	07276	*0000*	1,0000	10000	10000	
2	9	16000	00001	00000	10000	
15.50.	07152	00121	00000	00000	-, 00002	
0/010	01303	\$0000·	100001	00001	.0000	
	0/145	19000	00001	00000	-,00001	
71010	#00/0*I	.000,	10000	000000	10000	
۵	# 0 2 C 0 #	\$4000°	10000	00000	10000	
25750	5/0/0*-	# 000° •	10000	0,0000	00000	
1250	٠.) 	00000	00000	20000	
	6/8/0**	7000	10000	.0000.	10000	
0 : 1 : 2 :	•	2/070	00001	00000	10000	
ひょうこ	191/0	*070 •	22020	00000	2000n*	
	505/0"	20000	•	10000	10000	
: د	900/00	51100		00000-	10000	
	77	•	00000		20000°	
3	0/2/010	•	10000	10000	Tocho.	
00070	6/100		0000	\$0000	10000	
7 1 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	(•	10000	10000	
00000		7000	10000		10000	
	0.07547	. :		00000	20000	
· 1 3 3 4	-	•				
	41770	() [] () () () () () () () () () () () () ()			10000	
	, , , o	0.000	• •	00000	•	
4 4 7 .	09/0		07030	00000	00000	
75.		100		• •	00000 I	
04.000	77/=	06000	10000	10000	20000	•
3.0310	70		00000	1000	0000	
\$1687.	01/0	10000	10000		C0000	
÷	•	56000	00000	00000	20000	
13450	2	10000	00000	1000	20000	
.0/50	* CO. O .	#4000°		00000	₹ 0000 -	

G

933

CONTROL CONTROL OF THE PROPERTY OF THE PROPERT

	• • • •	NAVY - ACHK PLAI	TFUNDS - FAILFUE A	# 1 1	105.0 FEET	
	-UEFLECTION IN INCHES		//	KUIATIUN IN MADIANS		/KHANKB/
< 	-	7	•	•	7	
271704	0.000	98100	#2000 ·	00000	00000	
	710	000	•	10000	0000	
٠	07.55	95000.	10000	00001	20000	
•	070	•	20000	00000	00000	
•	-01032	•	10000	- 00001	- 00005	
> :		2000 ·	10000 ·	7000	•	
70/70		12500		200000 T	10000	
		02100	10000		30000	
6 5 7 7 7 7 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	•				2000	
55650	37000	47.100				
04133	14770	0.000	10000		3000	
10550	07040	37000	10000			
01/50.	00000	04600	2000			•
\$1250.	-,06272	00062	70000	£ 0000	0000	
00750.	07080	10000	M 2000	10000	10000	
13350		•	10000	**************************************	20000	
03347	0010	100574	20000	20000	00001	
0554	05903	50000	.00001	00000	0000	
	• 00010 • 00010	19900	\$0000	10000	.00003	
95757	-,06223	57000	40000	£0000 -	.00003	
20750	87K50.	3	10000°	E 0000 ·	00002	
2 .	3 : 0 :	• 00786	50000	10000	•,00003	
9/29/20	> :	20000	40000	9000	20000	
31111	E * 1 1 5 1	6/100	n 50000	7 0000		
70000		50000	2000		10000	
*****	> :		0000	90000	50000	
31/20		7410	70000	5000		
50220	700	70000				
50420.	. =	•	00000	F0000	10000	
. 06620	04195	200	90000	00003	10000	
. 06393	- 0.5043	01465	50000	£5000 •	20000	
02517	67070		40000	M3033*	0000	
16270.	-	01000	90000	00003	20000	
•• 04120	03575	-,00021	50000	£0000*•	10000	
CE405	-, U SH U B		\$0000	\$0000°-	00001	
05400	701	55000	40000	£0000 -	20000	
14110	01958		\$0000	₹0000*•	00000	
15110.	01646	-,01656	\$0000	- 00003	20000	
14010.	2		*0000	70000	00000	
********	-,01919	.00153	\$0000	~ 20000 -	000000	
-,00005	01843	.01675	90000	# 0000g	.00001	
353000	01676	11000.	10000	£0000 -	20000	
01182	01626	01H1B	50000.	K0000 -	.0000	
2/900.	1166	.01851	\$0000°	00004	- 00001	
62610.	-00017	0.00013	00000	2000	60000	THE POINT

N . LOINT ORTHERTICNG AND RELATIONS

בייאס בסאו	CTAG CONDITION NO. 2	z . e. J	NAVY - ACMM PLATFURMS	- FATIGUE	ANALYSIS - MLH 10	HLW 105.0 FEET	PAGE 6 10/05/76	
TABEON.	7000000000000000	A A STEEFTION IN INCHESSESSES Z	7	TOXETTE X	7	7	/===×EHAKB===/	!
1011	4 N 2 2 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	01500		10000-	#0000°=	• 00001	DELIGUE	
2101	099000	- 01519	11200	60000° 70000°	70000	- 00001 - 00001	GLUMAL UMLIQUE GLUBAL	}
								i : 1
								1
								1
								1
								1
7 7 8 P								1
								1

TO THE POR ONE OR OTHER DESIGNATION OF REAL PROPERTY.

/ seesseessee		7	X X X X X X X X X X X X X X X X X X X	ATION IN RADIANSOLL	7	/seekEnakkusss/
,1550	.26743	-,00041	20000	.00001	10000	
15500	28179	<u> </u>	20000	.00001	00004	
00551.	609/7	E #500 -	2000°	•	\$0000°	
/ a : 5.1 .	3030	77070			50000°	
145/4	. 26178	00424	20000	. 00001	50000	•
15721.	. 24115	17000.	20000		10000	
11721.	* 2054n	00197	20000	100001	00000	-
01250	67976		20000	-,00001	#0000°	
11261.	. 68867	20.00	20000	- 00001	K0000	
012610	152020	00049	20000	.00001	50000	
0 1 1	0,000	W 2000	7000°		50000	
	+ 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		20000			•
70031	72000	2000	2000	10000	C0000	
10020			30000	10000 T		
.10100	27592	54500	# 10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2000	90000	
13542	.29533	\$2000	00001	00001	20000	
.10100	. \$01/0	10000-	.0000	£0000*	.0000	
.16108	, 24506	00369	\$0000	.00001	50000°	
.10027	46706		£0000°	20000	90000	
12011	5,9665	00170	20000	00000	*0000 *	
3000	22062	2 100	50000	00000	00000	
~ \	0000	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	V 0000			
47.00			4 0 0 0 0	70000		
01001	07070	00700	00000	2000	2000	
> ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~						
40004	0 7 0 0 V	X 7 7 7 7 1	*0000		40000	
13239	64255	01500	20000	00001	20000	
.161/0	. 50155	\$9000	50000	90000	00000	
.10115	4/502.	.00135	20000	00001	70000	
.10400	, 50262	\$2000	.00001	• 00003	.00003	
.15418	. < 6647	₹9000*-	£0000*	£0000*	40000	
1704	. 2910h	,00111	20000-	00001	80000 B	6
.10/55	. 50257	.00257	.0000	00000	50000	
. 1001.	D 1 2 1 2 1 2 1 2 2 2 2 2 2 2 2 2 2 2 2	01100	95000	•	10000	
2010	11697	60000	•	50000	.00028	
010010	09105	70000		10000 · •	3000°	
0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1	200 2 0	9//00*	0000	10000	10000	
00/0	77.000	60100	10000	50000	90000	
100-10	0770		30000			
1	N1-420	4 - 1 - 2 - 4 - 4 - 4 - 4 - 4 - 4 - 4 - 4 - 4	**************************************	W = 0	V 00000	
2250	F-557	23000	70000	7000	0000	
0700		7 1 2 D D O		10000 ·		
27671.	9	: 5	10000	7 0 0 0 0		

1 >-	INCHEWATER	ATDARTE A STAT	LOCK ANALTOLO & THE LOSS LANGES	70000 10000	/ DESKENAKK BODD
50286	16110.	64000	20000	•• 00001	
60 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	19000	90000	50000	1 6000 g	
595	92/00	10000	10000		
25417	.00001	50000	70000	00011	
20024		10000	20000	#0000°	
26125	25:00 °	20000 ·	#0000 *	\$3000°	
- 0	40.00	30000	20000	00000	
28152			# 0000 ·		
C (4 K K C C - 4		1 1000	1 1 2 2 2 2	
y 0	1000	4000	2000	80000	
2			7 5000		
0 1		- P		D0000	•
3	0.000		2000	2000	
		N * 000 0 0	* # * * * * * * * * * * * * * * * * * *		
7 4		7000	7000		
2 .	7010	1000	4000	01000	
2					
24241	0276	3 C C C C C C	40000°	2000 ·	
014	70000	-,00015	60000	.00015	
1343	91850.	- 00019	00011	01000	
3/3	950	0001B	\$0000	,00012	
9 2 2	7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	91000	11000	50000	
7 7 7	0000	3 M C C C C C C C C C C C C C C C C C C	9000	10000 ·	
1205	00171	F > 0.00 -	0000	21000	
6427	\$ 6 2 0 °	84000	50000	70000	
5043	.05135	-,00021	.000	21000	
6500	02004	00014	00012	10000	
1019	.0010%	0.0000.	£0000.	00000	
6559	= 0550S	=.00022	00011	90000°	
0941	66100	£2000*=	21000	P1000 -	
5191	747CO.	00021	.00013	21000	
	B/ACC*-	-,0006	11000	90000	
102		5 0 0 0 · I	21000	•• 00000	
4655	2100	07000	21000	90000	
000	05000	2000	21000	90000	
	26400	/2000	61000	71000°	
27.40		\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\			
	65500	03000	21000	80000	
1000		1 NO 00 1	1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		
274				10000	
40			***************************************	80000	
0000	2 2	070001	\$1000°		
0/9/0	975/O*•	7000-	71000		
00227	07000	400mm	45 000	1	TIME TOTAL
3					100

THE PROPERTY OF THE PROPERTY O

רמעם כחי	LUAD CUNDITION NU. 3	. s. u	NAVY - ACHH PLATI	i ia	NALYSIS - MLW 105.0	S.O FEET	DATE 10/05/76	i 1
NOT NOT NOT NOT NOT NOT NOT NOT NOT NOT	/	CTION IN INCHESSES	/	X X X X X X X X X X X X X X X X X X X	TICN IN RADIANGELE	7	/esekEMARKSese/	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
•	0.00 0.00 0.00 0.00	N+000 .	0-01	72000°	91000*	10000°	and Tan	· · · · · · · · · · · · · · · · · · ·
1012	17420.	00272	.01954	87000**	00010	#3000 #3000 #3000	UNLIUNE CLUBAL GLUBAL	+
								!
								1
2 t t] . t . t . j								
• 47 3 4								1
								!
				-				· · · · · · · · · · · · · · · · · · ·
								† *
								T
<u> </u>								,
-								· · ·

LUAD CUNDITION NO. 4	2 8 5	NAVY - ACHR PLATFO	HAND - PATIONE	ANALYSIS - PLW 1	105.0 FEET	DATE 10/05/76
N(1) 1 2 1 2 2 1 2 1 1 1 1 1 1 1 1 1 1 1 1				4 4 6 4 9 N 1		A THE PART OF THE
×		7	*		7	
#1000°		74000.	20000-	.00001	00000	
00014	-,10132	•0003₩	00002	100005	.00001	
77700	•	9100	20000	10000	•	
97/000	10664	10000 T	70000°	10000		
6/500	: -:	00438	20000	10000		
\$ C 0 4 0 8	7	14000	2000	10000	00000	
プリロナロ・1	-, 10411	24000	20000	• •	10000	
*************************************	-,16219	>0.00.	20000-	10000	20000-	
0/100.	-,16509	1020	20000	10000	10000-	
\$/800°	٦.	00136	~.0000~	.00001	•	
00/04	٦.	95700*-	20000-	10000	20000	
7/100·	-, 10804	L6000.	000v2	00000	.0000	•
09195	16475	.00109	10000	10000	20000	
-,00846	10043	#\$ #00° =	-0000S	.00001		
65570.	-,17450	95000	.00001	20000	20000	
V1370.1	-,10853	.00109	20000	.00001	.00003	
77170	-17160	• 00438	22222	0	.00003	
BC250.	17448		10000	20000	20000	
07540.	17210	.00144	20000-	.0000	₹0000-	
04581	-,10947	.00121	20000	• 00001	.00003	
55270.	-17319	0<200.	20000	.0000	20000	
07760	17075	.00185	20000	00000	00000	
/ 00 A 0 • •	., 17178	SA500.	00000	00000	£0000°-	
	-,17452	- 00142		20000	20000	
	. 10458		•	-	•	
	-1/1/6	94500	00000	00000	£0000	
/ C# A O • I	DD7/1.	- 0010S		20000	20000.	
0/5/0	., 10945		•	-,00001	£0000°	
10010.	17100	50000	•	00000	£0000	
01000	17429	- 00170	20000-	50000	₹0000°	
17070	S. LOALM		•	00001	• 00003	
C*C***	-17573		10000	20000	£0000°	
97670.1	.17073	*1000	20000	10000	•	
07040	.17203		00000	00000	50000	
*****	-,17575	00214	0000	00000	10000	
*05*0°•	DD171 .	. 1520.	0.000	00000	•	
8/5/0		. 00100	10000	20000	50000	
/o/oc.	•	- 00159	•	٥,	£0070°	
\ B\$ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	1986	•	10000	10000	00000	
0/260	•	.	•	.00001	00000	
97701.	070.	05400	•	2000	•	
9 7 9	1/5/1	3	10000.	20000	•	•
9/400**	17142	-,00175	. 00001	•	£0000*•	
2	-,17501	0017	00000	00	#0000°	
04215	17176	7	07070.	9	\$0000°	
	17107	0,000	⊘ 0000°	.0000	M0000.	

DATE 10/05/76	/ess XRAE BY					•						•																											
5.0 FEET	, , , , ,	10000	0000	. 00000	00000	£0000°	10000	50000	90000	• 00003	M0000.	M P C C C C C C C C C C C C C C C C C C	01000	20000	.00007		90000	01000	10000°	0000	* 00000	•,00003	01000	80000°	00000	00000	50000		#10000 •	70000	M 00000	60000	00000	90000•	00000			90000	7:5:5
ANALYSIS - MLM 105	TIUN IN RADIANS-	10000	0000		.00001	£3000 -	11000	10000		10000	10000	20000	50000	10000	90000	1 0000	2000	\$0000	90000	97000	97000	• 00003	10000 ·	80000	10000	£0000*•	70000	20000	10000	00007	10000°	00000	40000	90000	51000.		60000	#0000°	
TFURMS - FAIIGUE A	/A	69000	00000	-,00012	.0000	\$3000°	S0000	99999	.0000	00003	N0000	10000 ·	20000	20000-	01000	\$0000 ·	04000	*2000°	01000	60000	.0001	01000	51000	21000	80000	50000	\$1000	21000	00013		N 1000	21000	400017		# COO.			.00013	€ Cac •
NAVY - ACHK PLATE	7	02520	30000	3850	0036	459	2 4 5 0	11100.	-00407	.00205	- 00107	11500	26000	.01981	-,01057	0/120	01307	69000	7510°	\$4000	D # # # # # # # # # # # # # # # # # # #	-,006/5	24200	10300	.01562	00150	20000	56.50	1325	00000	25000°	00321	-, 02025	-03434	71070°	75.50°	00558	*******	~ # C # O *
* 6 *0	LECTION IN INCHES	.25270	17405	20	17009	1714		17353	1692		- 1747B		-,15563	_		1017101 10171	16671	•,15349	2000	-,15556	- 1450B	-,14611	216014	. 09723	-,10511	-10275	103/3	0/560*-	22201.	A01.	2/4/0.1	E7570"	.05516	16570	** 05503	04040	85770	29770	6.05042
DITION NO. 4	/	D 7 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	87070	おつさかつ・	00140.	1		0/540**	-,09251	\$1000.	V V V V V V V V V V V V V V V V V V V	17000	1790	5+200*-	000	9.000.1	00102	00106	0777		·. 07870		2700°	**************************************	. 02509	15550.	20000		86750	-, U3003		00770	00050-	.05001	22042.	- C 200	.02578	510	75570"-
LUAU CUNDITION NU	SOLUTION ROADER	700	107	705	703	306	507	7.7	108	709	01/	717	301	208	500		9 0 E	200	0 20	210	F11	818	~ ~	, ,	306	40 A	200	909	603	016		1001	2001	2	7 0	, ၁		Э :	1004

HERE RELIEVED BEFORE PROPERTY AND SOCIETY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE

חשם כח	LUAD CUNDITION NU. 4	Z •8• D	NAVY - ACHK PLATI	TFOMMS - FAITEUE ANALYSIS	•	FLW 105.0 FEET	UATE 10/05/76
NUMBER NUMBER	1	/	7	X X X X X X X X X X X X X X X X X X X	X Y NOTATION IN RADIANGEOUS	7	/ SEEMENARK BOOS!
===		.04116	.01135	£1000 •	• 00011	00001	UNIT TOUR
1012	02575	1.04267 1.04403	04000	91000	000011	# 00000 # 00000	CLUBAL GLUBAL GLUBAL
							•
							-
! 							•
					:		
-							

£.7

		•		0001 LIC - 01011LL	1334 0	
JOIN! / TERRESTEEDEN	DEFLECTION IN INCHES	7	X X	UN IN RADIANGES	7	/ seekEnakk Bees/
959/5.	. 69260	+0200	50000	20000-	20000	
95925	.01771		50000	00002	60000	
0.0/0.	7/200	6.000.0 6.000.0	(A) (A) (A) (A) (A) (A) (A) (A) (A) (A)	•	11000	•
60000	67023	M0000		70000°	**************************************	
6/055	10110.	00045	90000		71000	
1 20041	.70150	0200	\$0000	- ,00002	20000	
. 50013	17000	•	50000	-,00002	60000	
0 b b b b b b b b b b b b b b b b b b b	6.01.00		60000°	23000°	11000	
7764	-04040 		6000°	•	\$0000°	
13.00°	6400	\$ 2000 ·	10000 g	20000	10000	
96505	78676	10051		30000-1		
. 5045	67841	17600	10000	•	V1000	•
.33658	. 69475	92600	40000		00016	
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	.71863	₹00505	-,00002	•	90000	
4/808.	,67355	-,00927	20000	00007	\$1000°	
D7187	L7770.	£ \$ \$00°	L0000.	50000	.000.	
37000·	.71710	00155	N0000*	50000	90000	
2//05	104231	2000	50000	- 00003	00013	
10000°	26100		7 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1000°	£1000.	
19750	07320	20200	n so o o o	40000	*0000°	
20000	69169	00000	.0000	\$0000	00051	
. 50702	,71506	60000	20000	50000	40000	
. 50850	,66957	.,005.7	20000	00007	51000	
. 35866	. 64163	.00457	£0000*=	£0000°	.00021	
80200	.71648	-00104	M0000*	•• 00004	90000	
26236	.67300	•0110	20000	*0000	00014	
77707	D 3 3 3 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	00110	0000) 	02000	•
クオアのの。	10417	\$9000	8000°	. 00013	S0000.	
30000	500/6	•	10000	97000	000010	
	/ 071/0		70000	70000	L0000 -	
1255°	5 1 9 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	•	00000°	# TO CO	1000	
. 34462	,71517	00571	40000	40000	01000	
90101.	.90788	71610.	.00114	10000	50000	
11204.	*67a04	12100.	10000	00000	09000	
60565	. 7100A	15000.	@nono*=	000	00010	
30KP4.	. 74605	.02027	90000	#0000°	90000	
. 57762	.67245	000544	= 0000S	60000	.00019	
3:	07057	00500	23000 ·	\$0000°	• 00015	•
97578	66530	92610.	3 f 3 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	50000	, 0000 .	
15656	916/916	2/200	21000	50000	~:	
70045	• 10134	F 0 1 0 0 0		9 6	0 4	
3 2	- X 0 4 4 1		0000°	4:000	>>000°	



NOTAL STORY OF PORTAL PARAGON STANDARD CHARGE TORGON OF STREET STORY STANDARD CONTRACTORS OF STREET STANDARD C

110		1	:			į	
1000 1000	067LEC *	Z 		× 1112111111111111111111111111111111111		7	/sssmines/
	-	1249	1610		9		
	3000	•	0028	11000	0000	00072	
	30502	66999		.00016	60000	• 00018	
	97529	- C - C - C - C - C - C - C - C - C - C	•	\$3000°	20000	20000	
	21000	10200	00100	71000	11000	\$2000	
	7 - 7	112/04	ERSON TO		10000		•
1000 1000	2.5	7 6	•	W			
11 12 13 14 15 15 15 15 15 15 15	19191	1,582/3	00100	4.000	0000	13000	
1000 1000	000/	05000	0197	34000-	1000	1000 ·	
1000 10000 10000 10000 10000 10000 10000 10000 10000	3234	65723	0240	\$1000 ·	5000	22000	
1000 1000	151	8	1000	B.00018	60000	0000	
1000 1000	9119	.65148	0187	4.00017	11000	0000	
Section Colons	8695	61059	01770	07000	9000	0000	•
\$519.5 \$519.5	/907	50014		00035	00021	00032	
19719 1900 1900	2035	.56440	96400	-,00030	20000	00000	
\$5446	1896	0.000	80000°	24000	00054	00051	
1000 1000	0350	612/50	•	-,00012	00012	£0000	
17494	0970	.55448	•	.00013	80000	90c00°	
1992 1993	0242	.50135	•	0.0000	00011	00000	
\$55746 \$55747 \$55717 \$55717 \$55717 \$55717 \$55717 \$55717 \$55717 \$55717 \$55703	1714	65/65	00303	00035	.00021		
19412	2321	.53746	.07758	27000-	\$ 2000°	.00021	
11 11 11 11 11 12 12 13 14 14 15 15 14 15 15 15	4384	,56322	•	07000	.00011	00000	
1920 1920	**************************************	12000	•	85000 B	52000	- COU12	
11000 110000 110000 110000 110000 110000 110000 110000 11000	16.0	7777	•	440001	\$2000°	91000	
19699 1969	123	11408	2000		21000	1000	
35203 39017 300049 30017 300024 300024 300024 300002 300012 300013 347643 300024 300025 300027 300026 300026 300027 300026 300027 300026 300027 300026 300027 300026 300027 300027 300027 300027 300028 300027 300028 30002	1704	00725	03758	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	7000°	* 9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
3 4 4 4 4 4 4 4 4 4	2025	35203	1166	7 # C C C C C C C C C C C C C C C C C C	14000	1000°	
343648 -002010 -00053 000025 000012	2250	39017	00000	67000	00024	00000	
\$4949 \$4443 \$4443 \$4443 \$4443 \$4443 \$4444 \$40445 \$40446 \$40446 \$40447 \$4004	8550	.3764H	•	00043	00012	20000	
\$4743 \$4743 \$4743 \$4743 \$4743 \$4743 \$4743 \$4743 \$4743 \$4744 \$4744 \$4744 \$4744 \$4745 \$4744 \$4745 \$4744 \$4745 \$4	1400	. 30303	•	05000-	00005	0000	•
\$4743 \$4527 \$4	6760	54646	00200	05000-	.00027		
15000 1500	9092	54763	•	V4000.	15000.	92000	
17617	200	. 38627	•	0.000	00005	000018	
10002	200		•	0.000	92000	E 1000 -	
17617 -17617 -20024 -16708 -16708 -16708 -16708 -16709 -16709 -16749	787	45470	7000	## COO - I	7 7000°		
100002	4740	17617	400	00000	000050	5000	
19708 .00019	1549	\$5002	0711	29000-	61000	0000	
- 14244 - 00001 - 000023 - 000023 - 000001 - 000023 - 0000023 - 0000023 - 0000023 - 0000023 - 0000023 - 0000023 - 0000023 - 0000023 - 0000023 - 0000023 - 0000023 - 0000023 - 0000023 - 0000023 - 0000023	1508	,1670A	257	40000-	87000	01000	
18749 . 000023 . 0000023 . 0000023 . 0000023 . 0000023 . 0000023 . 000023 . 000023 .	1075	.203¢A	.0853	00051	0000	0000	
10000 000000 000000 000000 000000 000000	2970	.14698	2400°	55000-	.00023	20000	
17240	9696	10759	.15666	00053	.00036	.00015	
16200 650000 6500000 650000 650000 650000 650000 650000 650000 650000 650000 6500000 650000 650000 650000 650000 650000 650000 650000 650000 6500000 650000 650000 650000 650000 650000 650000 650000 650000 6500000 650000 650000 650000 650000 650000 650000 650000 650000 6500000 650000 650000 650000 650000 650000 650000 650000 650000 6500000 650000 650000 650000 650000 650000 650000 650000 650000 650000 650000 650000 650000 650000 650000 650000 650000 650000 6500000 650000 650000 650000 650000 650000 650000 650000 650000 6500000 650000 650000 650000 650000 650000 650000 650000 650000 6500000 650000 650000 650000 650000 650000 650000 650000 650000 6500000 650000 650000 650000 650000 650000 650000 650000 650000 6500000 650000 650000 650000 650000 650000 650000 650000 650000 6500000 650000 650000 650000 650000 650000 650000 650000 650000 6500000 650000 650000 650000 650000 650000 650000 650000 650000 6500000 650000 650000 650000 650000 650000 650000 650000 650000 65000000 650000 650000 650000 650000 650000 650000 650000 650000 65000000 650000 650000 650000 650000 650000 650000 650000 650000 6500000 650000 650000 650000 650000 650000 650000 650000 650000 650000 650000 650000 650000 650000 650000 650000 650000 650000 6500000 650000 650000 650000 650000 650000 650000 650000 650000 6500000 650000 650000 650000 650000 650000 650000 650000 650000 6500000 650000 650000 650000 650000 650000 650000 650000 6500000 6500000 650000 650000 650000 650000 650000 650000 650000 650000 6500000 650000 650000 6500000 65000000 650000000 65000000 6500000000	9756	11290	0.054	09000	62000*	**0005	
#1000° ##000° ##0000° 000° 00	7867	. 16465	1629	44000	82000°	.00017	
# # # # # # # # # # # # # # # # # # #	09500	⊃ :	1726	2000	000036	*100°	
	かいここの	2	2	5000			



Z	-	U. B.	NAVY - ACHH PLAT	PLATFORMS - FAITGUE AN	ANALYSIS - MLM 105.0	0.0 FEET	DATE 10/05/76	1
/*************************************		ECTION IN INCREMENT	7	A A A A A A A A A A A A A A A A A A A	TION IN RADIANGE	/**************************************	/eeekEnamkoeee/	!
50480.		.15442	.04505	40000	45000°	F0000	3001 190 190	! ! !
90100.		15696	.0406	99000	07000	60000	CLUBAL GLUBAL	
	1							† i !
								!!!!
								! :
	1							
	1							
	l							
	1							i i i
	t							! :
	Į.							!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!
	ļ.							! ! !
	1							1
	1							
	l							! !
	í							1 1 1 1 1

		2	10				
1000 1000	:	-			Z		/000XF # ARK # 800
	-			×	,		
			001		10000	0	
	-		7000	20000	0000	000	
	~		.00200	. •	10000		
	-	0.4250	•	20000-	.00001	•	
	7071	•,22712	•	~0000	.00001		
	⊸ .	5477°	•	20000	10000	•	
	-	7627.	300	2000	10000	•	
1942 -23142 -00013 -00004 -000013 -0000013 -000013 -000013 -000013 -000013 -000013 -000013 -000013 -000013	• •	00500	֓֞֜֜֜֜֜֜֜֜֜֜֜֓֓֓֓֜֜֜֜֓֓֓֓֜֜֜֜֓֓֓֓֓֜֜֜֜֓֓֓֡֓֡֓֡֓֡֓֜֡֓֡֡֡֓֡֓֡֡֓֡	20000	10000	•	
124 124	• •		•	N 0000		•	
1946 1949	• •		•				
154 154	• -	11111	•	20000	10000		
1942 1942	• •	30000°	•	W 00000			
1947		7 N S N S N S N S N S N S N S N S N S N	•	20000 H	10000		•
10000 10000 1000000 100000 100000 100000 100000 100000 100000 1000000 100000 100000 100000 100000 100000 100000 1000000 100000 100000 100000 100000 100000 100000 1000000 100000 100000 100000 100000 100000 100000 1000000 100000 100000 100000 100000 100000 100000 1000000 100000 1000000 1000000 1000000 1000000 1000000 1000000 1000000 1000000 1000000 1000000 1000000 1000000 1000000 10000000 10000000 100000000	1010	00000) : 	20000	20000		
1942 1944		10/5/01	•	**************************************	1000		
1942 1942	-		•	20000	£0000°	#00000°	
1942	•	24037	,00266	E.0000.	10000		
19624 19624 19624 1960	-	2002.	•	10000	00000	-,00005	
1984	2	8877.	•	20000-	£0000°	70000	
1944	•	.2451	.00197	£0000*=	.00001		
150 150	~	.2410	14100	£0000.	, •	•	
1941	2	.2465	0040	£0000**	.0000	20000	
15425	-	.2435	09200 -	00003	00000	00000	
13400 144779 100000 100000 100000 140000 140000 140000 140000 1600000 160000 160000 160000 160000 160000 160000 1600000 160000 160000 160000 160000 160000 160000 1600000 160000 160000 160000 160000 160000 160000 1600000 160000 160000 160000 160000 160000 160000 1600000 1600000 1600000 1600000 1600000 1600000 1600000 1600000 1600000 1600000 1600000 1600000 1600000 16000000 16000000 16000000 16000000 16000000000 160000000000	~	1002.	•	10000-	00000		
1542 15440 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 1000000 100000 1000000 1000000 1000000 1000000 1000000 1000000 1000000 1000000 1000000 1000000 1000000 1000000 1000000 1000000 1000000 1000000 10000000 100000000	_	.2477	•	20000-	\$0000	70000	
15414	~	01012.		£0000*	≥00000-	#0000°	
15 to 15 t	2	60nn2		1.00001	00000	\$000°	
15414	2	- 2448B	•	20000 ·	£0000°	.00003	
5421	1561	-,24159	0035	00003	-00001		
15404 15406 15406 15406 15406 15407 15407 15407 15407 15407 15407 15407 15408 15407 15408 160000 16	-	-24448	.0077	00001	00000		
1415d		.247	1200	2000 ·	40000	90000	
14134 - 24369 - 00048 - 00000 - 000002 - 000002 - 000002 - 000002 - 000002 - 000002 - 000002 - 000002 - 000002 - 000000 - 000000 - 000000 - 000000 - 000000	•	•	0015	20000	0.000	40000	
15757 - 24549 - 00041 - 00000 - 000002 - 000002 - 000000 - 000000 - 000000 - 000000 - 000000	-	•	000	60000	10000	70000	
13380 14010 14010 14010 14010 14010 14010 14010 14010 14010 15010 15010 15010 15010 15010 15010 15010 15010 15010 15010 15010 15010 15010 15010 15010 15010 15010 16		07270	7000			•	
14017	•	01517	4000			•	
14016	•	1000	6 0 0 C	00000	2000	10000	
14343	•	212B	7440	0.0000 F	•	•	
14303 - 25904 - 000072 - 000000 - 000000 - 000000 - 000000 - 000000	-	2005	20015	20000	90000	•	
13967 - 25968 - 00072 - 00002 - 00002 15043 - 25347 - 01115 - 00002 - 00004 15522 - 25037 - 01115 - 00002 15527 - 01356 - 00001 15527 - 00364 - 00000 15527 - 00364 - 00000 1552 - 24557 - 00364 - 00000 1552 - 24484 - 00260 - 00000	-		0000	- 00001	20000		
1564324448001170000200002000020000410000200004100002000041000020000410000200000000000000011000000000011000000000011000000000011000000000011000001000001100000011000001100000011000000011000000110000000110000001100000000	7	*****	0007	20000° •	•	00000	
15553		7776	1 1 1 2		•	•	
15922 - 25037 - 01115 - 00002 00003 - 15507 - 00356 00001 - 00000 00000 00000 00000 00000 00000 0000	: :	25.7		2000	•	•	
13507 - 24557 - 001356 - 00001 - 00000 14504 - 245047 - 00242 - 00000 - 00000 15020 - 00000 - 00000	: -	7047				•	
14504 - 25047 - 000242 - 00000 - 000000 - 000000 - 000000 - 000000	-	4477	****	30000 T	•	•	
13626 - 20000 - 60000	•	1010	777	•	-	•	
	•	0063.		•	•	•	
	2061.	. r. e e e	9900	•	•	•	
ACCION PORCO II MOCUO II				2000	•	•	

ROTATION DEFLECTIONS 105

ACT PLATFORMS 2
TARTOR TO THE TOTAL TO THE TOTA

	•	1		† 1 ! !	!	1		1	!	1	1 1	! !	1	
S. C.	PAGE 16 UATE 10/05/76	/4E HARK 8/	UNLIGUE SLUMAL UNLIGUE GLUMAL											
90 14 14 15 15 15 15 15 15 15 15 15 15 15 15 15	5.0 FEET		20000° = 200											
2 4 50 2	rate - sts.	A Y Z	*,00016 *,00016 *,00018											
E . L . C . T . C . L . C . L . C . L . C . L . C . L . C . L . C . L . C . C	- FATTGUE	/x	200027 850000											
0 + 2 1 0 7	NAVY - ACMM PLATFOHMS	IN INCHESSOR												
2 4 2 1- 00	U.8.	CTION IN INCHES	04490 54490 54490 64990				•							
	ITION NO. 6	Zenemento de LECTION A	7040. 0540. 54740.											
1	DV	NORMEN NUMBER												

2000 Sept. 18

SECURITY STREETS

SALANS SALAS

prince and exercises are considered as a second

1,	* * * * * * * * * * * * * * * * * * *	Z H >		:	l l	7	/ BEERENANDER/
1	71976*		-,00678	100	90000-	-,00012	
1		1,77621	01790	. 00015	•	41000	
1792 1765	0000	21057	505743	\$1000	•	62000°	
	90524	1.76312	C9010*	51000	•	1000	
1	90317	1.77607	02676	4000	•	00031	
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	5765A.	1.42965	1900	_		.00013	
1,1755 1,1755 1,0001	79864	1.80252	-,01751	\$1000°		00017	
1992 1993 1995	11155	1.77605	-,02793	\$1000.	•	00000	
	15050.	1.81518	9000	9 1000		.00017	
1		1,78929	5/000	.00015	•	60000	
1	91915	1.80241	1970.	\$1000	•	5500°	
MEDICAL MEDI	D/7070	\$515¥°1	•	01000	•	£1000 •	•
1 1 1 1 1 1 1 1 1 1	200/10	11679	10000	20.00	•	\$6000	
1000 1000	7	04001	C0020.	# O O O O	•	35000°	
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	- 100 E	1.05041	7000°	01000	7000	91000	
1	37.73		67270	37000	2000	4 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	
1		~ Œ	35.30 ·	03000 · U	1000	9 4 6 3 6 4	
	240/4	1,78054	- 02501	A 30 30 4	00000	B C C C C C	
**************************************	170/20	1.70946	06070	.00011	00063	00043	
	10077.	1.77719	.01249	.00016	\$1000°	#1000 ·	
1,750/4 1,75	244242	1.75617	.00341	92000•	00012	.00011	
1	9/525	1.750/4	.01973	12000-	.00013	£7000°	
1	557/20	3/00. ·	• 00115	91000**	90000	• 00015	
1,000 1,00	250/20	1,64950	-,01326	. 00011	00003	00004	
1 1 1 1 1 1 1 1 1 1	7017	1.75211	65110	-* 00057	£ 1000°	97000	
1 1 1 1 1 1 1 1 1 1	100/00	25500 ° I		00017	50000	- 00015	
1	12000	1 • 7044	0.05154	• 00010	\$ 000 cs	27000	
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	7977	1.74542		0 V 0 0 0 0 • •	71000	57000	
1	15//6	N. C. C. C. C. C. C. C. C. C. C. C. C. C.	.00113	90000	* 0000°	*0000°	
1 7 7 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	91//*	1,64935	•	Z 1000 -	•	00033	
1 75882 00050 00000000000000000000000000000	3000	1.4757	25200.	91000	•	# COO.	
1.00004 1.0	N960A.	0/00/01	•	\$0000 ·	22000	97000	
1.00263 2.55712 0.00551 1.00263 1.70139 0.0057 0.00065 1.00263 1.70171 0.0057 0.00065 1.05612 1.72771 0.0054 0.0057 1.72573 1.7265 0.0156 0.0055	7:17	7047	90026	7000	61000	10000	
1.0004 1.70159 00517 000065 .40045 1.70159 00052 000065 .40040 1.04094 000370 000011 1.0512 1.7271 000944 000005 .41514 1.7565 001065	10°774	0.274					
**************************************		1.701.50	C 1 4 0 0 .	. 40000	7000		
**************************************	57085	78171	00002	17000 ·	A0000	25,000	
1.05212 1.04094 .000370 .000012 .000012 .000034 .000002 .010944 .000008 .000033 .00003 .000003 .00003 .00003 .00003 .00003 .00003 .00003 .00003 .000003 .00003 .000003 .000003 .000003 .000003 .000003 .000003 .000003 .000	0.735	C. 781	•	020001	00000	51000	
1,05212 1,72771 -,000834 -,00002 -, 44574 1,71862 -,00994 -,00053 -, 47.415 1,7267 -,001964 -,00053 -, 47.415 1,75674 -,00166 -,00055	07077	20030		10001	22000	0000	
.43574 1.71265 .01994 .001033 .04725 .00098 .00098 .00098 .001265 .00098 .001266 .001266 .00126	1.05212	1.02771	₩\$900.	20000	00014	00034	
1,77265 -000964 -000053	5/557.	1.71462	76610	#0000 · •	00015	00015	
. 41000. 1.0004	.04725	1,71265	70600	00053	.00016	00000	:
<u> </u>	517/6.	1.75874	.00100	•	£1000°	-, UOU \$1	
	90559°	750	.01652	- 000¢1	000	.0005	
**************************************	676/9	C :	11520.	5000	5	07000°	
12000 A10000 082100 886001 62010				1	17000	0.000	

opera i kraserendi kassassan paspada parendraren i paspada in dagaren da.

-1.

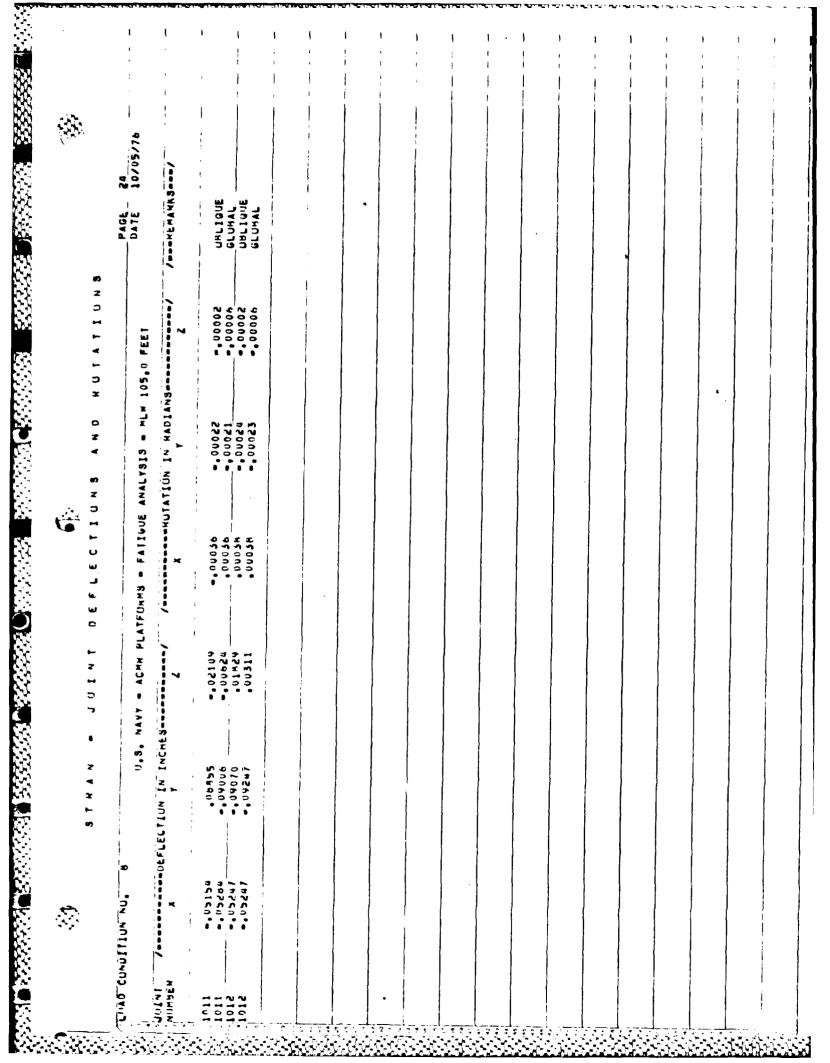
N

	के के किया है। के किया के किया के किया किया किया किया किया किया किया किया	2 4 2 6	0 F z H D		3 3 4 50 2	2 6 -	(3)	
רטעט בטעט	LUAD CUNDITION NO. 7	U.S. NAVY	- ACH	FORMS - FATTEUE	ALYSIS - HLW 10		PAGE 21 DATE 10/05/76	i
JULNI	//	DEFLECTION IN INCHES	7	X	X Y Y ANDIANGERE	7	/KE NAK Booo/	: † !
1011	1555.	207.77 COSC7	11231	00100	75000	.00019	USELIBUE	
1012	. 63504	87a64.	11000		.00103 .00048	. 00036 . 00036	GLUMAL CHUMAL	
-								
							•	
								! !
								;
		-						1
								i
ı								
								!

;

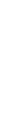
		NAVY - ACMM PLAT	PLATFURMS - FATIGUE A	ANALYSIS - MLM 105.0	5.0 FEET	
EF	-UEFLECTION IN INCHES-	/*********	/	TION IN RADIANS	/	/eeekEnakkBeee/
4	>-	7	×	>	7	
10500	•.29253	00318	£0000 -	2000°	20000	
40501	29001		0000	20000	9	
10501	200	•	\$0000°=	20000	•	
16257	75162.	•	£0000 •	20000	•	
0000	20075	•	50000	20000	9	
27.0	•	•	\$0000 H	20000		•
20.00		20000		20000		
570	24540	, ,	50000	20000	•	
6969	<976A	00677	M0000	2000	10000	
.10507	24611	-,00572	£0000	20000		
1200	. 24689	•	00003	20000		
3	- 3c452	00317	£0000.	10000	£0000°	•
70.55	50113	•	E0000 -	\$0000 \$	£0000°	
7	50304	2010	70000	20000°	.00003	
707	51614	- 00314	£0000.	70000	50000	
1512	- 50941	•	* 00004	- 00002	20000	
5.77	51515.	*010	10000	03000	50000	
3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	577 T S = 1	7500	10000 ·	7000	90000	
75.13	4115	2000	30000	2000		
1/471		2400.	40000	20000	C0000-1	
_	3120		7000	10000	0000	
1001	3	#/ #OO .	.00001	00070	00000	
1542	51560	B4500	£0000-	70000	90000	
17541	-, 51023	•	70000	50000	-, 00005	
/115	⊶ .	•	1.000.1	00000	50000	
7107	V2/10 -	****************	90000 I	#3000°	50000	
2427	16116	11700	2000	10000	70000	
. 🔪	31550	•	# 0000 F	10000	90000	
1204	-, 51006		M7000	£ 1000 .	50000	
7845	3189h	.00347	E0000-	20000	10000	
917	-,31370	60000	£0000*=	20000	•	
1254	3151A	00903	•• 00001	00000	50000	•
7571	05815	8000.	2000	#0000 ·	•	
0.44	7 7 1 1 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	004/0	5 × 5 5 5 5 6 5 6 6 6 6 6 6 6 6 6 6 6 6		•	
	27515	7000	60000	10000	00000	
1/516	55198		# 0000 · •	F 1000		
11325	-,31552			20000	70000°	
コアコケ	-, 5228h	.0144	•	50000		
1056	-, \$2205	3	£0000 =	70000		
1158	n	00622	00000	00000	90000	
0100	32035	200	10000	10000	=	
٥	. \$150	00401		00	80000°	
^ '	-, 51516	00021	50000°	.0000	40000°	
1111111				,		

DATE 10/05/76	/s==xpx4xx0e===/	1											•	•																														U#L14UE
105.0 FEET	/**********	2	00000*-	0000	.00012	60000	#00000 ·	•		•	60000	90000	0000	0000	40000		• •	0000	00000	000	5 2000 ·		10000	+0000	70000	20000		00000	00000	60000	UNDOO .		#700U	50000	•	22000		0000			7:00	-00013	\$0000°	£0000°
ANALYBIG + MLH 105	TION IN RADIANS	>	20000	01000	20000	0	10000	9 0	00000	0	0	00000	•		00000	•	•	00n17		20000		2000 T	60000	60000	20000	21000			20000°	0000	71000	000		-,00012	- 00013	7000	0000				.0001	91000	12000	. + coc.
ATFURNS - FAIIGUE AN	/	×	11000-	50000	30.	55000°-	00000	Э.	10000°	20000	.00001	\$0000.	20000	7000°	#0000		51000	00011	.00013	81000	11000	e 1000	000014	91000	• 00016	.0002	000	00013	60000	77000	7000	42000	42000°	0000	V	7000	12000	62000	.00016	\$2000°	#5000°	72000°	A2000	10000
NAVY - ACHH PLATE	/	7	4070°	04206	79700**	5 8 7 O	6 - C		7.000	.0059	1900.	.000	69500.	700	A 1 1 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	4570°	8670.	0731	-	-4	7070	• •	0.18	59600	-,01575	0.000		0000	-,01469	4740.	- AC-00.		-,00141	10	•	20000	07.25	2050	01	0044	.0074	9:	1610	C>
z • m • ∩	-DEFLECTION IN INCHES	-	-,45392	-,31613	52021	.3151	15.00	4010	31249	31709	•	-, 51272	34007	0.515.0	•	7850	2760	. 285/4	•	•	. 23.00	• •	-, 29216	••272°9	-, 27602		-,19355	205ch	07000		2000	.2041	2125	BRR.	7			_	1107	2	\$060.	0 7 7 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0) i	0 7 000
מ יטא אטן דו	/*************************************	×	17700	5	ם	0 7	1/442		. 0	~	~		6/100/0		137	25 ACT		~	15018		7007	.13758	. 15408	175	٠	111500	1144	7 7 7	2 2 3	v -	2000	- 14104	-,11505		00771-		, ,	۔,		-,05606	700		1	\$\$/ol.
CLAS CUNUITION NU	10106	A DEMON	204	و	•	2 .	- ! -			707	106	700	710	117	100	- N	1 M C S	208	, 805	202	> 10 0 4	0 0	oie		2.0	1 0 0 0 0 0 0 0 0 0 0	506	906	S - 0 -	000		606	-	116	21.	* O O T	1003	1004	5001	1000	1001	6001 6001		0101





			°0°	NAVY - ACMK PLATE	DRMS - FAITEUE	ANALY	105.0 FEET	DATE 10/05/76
		×	IN KIDGES	Z - J	I X	- STATE AND THE STATE OF STATE	7 · · · · · · · · · · · · · · · · · · ·	/****EMARKS***/
		8/03*/	0455	-1.2325	-55.5892	-224,3465	5.5498	UMLIQUE
-54.049 -1104 -151.054 -17.054		-4.5305	~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	2227.E1	01:0:5/10	141.6264	-51.4066	GLUHAL
-5, 5)? -6, 5)? -6, 5)		-0.050	4.1914	-37,0386	-237.00.58	127.0679	14.7.40	The Light
=28,0543 31,4305 = 190,052 290,0624 =21,7532 = 250,054		-4.4239	-5.45/2	39.4491	-196,7521	27.9364	407.00	
-28.0543 •.5310 •.11.2375 298,0624 •21,7552		-2,4238	-16.3693	3/.4305	-190,/561	29,1660	-5.0054	6LUSAL.
		-15.3606	-28,0543	5310	-611,6375	296,0624	-21,7532	
							1	
	-							
								•
]							
	}							
	}							
	}							
	1		,					
	1							
		·						
	ł							



STREET CAS SECULOS SCHOOL STREET

ij

:	1		•		1			! !	1	1	1		1	 	,		•	1	 - - 	1 1 1	:	1	1	
PAGE 2 DATE 10/05/76	/BESKENAKE GSES/		UBL I GUE	GLUBAL	טאר ו פּט		GLUBAL																	
5.0 FEET	/	, !	-4.1020	42.436	20120	2000	2,3144	14.9493				!												
ANALYSIS . MLW 105.0	PERSONAL IN INSTITUTE		176.3299	110.01.44 110.7 IF 18	-103.0851	-26.7315	-27.4A74	-202.6924																
FURNS - PATIGUE	/	77707	\$000°/V	131.0546	183.4265	157,1762	157.1762	479,6352																
VY - ACHK PLAT	7	76.70	1010	20,4112	27.0771	1204.15-	-20.8720	. 9685																
U.S. NAVY	TEA THE SECTION OF A PARTIES OF THE		7/32/3	0455.8-	0.0172	4.4870	9.0317	20.6967									İ							
1154 40.	70000000000000000000000000000000000000	-5.5949	4.1750	4.5455	0.0124	4.40/6	6.65/6	11.0524																
5	NUMBER	1019	0111	1011	1011	7101	7016	TUTAL					enge je						4 2 5					



NO. CONTROL BOOKERS INCOMES IN SECURIOR

Ç,

THE STREET STREET WITH STREET

	*S*A	NAVY - ACHH PLAT	ATFORMS - FATIFUE	ANALYSIS - MLW	105,0 FEET	0ATE 10/05/76	! f :
0 M	SET CACK IN TO SEE	7	THE THE THE THE THE THE THE THE THE THE	IN INSKIPS	Z=H	/*************************************	
26.3472	.0835	-4.1748	-884.2943 -590.7559	-741.4414	12,1606	OBLIGUE	!
	16,5265	-114.3693	744.2648	462.4899	-26.5352	UBLIQUE	
4545	00000000	117.0560	6910.0001	124.3601	44.8966 • 30.9159	GLUMAL UMLIUUE	
43.4109	-45.1572	-1.4781	-2044.5933	993.7458	-4.2017	GLUBAL	:
							1
							1
						•	
							1
]
							1
							-
							1
							!
							!
							†
							1
							! !
							· ·
							!



SPRINTER CRY MUUNCH ROMFURGE RAGE

100 100 100 100 100 100 100 100 100 100			U.S.	>	C	FATIFUE ANALYSIS - MLM 105.0	US.O FEET	DATE	10/05/76	1
19.01.0	# - 11 7 T	7	Z 4		X-FX-E	CHENT IN INSKIPSE		/ DOONE MAKES	/***	;
13,4012 13,4012 46,1053 46,1043 46,1043 45,4013 10,704 46,1053		•	8500°	5.2586	•	568,4125	-10.1700	310 t mil		!
30, 472	~ _	D	13.6112	5.1854	461.6423	-326,2423	82.9417	GLUBAL		
30,4,2,2 (2,2,2) (2,2,2) (2,2,2,2) (25.42	15.0045	66.0255	-604.7442	-350.4365	14,2847	UML TOUE		
30, a/38	- - .	6.5121	10,1050	/05/***********************************	000.4157	-353.786S	-45.5500	GLUBAL		
34.473	1	0.5141	25.6046	8457°04	592.00¢	-149.0072 -148.6515	12.6716	UNC 16UE		
		30.4758	56.4	4,0725	1653,7201	-626,6905	27.3973			1 1
		;								
								•		
										1
										1
							•			
										į
										İ
										į
										!
										İ
										į
										i
	!									į
										1

N. V

10647 1106 1106 1106 106700 10670 10670 10670 10670 10670 10670 10670 10670 1067	200		0.8	NAVY - ACHR PLATE	TFORMS - FAILEUE	ANALYGIG . MLE	105.0 FEET	DATE 10/05/76
9417.502.	2 Z Z	**************************************	IN KIPS		Z	Z.	Z=W	/ seekErykoss/
111120 1740 1750 1750 1750 1750 1750 1750 1750 175	00.	47.0647	8959°07*	-5.3684	-262,2393	-2131.0307 1280.8851	24.9014	CHLIQUE
1001.00		-61,1168	-61.120R	-250,7150	2050, 3243	1159.9076	-64.5618	OBLIBUE
144. 104. 144. 144. 144. 144. 144. 144.		-14.0270	-36.6356 -84.2778	244 C448	1860,1356		500 - 100 500 - 100 500 - 100 500 - 100	CELOBAL CBL 19UE
	ا د	-105.5185	-146,2609	3.9731	-558a,10a9	2966.2653	-205.2166	etubat.
	ł							
	!							



35456 XXXXX SXXXX

,	; ; i	•							1									1
	PAGE 6005/76		/**********/	UMLIQUE	GLUHAL	UML TOUE		GLUBAL										*
	0.800		Z=W	-17,5239	135,5537	10,363	19.7550	36.443B										
	FAILCUE AMALYSIS . MLW 105.0		**************************************	428.0081	-560.259a	-251 6011	267.4264	-1483.1304										
4 1 UN F UN	TFUMMS - FAILGUE		# #	110,4143	730.7#16	470.0210	5464.486	2661,2978										
U 4 W 2	NAVY - ACHH PLA	/**************************************		0,6840	96.0318	95.3174	4440.001	15,9296										
- -	.s.2	SESSINCE IN A POSSESSES	F • •	\$070°	7244.05-	28,1059	20.5324	83.0303										
	LUAD CUNUITION NO.	10		0/20.624	11.5004	25.423	10.00E	7075.77										
	LUAD CUNI	To I to	ACM SER	20101	1011	1101.	1015	TrifaL	7 7 7		, 3	- - - -	·					

S.

I CHARLE SCHOOL BESCHOOL SERVING

4.

F=7 F=7 F=7 F=7 F=7 F=7 F=7 F=7	1:	AT ONO A STREET OF A STREET			270	05.0 FEET	
12,500	;)	Z		/ IN TARKO /
10.12		10.054	-12,5666	594,7543	-0061°1904	57.4306	USLIUNE
14, 40.1	1	200100	-674,0815	6334.5865	10110150E	-1038.8203	SE URAL
14-4440 1450.0601 1450.0601 125.000 125		1 20° C'50 E	1504.700-	2011100	3790,3537	579.986.1	3001100
14.4449 +17474, 4176 9456, 7347 +556, 5352	- }	-207.0845	074,250	#5972,6340 #5972,6340	1850,0601	-164.5348	UHL I GUE
		**52,1486	14.0000	617474,4178	9456,7347	-536.3352	GLUBAL CLUBAL
	•						•
				ı			
	l .						
	ş.						
	l						
	i						
	1						



Ú,

		2 4 @ F 00	8. M	TION FUR	E 6 X A 8 B B B B B B B B B B B B B B B B B B	0 L Z M Z J		
LUAD CONDITION NO.	1110% 20. 6	•6•1	NAVY - ACMH PLAT	TFORMS	- FAIICUE ANALYSIS - MLM 10	MLW 105.0 FEET	VAGE 8 10/05/76	
a deadware.	/FUNCE		Ztu Atu	X=E	A STATE OF THE STA	Z=W	/***KEMAKKS***/	; ;
1010	14.0500	50000	11.3589	120.4764	1539.4151	194,2240	UBLIGUE GLUMAL	
1011	17.4647	38.1505	120.0104	1420,1042	-791.7868	-109.0128	UBL 1 4 UE	
2101	07000	20.5471	-104.5485 -104.5595	1451.0251	-4#0.0228 -470.9583	21.1591 -58.1407	UBLIGUE	!
TUTAL	63.5775	112.5424	27,9585	3962,4919	-2154,6283.	27.0705		! ! !
							·•	
								1
233								
\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\								
1, , , , ,								
								 ! ! !
, , ,								
<u>.</u>								
1								!

PAGE BENDING . ACAR PLATFURMS . FAITGUE ANALYGES . MLM 165,0 FER 3 3 6 3 3 3 3 3 3 3 2 2 2 2 2 2 2 2 2 3 41 55 47 MUMENT M2 U.S. NAVY N = 0 0 0 0 2 2 2 2 2 20,200 6 5 5 5 5 34 5 3 3 0 0 4 3 3 0 0 0 0 0 0 2 2 2 2 3 0 0 N 0 N 7 401 SHOUP AND SECTN -1 K アメン

	7										 -			
TERTER CACCE	7 T 7 T 7 C S	FUNCE	MUMENT	MUMENT E	T TENEBREAL PROPERTY	URCE	NOTSHOL	AXIAL	BENUING	5	CHEAR	TABLO	CCMB	
1		AIPS	INOKIPS	IN-KIPS	S d I Y	*	INSKIPB			ass K SI as			CHEC	ļ
100 -00 - 1	9	0		.01	_	000	9		c	0	00.		0	
	9.5	0	•	•	00	000	0		00.	0	00.		0	į
	•	0 (9	e :	Э:	30°	9	Э:	3	0	00		0	
		000	3 3	0 0	2 2	000		9 9	88			000	000	ţ
- 100 -10- 1	د د	0	9	-	7	9	9	9	0	9	90		0	
	3.6	00.	. 01	0		•	9	2	•	•	0		0	
		=	20.	70	00.	20.	00	00	00	00	00	00	000	
	0 0	00.	50.	-	٠.	•	00•	2	0	0	00.		0	
	3	0	40.	-	2	!	Э	2	0	0	00		8	1
5- 100 mlo- 1	•	0	ာ	*0.	٦.		00				000	000	0	
	3.6	9	3	0	3		3		0	0	0	00	C	1
 - 		9	>	9	3		9			0	00.	00	0	
	0 :	000	υ: -		00:	0.0	00.	9	00.	.0.	00	30.	100.	
	,	>	-• 1	pi j	> i		э.			0	00	00	0	1
5- 200 UKL- 1	•	0	.10	.14	00.	90.	S	00.	Ç.		00	30	¢	
	•	0	V		000	00.	\$	9	C		00	00	0	f
	7.	٥.	Ŧ	0		00.	ŝ	•	٥.		00	00•	3	
	5 · C		000	90	9 9	9 6		000	2 6		9	000	000	
	•	•	• .): =	•	•				•	í
- 505 -16- 1	o .		₹ D •	57.	Э:	3 : 0 •	3.	9	0	20.	00.	00.	0	
	9,	0.0	50.	010	ວ:ເ	000	0 :	2	្ទ	<u>د ا</u>	000	0 C	9	ļ
	• :	> :		/ D • /	> :	200	•) •	•	•	0.	0 0	0 (
	. e . s		70.	.11	000							0	000	
									•	. '				!
1 1011 107	2 4		0 1	. 20		9	•	9	0 0	9 0	0 0		C	
		٠, ح			>! =	200	> C	0 0) c		300		: c	1
	. 0	0	• •	• 5	000	90		9 5	•	•			, c	
	14.5	20	2	-112	9	000	00	3	00	01	00	00	100	
- 301 UKL- 1	•	ာ	7.	æ	•	•	~	99	00.	ķ	90		0	
	•	0	\sim	₽.	3	0	~	3	300		0		0	į
	~	20.		57.7	90.	20.	2,25	00.	0.0		00.	00.	000	
	•	0	v	•	.	•	~	9	10.		00.		C	
	Š.	0	2 ·	-	-	<u>.</u>	·	8	201		00		•	}
- 303 120- 1		•	~	94.	200	90.	•	00.	.01		00	90	0	
		٥.	3	3	Э	0	ે.	2	9		0	00	8	.
	•	٥.	9	3	9	20.	?	?	0		00.	00.	8	ı
	5 4 5	0 0	~1.	92.	o :	9 6	60	000	10.		0	0	000	
	ů			-	2	•			٥		5	=	Ç	

10.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0			## ## ## ## ## ## ## ## ## ## ## ## ##	M	1	**************************************
1.5	n 0000 0000 0000 0000 0000 0000 0000 0					
2						
1						
00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0						
2		00000 0000 0000				
200 000 000 000 000 000 000 000				00000 00000		
4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2						
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2						
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		00 0000 0000		000000		00 000
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		000000000000000000000000000000000000000		2 20000 0		3000
20.0 20.0		000000000000000000000000000000000000000		2000	9900	300
2		000000000000000000000000000000000000000		9000	900	
7.20 0.00			000000000000000000000000000000000000000			00
2		00 0000		000	00	•
2		0 0 0 0 0	000000000000000000000000000000000000000	• •	0	•
2.0 2.0 2.0 2.0 2.0 2.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3	20000	00000	000	•		00.
2.0 2.0 2.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3	000000000000000000000000000000000000000	0000	000		•	00
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		00		10.	00	00
0.0 0.0 0.0 2.51 1.2 2.5 5.0 0.0 2.5 5.1 1.2 2.5 5.0 0.0 2.5 5.1 1.3 2.5 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5		>	0.00	<u>ء</u> (0.	00
0.0 .00 .51 .1.5 .2.5 .1.4		00			00.	3 C
3.9 .00 .00 .00 .00 .00 .00 .00 .00 .00 .				•		
7.5 00 5.14 -2.9 1.3 00 7.47 -2.9 5.0 00 10.79 -6.3	90°	1.17	•		•	00
1.3 .00 7.97 -a.6 5.0 .00 10,79 -6,3	30	-			00	000
5.0 .00 10,79 -6.3	70	• -	000			•
	0.0	-	00		00	000
2 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		4				
		9 9			•	•
	00.	90	00		00	000
4.50114 .5	0.	90.	00		•	
6.6 - 101 - 6.62	00	900	00		0	00
00.00.00	0.	0	0.00	_	6	9
00.	00	2	00	20	•	
7.3	00.	00.	00.	00	00	000
	000	?	00	•	•	00•
	•	2	00	.	0	00
.0 .02	0. 00.	000	0. 00	9	•	9
0.0	00	000	0	0	00	009
0.0		0 0	000	6	00	
50 50	0			5		

STRAN MEMBER DET"AIL MEPORT

CONTROL OF SECURIOR OF THE PROPERTY OF SECURIOR OF SEC

						•			•					÷
1	-	UIST						43				- 1	N	
		ר א ט ט ט	2 ×	_	_	X 4 4 4 5 5 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6	•	5	X I A L T K E & S	Z >	7 ×	************************************	2 W W	C 2 1 4 4
	SEC 7.8	-	,	A X I	3 Y Y Z	χ σ	₩.	a i			S X = E	1 t		CHECK
	0 H 1 G +	0.	07	0	0	3		9	•	90.	•	00.	00.	3
1,	-	0.0		00	9 5	.		0 :	• :	2	0,0	00	00	3
1, 1, 2, 3, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,		. ၁	0		•	• •		> =	•		> 0			2 6
		7	100	.17		2		> >	2	00	Ò	00	0	
1	140-	0 0	0	•		_	0	-	-	0		00	00	0
		8.2	0	•	•)	0	-	3	Ç.	i	00	00	00
1		r. 0.	0	70	•	3 ·			•	٩.		00.	30.	0
11. 1		54.5	• •	• •	•	2 0 2 3			0 5	9		0 0	000	0 0
1			•						•	-			A	7
1	ישארי	0.0	0	16.		3	0	1.0	3	0		.00.	90.	0
15 1 1 1 1 1 1 1 1 1		20 ·	•	55.		∷c		2	.	°,		00	00	၁
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,		٠. :	Ç, (70°2		> :	9	٠	3	•		00.	00	C
1 1 1 1 1 1 1 1 1 1		6 9 7 9	3 (7.7)	٠		.	9		00.	00.	0
14.5 1		15.0	0	6.65		30.	2	٠. ا	~	•		- 006 -	00	0
123 123 124 125	3 123.	0.0	~	N.	=)	•	80	2	0		00	00	0
14.5	ĺ	~	~	.17	•	Э		•	3	C		00	00	S
1		3 .	۱ پ	21.	S	Э:		Э.	•	0		00	20.	00
14.5 1.0.0 1.1 1.0.0 1.1 1.0.0 1.1 1.0.0 1.1 1.0.0 1.1 1.0.0 1.1 1.0.0 1.1 1.0.0 1.1 1.0.0 1.1 1.0.0 1.1 1.0.0 1.1 1.0.0 1.1 1.0.0 1.1 1.0.0 1.1 1.0.0 1.1 1.0.0 1.1 1.0.0 1.1 1.0.0		⊸ ⊽	٠,) (i	7 -	> =	•	ာ :	•	•		9	9	0 0
7.2			!)	• :	.	•	•				
1	6 123-	0.0	- 05	. 14	Œ	2	0	~	3	•		00.	00.	Ç
		~ · · · ·	20.		~ ·	3 1	0	-	3	0		000	00.	0
UAL		7.5	70.0	5 0.	Ø :	> ;	٠	7	.	•		00	0	0
LUNCE 1 0.0 = .04 = .259 11.05 .12 .01 5.47 = .00 = .02 .01 .001 .001 .001 .001 .001 .001 .			100		, .	> 3	2 9	-	•	•		9	9	9 9
1 Unc. 1 U.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0					١٠.	•	> i	•	•	•	-		20.	>
14.2	1 046	0 0	70.	46.5	1.0	-	0	•	٥.	0		10	10.	0
14.5 - 04649001201			90	1.45	0	<u>٠</u> .	C	•	٠	٥.		100	10	0
125		7.7	70.	2 : V :	6	٠.	0	•	•	•		0	50	0
5 DAL 1 0.0 -0.1 10.44 -0.01 -0.00 -0.06 -0.1 0.02 -0.01 0.0		29.5	900	• •			0		္ ၁	0 0	-	00	00.	00
7.2 .201200000001000001000100000100010001000100010101000001010102000001020001020000000102000102000102000000010200000000000000000000101020000000000	0 125-	ن ع	~	12	0	9	•	9	-	20	•	00	0	c
14.5 .2015 .00 .001 .001 .00 .00 .00 .00 .001 .00 .00		7.2	N	., 12			0	0	•	0.0		0		
21.7 .20 =.13 .67 =.01 =.00 .06 .01 .01 .01 .00 .00 .00 .00 .00 .00 .00		14.5	~	•115	ຼ	(•	•	_	, Э	8		00	0	-
3 DKL= 1 0.0 -2013 1.200100 .00 .01 .02 .00 .00 .00 .00 .00 .00 .00 .00 .00		41.7	~	• 1 3	٠	•	°	Э	9	10.		00.	00.	0
3 DKL= 1 0.001 10.44 -6.570911 -2.320002 .00 .00 .00 .00 .00 .00 .00 .00 .00		0.63	~	13	7	•	0	90.	Э.	20.		000	00	0
7.101 1.75 1.200911 -2.320000 .00 .00 .00 .00 .00 .00 .00 .	S DAL-	ວ ວ	•	10.44	6.5	•	Ξ.	د. ۶	3	0		00	00	9
4.201 -7.49 6.960911 -2.320002 .00 .00 .00		7.1	9	1.75	7	•	٦.	2.3		, °.		00	8	8
1.4 = 10. 10. 10. 10. 10. 10. 10. 10. 10. 10.		э.	0	77.6	3	•	~		3	0		8	00.	S
		-	0	•	•	•	7	٠. د	•	•		00.	00	0

FATIGUE ANALYSIS EAST COAST AIR COMBAT MANEUVERING RANGE OFFSHORE KITTY H. (U) CREST ENGINEERING INC TULSA OK SEP 76 27-71-100 CHES/NAVFAC-FPO-7616 N62477-76-C-0179 F/G 13/13 AD-A165 651 416 UNCLASSIFIED NL.



MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963 A



PAGE U.S. NAVY - ACMR PLATFURMS - FAITGUE ANALYSIS - MLM 105.0 PEET LUAD CUNUITIUN NU.

STRESS UNITY	100 100	01	00.	000	01.	01	100	01	000	1	00	1 00	1 .00	.01	7	1 .00	1 .00	.01 .007	• • • •	1	00.		.01	00. 10	1	00	00	00.	200 000		000	01	3	1 .00	1 .00	000	100	.01 .005	100
SHEAR	70°							10.						10.									010						0.0				10.					.01	
BENDING BIREBO Y Z BETTERESTER	205	9	•	2 (•	•	0	.01	•	0				10.		•	•	10.	•	0	0		10.		0	0	0	00	0.0		•	°	.01	•	C,		0	70.	c
AXIAL SIMESS	00.	:	•	•	>	•	9	.01	3	2	.01	þ				-	-	. 15	-	-	-		1.			-		-	•		7	7	18	~	∹		0	3 0.	
TOKOLON	85.5	, .	7	7 :	7	is.	5	13.54	'n		5.	5.5	5.5	10 m		17.0	17,0	-17.01	2.5	17,0	3	2	85.8	•	2	3.	7.	. t	07.0				9.74	۲.	7	7	3	77.	•
URCE FZ FZ AIPS	2:	٠,	٠.			2	ت	•,2b	Ň	Ž		-	-	01.		• 20		52.			~		• . 26		2	2	~	2	62.0	u : ●;	.36	386	95.	98.	• 38	00.	000	00	ē
STEE THE STATE OF	10.1	•		•	•	•	2		`	•	70.	3	コナ	3 S		.63	603	50.	۰ ه	,63	•	S	15	٠.	J.	N		Ň,	# 5 V		15.	3	.,51	٦.	4	-		01.	
NUMENT /	18. 9.	`.	ñ.			00.8-	5,49	18,96	32.47	45.45	~	9	٥.	#18.80	-	Š	_	78.87	453°CT	-42,07	27.	6	13	ġ	۸,		-	•	1,77		N	5.0	4.7	10.01	1		Š	3 0 :	
MOMENT BY LV-KIPS	-7.35	•	•	•	ň	-10.57	.14,18	-17.79	-21.40	-25,01	-15.55	-13,28	-11.04	- C - 7 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1		-18.43					10,59	Ф,	3,15		21.0	21,26	17.24	15.44	2 4		4.05	4.81	14.47	20.14	25.30	-1.00	-1.55	77.	
T X T X T X T X T X T X T X T X T X T X	200	•		•	•	N	Ž	-1.20	Ñ	~	N	~	2	1.25	•	Š	v.	15.52	Ž٠	v.	£.	S	3 0	8 .		7.6	7.0	4 :	54°47	<u>L</u> į	₹.	3	450.46	₹.	3	•	0	90.	•
T S T	0.0		U =	• 3	· ·	•		2,3	•	•	0.0	101	6.3	7		0.0		· ·	a .	0	0.0	101	6.3	3 .	0	•	•	•	7 4		0.0	1:1	۲,	3.4	0.4	0.0	3.8	0.7	7 .
AND AND BECTA	טאני ז					164- 1										J.4- 1										364- 1				1						105-1			
2	300- 400					401- 501					401- 510					403- 503					403- 511					406- 500					400- 515					501- 502			



TO A LEASER OF TALE AND STREET

Chilt.

PAGE

	1810									>	•	
PORT PICTOR	7 2 L	FURCE FX FX FIFS	ACAENT AY AY LVEALPS	MUNENT MA IN-KIPS	A FURCESSES FURCESSES FY FURCESSES FY FIRM	FUNCE/ FZ KIPS	TURBION MX INEXIPO	AXIAL GIREGO	BENDING STRESS	S STEAR SIRES	SHEAR	CONTROL OF THE CONTRO
01- 504 105-		1.90	•	2.5.4		10.	5	40	- : :: ::: · · · · · · · · · · · · · · ·			
	3.8	-	70.7	₹	9 9	0	96		•			607
		20.1-	2.	7.		10.	95				0	.005
	1104	9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	74°•	1.56	ल ज ल ल • (100	90	90		000	0.0	400
104 010		•	3 30	י מ	-	y			, 			
		72.5	-20.11	28.1			75.07	200	•		9 6	V
	200	~	-10.50	-45.50	05.1	1 30	24.07	20.	• •	100		
	9 -	.2.27	57.0	52.94	1.50	3 30	22.07	200	- 1 I		60	200
	İ								•			
01- 622 200- 1	o -	1.97	4.73	25.55-	2	•	30°	SO.	£1.	100	70.	800
	10.2		5.57	t :∃	07		20.0	2 2	90	5	100	500
	15.3	1,97	-7.41	×.	61		7			0		900
	20.4	O	•11.53	23.56	20.	900	\$ 9 .	506	115	5	5	609
502- 503 165- 1	1 0.0	1.21	-1.11		60.			9	70	96	00	400
	3.6	1.21	-1.20	-2,12	90.			90	20°	0	0	.003
	7.0	1.21	-	S.	90.	•	•	70.	10.	00.	00.	.002
	15.1	1.21	-1.47	5.00 5.00			. 21	9 9	m .co	9 9	9 0	. 00 o
	i	•				•						•
-601 -06 -30		3 1 1						9 3	20.	•	9	9 4
	-	70	93	10			20.	3	00	900	00	
	11.0		.17	N	10.	00	50.	3	10.	00	00	100
	15.2	.04	979	04.	10.0	200	50.	9	.04	00.	00	.001
02- 505 105- 1	0.0	***	7.	င	00	00	60	02	0	00	90	0
	, v.	~	-16	~	9	200	60	22		8		0
	7.6	., 24	10.	M.	20.	90.	6 0.	- 02	•			9
	15.2	22	2.5	.00	2 2	000	999	20.	100		000	700
63- 505 165- 1	1 0.0	.67	45	4.01	÷0.	.00	_	20.	* ***	•	90	0
		19.	18	-5,17	≥n•_	10.	~	20.	.03	00	0	8
	^		50.	∢ :	20.	0	~	20.	20.	80.	0	8
	15.1	•	20.	000			0/0	2 2		9 6	000	N 00
030 404 3150		40.04	25.4	- 3	12.15		14 910		•	; : 	•	
•	-	10.75	3.45	-11.90	: :	•	-35.61	. 2			200	
	2.0	-54.94	-12.00	10.1			-35.61	2.5	10.	2	2	.012
	•	20°08-	45°25°	52,10	.	£ :	-35.61	4.04	•	5 0.	50.	_
	•	١			,	3		1	**	•	•	•



: (%)

STRAN MEMBER OFTAIL REPORT

	5					-					-		i
PERSONAL GROUPS	702	FURCE	MINENT	MCFE'S I	P-SHEAK	FUXCR/	TORSION	AXIAL	BENDING	STRESS	BHEAR	SHEAR	BLOS
	2 4 4	4 2	2 X X X	7447	2	80LX	4	7 1			- 1	ש אב ה	
•				J. ▼ si ii si	4		1) }]·		1	•	ł)
1 -002 529	0.0	-4.10	2	-		61.	÷.	7	-		10.	.01	•
	S	-	•	2	•	21.	*	٦.	0		0	0	00
	Э,	-	→	-4.72	∍	•19	-1.46	•.11	03		10.	• 0.	• 007
	s		~	1.	₹.	• 19	7.	₹	•		• 01	• 01	0
	_ <00.3	∹		1	•	60	-1.46	7	7		0	10	20
505 105- 1	0	_	7	^	э	00"	Q	9	•		•	c	6
,	• 5		: -		, ,	•	9	20	• •				•
	2.	10		\$2.	3	20.	30.	20	0	i	0		100
		_	7	-	Э	00	3	3	0				0
	Š	-	٠ •	►.	3	600	3	9	0				0
	•	a	4	1			•	- 4	•		;		•
	-		9				> =				>))
				36.1	60	0	•	• •	•		, 0		3 5
	-		3	10.00	•	0	, 9	2	. 0			•	
	15.2		1.84	9,37	60	.01	1,06	•	0		0	5	007
	•		1		;		•				 ; 		,
1 -601 006	.	0 4	٥	.	• :	0	-	2 6	0 (00
	•	, 1	4	n c); •	5 C		> :	> 0		9		9 6
	•	, 1	9 3	•	•		•	> =	> C		o c		9 6
	15.2	9		7.03			97.	200				3 6	900
			,	· !	•	•;	•)	•				•
606 JLS- 1	5	17,90	22,54	0.5	~	.34	\$.27				10.	_
	1,5_	0	Ð	2.4		34	2.5	729	0		0	.01	5
) • ¢	٠,	3	Z .	7	3 N.	٠, د د	.27	0			10.	5
	3	97.90	BO . 1 :	15.26		•	-5.39	.27	50°			10.	.013
		2	•		~	96 9	7		0	-		10.	•
624 200- 1	5	7.	10	٠,	V	70.	2	.07	-		.02	₹0.	-
	5.1		3	3	02.	0	2		90		205	20.	0
	•		•	0	v	0	•		0		20.	20	00
		2,73	98.	-10.21 -21.24	2	20.1	£6.1		•0•	4	7 0	٠ د د د	900
		· ·	•	•			•			,			•
710 71-	0.0	\sim	•	31.7	~	N	5.5		0 9			• 01	0
	ů.	~ '	ġ.	3.4	•				40			. 01	0
	:	יי	?•	2	• :	v	,,		10.			0	0
		1.25	D 7 8 7 9 6	17.050	27			5	•		.	0	700
	•	•			•		•						>
711 Pl- 1	1 0.0	38,55	3 :		., 73		£6.0	.17	00.		0		0
		֓֞֜֞֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֓֓֓֓֜֜֜֜֜		200	•		2	→ •	0		0		-
	ů.		٦:	2 0 =		000	•	.17	• 01				
	•	יי	7.0	3 · / o	`	•	•		-		o		5
							•				•		•

:										Č		108/11	
			U.S. NAVY	F - ACHR PLATE	DKHS .	ATTOUR ANALYBI	N I II	105.0 FE				9116917	!
l	TSIO	į			į			1			>	2	
THESER GROOT	A 4	30404 F x	ACMENT A×	FOMENT A	/eeesuneak	/ OKCE====/	NOTONOL	AXIAL	BENDING V	STRESS	SHEAR		COMB.
SECTA		A 1 4	LNEKIPO	INSKIPS	X I P &	2 T T	INSKIPS			81			- 43
512-712 -11-1	0.0	9.	25.30	25,34	•	98.	~		•		10.	.00	0
	•	-39.46	54.68	17.90		•39	~	~	.03		101	10.	•
	~ °	07.05.	07.72	12.45	•	٠. د د د د د د د د د د د د د د د د د د د	~ !	~:	•		5		5
	25.3	39.46	143.02	1.55	20	92.9	9,75	9	60		10	70	011
- 621 JL6- 1	0 0	2.1	11.47	-77.99	1.1	90	\$	3				,	2
; ; ;	5	2.1	17.41	449.10	1 1	37			•				, -
	3.5	-2.15	22.05	-120.34	1.10		36.54	20.	00		100		700
	9	2.1	26.27	-141.05	2.4	930	6.5	3	•		0	0	3
	0.1	2.1	33,07	-159,61		. 30	9,5	3			20.	20.	0
• 625 JLb• 1	0.0	- 5 4. 7 th	-14.12	45.12	•	₫	2 2	4	•		C	6	2
	5.	-55.78	30.30	62,33		• •	. E	20.			5 C		; ;
	-0.5	-53.80	14.07.	17.6/		0	36.2	2	- 0		100	100	5 5
	9	-53.83	B5.48	95,51	•	•	38.2	~	0			10	• -
	100	-53.86	-95.75	110,57		5	2.0	~	9		103	00	•
• 626 JL6• 1	0.0	47.90	47.28	11.41	•	3	7	,	C		Č		=
	1.5	57.90	55.68	20.02		9 0	E 1	12					-
	3.0	57.90	01.00	41.91	•	970	5,45	~	70			-	0.0
	9	57.90	72.51	25.40	7.	97.	5.4	.27					5
		57.92	80.50	25.49	3	100	3.	12,	Ο,			101	_
- 651 JL0- 1	0	2.1	32.94	-159.53	7.	~	6.7	02	• 10		0		500
	1.5	2.1	38.19	-174.33	•	, 28	6.7	2	-		20		500
	3.0	2	43.36	-164.00	3.	~		3	-		0		900
	e -	20.15	40.00			2 1	36.74	2 .	71.		~	ر د د	900
						v		>			90.4		
- 703 20D- 1	0.0	1.97	-11.55	43,50	3. ·	*0**		50.	**			10.	0
	5.4	1.99	-11.26	24,51	9	0	7	Э	-			0	9
	10.0	2.01	.5.01	15.04		. 12	-1.13	\$0.	60.		20	20	•000
	10.3	20.5	00.5	28.20	₹.	12.	~	S > .				03	C
	2	60.2	61.15	-34,10	ζ,	, 29		50		•		201	_
- 653 JL6- 1	•	-33,80	-96.10	109,94		•	36.4	~	•		10.	.03	.015
	•	-53, HU	-105.90	122,54	0.	3:	38,4	~	_		20	2	5
	S.0	-53.74	-116.40	132,91	•	12	-38.46	# 5 4	11		20.	20.	9
	•	-53.66	-115.77	140,96		7	36.4	¥	₹		20°	20.	5
	•	-53.62	-110.08	146.85	7	900	36.4	2	~		201	- 70° -	5
- 701 200- 1	0 0	2.74	-1.55	-21,48	7.	•	•	.00	_			0.0	-
	5,5	2.75	-4.50	-45.45	3	0	٠.	Э	, 14			0	0
	0.4	2.17	-4.71	-18.56		10.	1.92	40	• 10		10.	10.	900.
	C . D .) V	70.7	3		¢	3						c

CALAN AREGER OFTARIC REPORT

RESERVED BELLEVER BESTERE BESTER BEST

(3)3

######################################



PAGE

7 L 3 d 3 d 4 d 4 d 4 d 4 d 4 d 4 d 4 d 4 d) : 7 4	4 2 3 1 1	#CHEST	_	/essenteax furce		TOKOTON		BENDING	ひにはないの		TAN TO	
-000		A I PS	BALXON	IN-KIPS	20 X	Selv	Salvevi	0 I NE 00	-	, xxxx		¥ .	CHECK
	0	15.6-	-23.72	86.65-	75.	.27	-1.25	~	•.26		90	90	120.
	12.5	-6.20	5.17	16.70	7	-	-1,25	7	10		20	8 0 g	0
	45.1	. 4.20	15.02	47.02	3	٥.	-1.25		-10		70.	.0	-
	57.5	-6.10			. 43	51.1	-1.25	• •	10.		~ 0	20.	.013
	~ ~		*	- 58.60	07.	~	•1,25		. 24		207	- 6 0 <u>8</u>	020
02- 705 157- 1	c 0	٠.	30.	.6,53	7.7	•	.30	.22	.12		.05	• 0.8	
	4.7	٦.	5 P. P.	P. 1-	•	•	0.50	, 22	10.		10	10	5
	•	4.10	\$0.	3,51	•	0	0.50	. 22	• 0 •		100	.0.	3
	16.8	 	11.01	2.00	9.5		900	42	200		0 -	0.0	200
			:			•	!	:	i			} . ; 	
1 -/01 +0/ ->0/	5 F	3 3	,	3 1	9		-	3 6	•		o 6	0	100
		30	7	3	> =							36	> c
	14.1	30	71.	72		0							9
1	10.8	70.	.27	7	0	0	01.	9			00	0	8
105- 705 107- 1		88.0		00.44	\$1.0	00	90,0	=	-		6	Č	2
•		07	-14	1.15	3	00	70	•	10		5	0.10	700
!	3	17.	\$0.	2.64	. •	30.	70.0	£0.	00		00	000	00
	1001		.0.	79.	40.	20.	70.	3	- 05		50.	10.	
	16.8	59.	20.	*0°5	• 13	000	300	9	-11	1	20.	- 20	0
763- 705 137- 1		•2.70	-1.73	*8.58	Lo	.01	-,26	71.	.15		10.		010
	7.4	-2.76	=1.26	58.1	.07	•01	• . 26	~	0.0		0.1		5
	3	-2.76	97.	11.11	L0.	10.	• . 26	** 1.4	0		10.	.01	
	7 .	97.70	75.	50.5	•	0.	92.	7	. O.		- 0	٠. د	-
	6.	6,10		0, 50	7.	100	99		•		100	- to•	_
703- 801 200- 1	0.0	^	-3.75	49.22	65.		~	٦.	92.		.03	.03	• 022
	12.5	~ .	47.5	15.00	97.		4	-	80		90	70	0
	1,00	000	• •	75.55	•		∹.	∹.			9	0	5 :
	20.5		10.05	\$4.75	35	0			20	ļ	20	20 0	3 2
705- 805 JL7- 1	0.0	-51.64	-31.58	~	~	-1.07	-	3	60		90	90	0.00
	~ :	-51.54	-92.78	3	D 1.	•	~	3	-115		20	20.	20
		70.10	CV-001-	~ •	A 1		⊸ .	.	• 15		20.	70.	920
	7.7	151.95	14.02	75.02	26.	1,006	11.42				9 6	900	9 10
				,				•	!				
104- 705 107- 1	0	70.	10 (1 10 (1	# to # #	3 T .		£0.	70.	• 14		₹0.	*05	900
	• •	7 7	2	2	5.5	• •	50	ວ :	100		5	5	0
		1 4		7.4	3	•	7 7	*	9 9		• •	9.0	Э (
	• I			20° F	3 3	2 9	9 # > °	•	N 6		~ (70	500

THE THE THE THE THE THE THE THE

(1)

HAS HAVE MANAGED POLICION WHO WAS THE WOOD OF THE POLICION WAS AND WAS

												;	•	
TERENT	S KOUP	1	FUNCE	MUMENT	- Z	EARF	UNCE	TURSIUM	XIAL	BENUING	STRESS	SHEAR		
ل	SECTA	֓֞֝֞֜֝֝֓֞֝֟֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֓֓֓֡֡֝֓֡֓֡֡֡֝֡֓֓֡֡֡֡֝֡֡֡֡֡֡	8 d l x	2 1 x = 2 1	8414-11	2 X	SATA	SAT X=VI	֡֝֝֝֟֝֓֓֓֓֓֓֟֝֟֝֓֓֓֓֡֟֝	- 1	2 	- K	4 F	C C C C C C C C C C C C C C C C C C C
4	1 130	4	3		r u	٠	•	•	•	•		;	•	•
-			200	27.1	V 40.	70.	9 0		•			•	•)
 		3	30.	1.58	50.5		10.	35	30.	0		0	0	500
		14.1	•• 90	3	1.02	2	0	55.	•	0		01	10.	õ
		10.9	- 1×0-	-41/5	-5.31		0	~	•	0		0		9
100	157- 1	0.0	-3.42	35.	-1.70	?	0	7	7	0		0	0	-
		4.7	3.42	40		9	Ó	-	1	0	;	00		5
			-3.44	1001	79.		10.	12	. 1.8	20.		00	00	. 013
		14.1	-3.42	1.13	1.81		0	-	7	٥.		00.		$\overline{}$
		20	-3.44	000	3.00	>;	•	-		•		10		_
80.5	200- 1	0.0	11.28	29.95	=14.78	2	~	1	-	-		Ą	=	6
. 1		12.5	11.22	-3.67	1 4 2 4	70	-10	. 23	05	0.3			0.0	015
		45.1	11.19	-10.55	3,93	7	0	7	52	-		00	00	2
		37.6	11.17	-13.56	99.0	9	~	~	~	80		0	C	•
		50,2	11.18	13,45	1,97	ď	N,	3	\sim	0		10+-	. 01	5
0	11.70	0 0	***	3 5	20,000	£	•	9	7	•		4	•	-
)		7	20.48	75.67	14.68	***	Š	20.0	7 7					• ~
		74.5	49.40	94,10	39.45		0	20.0	42			20.	20.	~
		61.3	50.62	60.72	57.83	•	15.	-50.05-	. 42	200		10.	F O.	. 023
		7	69.45	7	13,10	7	۰.	2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	4.2	0;		40	70	~
010	1 -54	0.0	~	10.40	-250.46	•	ď	3	9	-		00	00	0
		~	~	41,67	-227,74		~	2.5)	10		00	00	ိ
		3	۲,	14.14	-205,02	•	ď	5.4	000	0		00.	00	0
		21.3	1.23	00.4	162,50	12.	12.		00.	91		00.	00	600
		В.	•	666.33	95 4 619	•	V	T	900	200		00.	00.	C
611	1 -74	0.0	5.5	-204.67	•	•	-			.13		.01		~
		7.	8.5	-191.57	0	32.	₩,	~	~	₩.		101		5
		7.5	S .	-176.60	v.	s,		7	-	00	٠	10.		5
		7.17	65.54 65.64	80.4011	47.50 41.50	, ,	0 4	20 1	51.	200		?	<u> </u>	0.00
) .) !		7			-	•			101		\$
816	F2- 1	0.0	•	~	Š	•	-		~	0		00.	00.	_
		•	è:	∿ .	Q:	٠,		7.	~.	C.		00	00	5
		•	•	~ :	Ž <	•	⊸ •	•	∹.	÷ (0	0	5
			65.00	178.74	107.48			C 10	9			9 0	9 0	100
1	İ		•		1	•								•
9 0 9	1 401	c •	12.	2.11	7.76	30.	10.	7.		2		10.	10.	\$00
		n ,-	v	1,03	9,16	5.	2	4 :	Э:	0.13		00	00.	Ö
		- ·	12.	1.64	97.0	` ·	•	3 :		9		(c	10.	ō (
		٠,	v	•		67.	2		>	2		> 0	9 0.	
		•										•		

COMB. 00000 00000 446.00 0000 0000 00000 00000 # 0 0 0 # 0 0 0 000 00000 12/05/76 W W = W W 2222 20000 2222 2220 00000 N - - - N N - - - - N 22222 . M N = N M 20000 83888 20000 00000 20000 22228 - 6 M 3 N 0 0 0 0 0 20000 - 5'5'F 00000 FATIGUE ANALYSIS - MLM 105.0 FEE AXIAL 00000 3 3 3 M M 2222 22222 22222 27.10 27.10 27.10 27.10 22,222 7 7 7 N N N N N N 10.1 N 0 0 0 0 00000 2222 22202 20000 00000 4 2 2 2 2 20000 4 to to to 2222 S ACAN PLATFURMS 20.39 62.02 54.07 25.25 MUMENT MA IN-KIPS 3.43 61.41 62.45 5.45 E U U E E O O C C C 117.90 1 1 1 1 1 2 2 2 2 2 3 2 2 2 2 3 2 2 2 2 2 \$ 0 0 0 ¢ N S S C O 2222 0000 0.00 11.00 14.00 16.00 1 2 - N N 3 27.17.2 24-5 PEN STA SECTN CUNUITION 200-907 100 7 4 6 407 805 9 0 **3**0

64

D

مينار. معالم

W.

2	12 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	HUMENT HZ IN=K1F8 = 9.80	**************************************	F				97	BHEAR	7 7		
2	113 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	7 P.S 8. F.C 5.29	とくいしのりしりり	֡					とせいこの			
4 600 2 00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Y	A A A	*	24	NOTE X	A F S C		207	BTRESS	6177 F	CNITY	
2		O 12	Salx	KIPS	Salkeri		•	81		/	CHEC	
4 6 6 1 6 1 6 6 1 6 6 6 6 6 6 6 6 6 6 6		ŝ	•	0	7	1.3	90.		00	00.	• 0 5 9	
4- 605 108- 1 5 9 9 4 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		•	•	0	4	٠.	#0°=		0	90.	3	!
2- 605 108- 1 5 7 1 1 1 2 1 1 2 2 2 3 3 3 3 3 3 3 3 3 3 3		9.4	•	9 6		? "	0.0		8	9	Э;	
4- 605 108- 1 0.0 11.4 17.1	1, 1, 2, 4, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	8.23	0.3	30	2 4	95.	60		000	000	620***	1
2-800 146-1 0.0 -2 17.1 17.1 17.1 17.1 17.1 17.1 17.1 17.	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		7	0	7	9	-		60	0	2	
2 800 146 1 0 0 0 62 62 6 600 146 1 0 0 0 1 62 62 6 60 6 146 1 0 0 0 1 62 62 62 62 62 62 62 62 62 62 62 62 62	23.00	1.00	50	<u> </u>	00	63	90			0	M 000	'
4-806 144-1 0.0 -2. 17.1 -2. 17.1 -2. 5-806 144-1 0.0 1.4. 17.1 -2. 17.1 -2. 17.1 -2. 17.1 -2. 17.1 -2. 17.1 17.1 17.1 17.1 17.1 17.1 17.1 17	01 2 2 2 4 2 5 1 5 1 5 1 5 1 5 1 5 1 5 1 5 1 5 1 5	2,79	ີ•	•	•	Э	C			00.	9	
2- 606 146- 1 0 0 -2 1 1 4 -2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2	2 2 2 3 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	79.	90.) (9 6	9 F	٥ •		- C		200	
2	1 444 1 444 1 444	٦,		-	•	6 4 5	- 010		900	9 N E)	!
2 600 1400 1 0.0 1 1.4 1.7 1 1.4 1.7 1 1.4 1.7 1 1.4 1.7 1 1.4 1.7 1 1.4 1.4 1.4 1.4 1.4 1.4 1.4 1.4 1.4 1	1 2 4 7 8 6 6 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	-8.23	4.14		1	7	-		7 0 °	. 0.2	5	
2 600 14de 1 0.0 1 1.4 1	20.2	2 3	700	70	7	-	3 9		100-	100	5	
5- 606 146- 1 0.0 1 1.4 1 11.4 1 1 1 .4 1 1 .4 1 1 .4 1 1 .4 1 1 .4 1 1 .4 1 1 .4 1 1 .4 1 1 .4 1 1 .4 1 1 .4 1 1 .4 1 1 .4 1		70,5		9	7 "	• -	•		•	2	5 6	
5- 606 146- 1 0.0 1 5-7 11.4 17.1 17.1		3,0	40	0	97	. 13			200	000	7 7 7	
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1				!	; ;	, '		 		, ,	1
27.2	, , , , , , , , , , , , , , , , , , ,	70.0	0 4	V 100		•			5	5	9 0	
1701 10 66.8	2.21	1.70	99	0	• •	3	30		100	10	> 0	!
44.8	2.00	5,96	3	0.0	9.38	9			0	5	000	
	27.7	10.15	90	0,	•	3	970		100	.01		i
7.8	15,11	41.26	77	70	-	1	*		,	-	3	
0.7	3	13.50	2	•	: =		10		0	6	010	
24.8 7.46	-2.74	-31,40	00.	.03	1.15	15.	91.		8	9	.017	i i
0.8 7.3		2	12.	•	٦.	N 1	Ð .		5	10.	.013	
0.	2	45,54	•	200	7		124		50	0.3	020	!
.0 61.	3.68	æ	•	19.	9.0		• 01		70	70.	.015	
6.1	Ð	E.	-, 18	•	9.0	M.	200		£0.	00	9	!
6.2 61.	.	ન્:	च ()	•	D	~	0.		9 0	50.	• 016	
20.00 TA .000	11.01	1.50	. 58	91	30.61	25	002		3 3 0	90	016	1
5.1 0.		ŝ	£4.4	•	ď	00	207	٠.	00		3	
801 102	29.5	7.	4.2	0	Š	•	50			0	0	
6.2 1.2	52.4	-76.68	8 T S	0	· "	Э	50.		0		0	!
64.5 1.65 57.4 1.75	47.05.	35.66	8 8 2 3 4 5 5	900	55.57 57.57	9 9	N 6		6	0	200	
	,			ļ	•	•					>	
	-151.00		05.	4	•	31.	100			• 01	_	
		V .	05.6	۰, ۵	•	513	70 9			10	0	-
	10.07	10.21	05.	9 4	0 4 0 4 0 4		100		5	.	0 (
2.44	; ;	. 2	0.7	, c	• •						- 0	

7 * # C 1.00. NAVY & ACHA PLATFURMS A FATTGUE ANALYSIS & MEN 105.0 PRRF

		FUNCE	TABE(IE)	このまった			TORSEON	AXIAL	BENDENG BT	PE 56 ST	SHEAR	SHEAR	COMS
024 X35672	0.4 P. 1.4	841 x	867 X-27	Sdl Meni	70 A T Y	KIPS	INSKIPS.	1 KE 33		į			U V
2- 915 -5	. 1 .	-30,45	178.19	7.4	-	e.	•	911-	000	•	3	10.	-
!	Ð	-34,45	117,03	-	91.	50.	080	97.0	000	-	Ò١		9 (
	10.6	٠,	50.47	~•	٠.	ę	•		0 0	•	Ъć		- -
	•			?,	٠.	c 4	•		•	• '	> <	•	9 0
	36.4		60.00	•	•	E.	•		•		•		•
1- 902 184	5 7 1 -	-1.41	3.14	1	*0.	0		5	00.5		Ċ	10.	Ċ
)	r	. ₹	: ±	-	10.	10.	30	5	-		ø	C	~
	15.7	3	1.73	^•	07.	Ò	7	_	0	•	Ġ	- 0	0
	4.0%	1 7 7 1 . 1 1	70.1	.52	£ .	10.	6.63	00.	20.	•	S	0	\$00
	27.4	-1.41	\$5.	£	53.	0	5	-	0		9	101	•
301	-	1	9		2	0	30	۳,	7				018
253	· £	, ,	• •	11.	99	10.	0.00	97.	60	•		6	010
	15.7	. T	8/-1-			10.	2	01.	9		30	70.	0.1
	8.0 %	*	-1.07	•	9 0.	C	2	-	•	•		300	.015
	47.4	-3.83	٠,	•	90	10.	10	01.	Ċ	1	-	101	• 015
101-1001 JL9	0.0		-17.11	-		\$0.	-13,99	00		•	M O	100	C
		50	-15.64	£		0	~	00.		į	20.	50	c
!	10.2	20	15.01.		50	70.	413.8	000	*0*		#.O.	10	200
	3	00.	-7.01	500	•	0	4	00.		•	70	20.	Ö
i	36.4	90	1.54	200			4	29.			20	200	C
1-1002 18U			40-2	ç		0	04.41		*0	•	101	10.	. 012
•		T.	1.50	3	3	٠	06.1-	٩	•		10.	Ö	0
	41.1	5	1.24	2,28	50.	00.	-1.90	.41	₹0.	•	10	6 01	•011
	51.7	E.	3.	T	3	•	2000		10.	•	٠ ا	10.	.010
	44.2	5.	*/.	9	3	0	1.90	4	40.			Ç	5
1-1004 150		3,4	79	•	10.	10.0	٥	6.43	ò		3.00		_
		•	***	3.84		10.		4.43			100	10.	9
	41.1	4.6	1,68	0	10.	10.	Ď	2.43	0	•	- ;	Ċ١	⊶.
	51.7	f	£.5.		>	100	0			•			-
	44.2	7.0	-5.41	4	10.	1000	•	590		-	10	0	-
4- 405 164	3 1 0 ° 0	;	eć.	0	2.	0	15.	£ 5 •	0.0	Ī	300	10.	• 0 0
1		ĩ	\$0.	0	7.	0		40.0	•		0	10.	\$000
	13.7	; !	-1.85	1 H.	2.	10.0	.57	90.	•	•	. O J		\$(.0.
	40.0	•	.5.U3	ę	•	9	.57	40.1		•	 	90	900.
	47.4	;	27.50	S.	3	0	15.	80.0			30	10.	8000
\$01 HOD #2	0-0	900		=	٠	20.	.36	07.	0				200.
	,	•	05.	• • •	3	00.	.36	00.	- 0 S		10	104	000
1	13.7		10.	Ň		000	95.	000	0.				3000
	A. 0. A		55.	.1.	10.	20.	•\$•	00.	•	•			.00
			•	ì		: *	•	* 1	•				

STRAN MERSER DETAIL REPORT

(C.)

	2										>		:
HERRER GROUP	•	FUNCE	MOMENT	HUMENT	MAM	FUNCE	TURBIUN	XIAL	BENDING	STRESS	SHEAR	×	-
SECTION AND SECTION		× 1	¥ 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	7 L	7~ E	7	M ·		>	~	THES	æ	としている
2	1	L •		0 1 4 2 1	•		4						3
02- 905 104-				•	3	0	-	>	0				0
	•	-	54.	S	٠.		-	2			9		0
	15.7	•	£7.	£4.	00.	00.	• 1 •	10.	70°-		00	00.	.002
	3	_	07.	۲.	3	0	-	•	٠.				0
 	~	-	. t n •		•		~	?	۲,				6
03- 905 169-	0.0		•	7	=	C	-	•	•		•		-
	٥	•			•	, 0	: -	•	•		, c		•
	15.7	2 2 2	-	62.20	2	70	• ~		0	•			•
	40.0	•		2.2	2	0	-	07.			0		5
	7	•	Ž	1.7	•	0	-115	v			00	30.	5
	÷	•	•			•		•					
-091 2001-50	• •	, .	67.	•	0 ·	.0.	00.	m. 21	00.			.01	• 013
	•	. u	0001	3 :	າ :	000	3	'n	20.		00		<u> </u>
	•	. 1	55.7	•	?	•	>	ď	•		10.		3
	٠,	E 1	1/010		?:	•	2 (4	9				.
	•	•	00.5			2	>	•	2		10.		<u></u>
03-1003 319-	0.0	_	41.67	- 59.15	3	7	1.0				0.		0
	20	1.2		~	91.	~	7	3	•		0.2		
	10.4	-1.24	2.	-2.14	3	•00•	11.49	-, 02	00.		10.	.01	0
	3 ^	-	.	٠,		5	*	• ·	0				9
	v	•	•	c_		u.	7	2			-	0	_
03-1005 180-	۰	4.	-5.74	44.55	•	.01	~	٠				10.	\sim
	10.0	-10.H3	٨.٧	•	13.	10.	1.51		•		104	0	920
	-	•	7.7	-	?	0	~	٠.	•				* 0 5 4
	٠,	10 (05.1-	-	•	10.	~	•	•				~
		£0	`.	•	•	0	•	7	•		0	0	~
-601 506 -60			51.	₽	Э	0			0		00		0
1	•	115	•	90	000	00	711.	2	20.		00	00	001
	15.7	-	15.	~	>	•	∹		0		00.		00
	ď		07.		2	•	7	Э	0		00.		0
		-	>	\	>	•			0		00		0
-691 906 -70	•	3.9	*5*	٦.	٦.	0		٦.	•				5
	ċ	~	٥	-2,65	3.		٥	7	0		0		_
	15.7	J	~	70.	30.1	10.	.63	16	05		.01	10.	.013
		٠,	•	ς,	•	0	٥	~	•		0		•
	•		~	=	•		•	7	-		0		_
05- 906 169-	•	7	11	٤	٠,		7	-	10		0		2
	•	^		3		9	7		0		0		•
	13.7	4.73	3,25	1.79	. >	₹0.	710	• 1 •	70		00.	000	.011
	•	۲.	•	÷.			٦.		10.		0		-
	r	٢	4	•			٠	•	٠				

1

1

STRATES UPPER UPPER SEPURA

2	TSTO		L Z U F C X	N J M J M J M J		- 5 <u>7 8 1</u>	1010 P. O. O. O. O. O. O. O. O. O. O. O. O. O.	× 1 × 1	10	3	→	24	
UMMEN AND		7 T X	84 X X X	. ø	X I P S	2 4 8 4 I A	XXX	STRESS /	>	2 = X S T = = =	STRESS	STRESS	CHECK
0-1004 18C+	1 0.0	7	2.43	~	2	•	•		0		0	00	
! !	10.0	977	1.04	-1.95	3	00.	15.	. 63	20.		00	00	3
	Z1.1	•	-	11 X .	: •	•	.51		0		0	00	5
	\ • 1 o	•		75.		•			•			00.	5
		•	67.	67.1	•	2	15.		0		0	00.	_
-1005 180-	1 U.C	10.68	24	~	Э	0	1		0		.00		02
	10.6	¥.	66.	~	•		36	3			0		-
	21.1	c (2.5	-1.59	3 :	0	M :		0		00.		5
	5 1 5 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4		4.00	3 2		0 0	9 7	4 4	10°		0	000	0.0
	!	•			۱,		١.		>.				v
-1006 364-	1 0.0	1.25	-33.44	9.50	•	4	•	20.				2 0.	0
	- G • F	~	⊸.	25,50			3		C;			10.	0
	16.2	1 · 1	14.11	70°92	60		6.59	20.	70.		7	5	200.
	7	•	•	70°71	~ ′	~ ·							o
	36.4	-	10.10	180.00					0			- 105	2
- 910 75-	C.0	۶.	35.34	24.	•	-	5.5		0			0.0	0
	1.0	~	10.01	5	65.	-	5.5				0	10.	0
	16.2	•	7	9	n.				0			0	0
	52.4	1.25	-39.73	96.98	5.0	01.0	75.57		. 20				000
		ى) di	' 7						
	0 0	44.55	-147.64	1 E		3	0 20	1					9 0
		·	47.48	 2	v	œ		-	.0				5
	•	٠	16,24	14°64	·,	€	Ω.		0			. ·	0
	٧.	S.	98.05	72,45	J.		2					10	0
- 912 -	0.0	10.05	146.75	-27.94		•	30	~				0.1	_
	XO.	70.05	134.60	-37.77		0	Ð	7	0				0
	• :	7 ·	V4.00	04°75"		•	0	∹.	Ç				0
	24.54	150,40	40°40°	72.70	•		0 9 0				5	0 0	
			1				; ·		•	,		! : !	, ,
		7.75	5.57	7.67							5 -		710
	•	. `	2.01	50.5	(⊃	0		V	0			10	50
	•	7	75.	3.24		•	•	~	C			10	5
	٥.	۲.	-3.64	\$40		0	1.0	ž	c			01	0.1
-1004 200-	•	2	-4.52	99.6		50°	્ય						_
	10	7.24	•	7.31	20.	.03	62.	910	90		0	8	0.11
	ċ	~	77.76	£6.0		C	1	-	•				-
		•	•			•	•	•					-

STRAN LERBER DETAIL REPORT

T.

THE PERSON OF THE PROPERTY CONTRACTOR SECTION OF THE PROPERTY SERVING THE PROPERTY OF THE PROP

	5								į		,	•	
MEASER GRUUP	1 1 1 1 2 2 1 1 2 1 1 1 1 1 1 1 1 1 1 1	FURCE	MUMENT	-	HEAK F	12	018XD	AXIAL	BENDING &	40	STRESS	BHEAR	CUMB. UNITY
210		87	94 X X X X	INSTING	K I PS	KIPS	BATYENT		800000000000000000000000000000000000000	•			
002-1003 200- 1	0.0	14	23	17	100		•	000	•		00.		000.
	9	~:	10.44	o; :	3 :		٠ •	? :	÷.		000		00
	0 7		C 0 2 2 1	3 3	•	2 0	2 1	.	•		9		36
	56.0	3	5.07	5,20		01	95		0.00		00	00	. 200
2-1004 140- 1	0	02	-	04.	9				Ö			c	0
	2	70	3.46	45	2		10	9	0.0	į			3
	10.0	70.	-	80.	0		10	3	0	i i			. 0
	0°0	7	1.70	9 0	•	7 0	 					70°	.001
		•	3	- 251				>	000				•
2-1005 140- 1	0.0	•0•	-3.29	1.14	•		ď	9	0		00	90	0
	TO .	90	-24.15	e, 16	2		~	3			00	00	3
	16.0	0 ·	15.	61.	00.	10.		00.	20.		00.	20.	.001
	3 '	•	02.	12.	•		~	3	٥.		00•	00	0
	36.0	٠,٥٥	1.36	-, 23	2		7	00	٥.		000	00•	001
-1005 200- 1	0.0	1	-13.14	18.9-	3	\$0.		.21	90		00		-
	r.	٦,	09.8	200	2	\$0.5		25			00		~
		•	0 :	62.5	• :	, i			9 (0		 .
		7.87			000	n :	27	17	- C			•) ·
	•	•			į			!			•		•
-1002 140- 1	0:	10.	20.1	.10	000			00:	\$0°		10.	.01	200
		:: >		>, -				9 0	> c		> c		
	3	0	0.1	. N	, ,	9	3	3	•				, c
	· ~	œ.	-117	36	3	0	3)	0.1		010		
-1006 200- 1	0	.1.11	54.5-	7	07	70		•	•		00		100
	0.0	-1.11	£	7	•	~0.	Ð	့ ၁	•		00		3
	10.0	-1.1.	4.07	1.78	00.	₹0.		50.	20°-		00	0	.003
	0 . 7	•	4,52	-	9	70		?	•		00.		• 003
		' 	0.57	7	3	20.		2	•		00		#00 T
05-1006 200- 1	000	eh. 30	.,15	90.			3F)		00		90	00	•
	0.0	~	3.07	1,10	3		75.	~	٠.		00	0	5
	15.0		6,20	2.24	10.0	\$0.	75.	.17	0.0		2	00.	0
	0.37	٠.	3	3,48	2		, 34	٦,	٠.		00•	00.	5
	36.0	96.90	12.00	70.2	- O - O		77	=	C		C	Ç	



TACAUX TEVELS SARRES SAR

19 10/05/76 PAGE U.S. NAVY - ACHK PLATFORMS - FATTGIE ANALYSIS - MLM 105.0 FEET LUAD CONDITION NO.

1	MEMPER	1		×	ACIAENT AY	UMENT M2	T T	UNCE	01890	X I AL	BENDING	STRE	STEAR	BHEAR	COAR.
	!	SECTA		A 1 F G	27 X = 2 7	カラ エメースコ		2 I V	¥						S
	10	- 204 5	0.0	00.	000	٠.	•	•)	•	C	0	0	0	
			3,6	00	00	9	2	0	0	3	0	•	0	0	0
			-	00.	00.	9	٦,	•	0	.	0	0	0	0	00
2			• •	00.	20.	0	.	•	0	3	٥.	0	0	0	8
			3	٥.	00	0	-	9	3	?	0		90	•	
2	07	2016	0.0	C	9	C	3	00	٥,	9		0	0	Č	00
10 10 10 10 10 10 10 10			3.6			9)	0	•	00	0	0	0	ō	
2.			7.3		20.	Ċ	>	90	2	00	0	•	0	ō	3
			Э		3	°.	2	00.	0	9	0	2	0	Ö	00
10. 10. 10. 10. 10. 10. 10. 10. 10. 10.			3	20.	\$0.6	_	>	00	•	00		•	0	ō	S
10 10 10 10 10 10 10 10	Se 10	4 1 0		90	2	-		0	3	•	9	<		•	-
1	,	1	•	0		0)			9				C	. 0
10.0			7.5	0		; o	0	0		. ၁				. 0	. 0
11. 3			0	0	7	0	Э	•	•	Э	0	9		Ċ	-
11.3	!		3	0	.	••	→	0	?	>	C	2		٥	00
11.3		ر د	•	C	60.	0	2	•	3	3	C		0	0	00
1, 2, 00				C	17	0	2	9	3	9	0		0	C)
11.3				0	. A.	0		•	3		0		0	0	3
20			_:	0	•	0	3	0	4		0		0	Э	Э
10.	1			C	v.	0	.	9	3		0		0	0	•
10.4	1- 20	2 418-		•	0	-	•	•	0	?	0	•	0	00.	0
10.9			5.0	50.	\$0.		3	0	Э	3	0	0	0	00	9
10.0			7,3	\$0°	50.	0	٦.	•	ō	•	0	•	C	00.	Э
1			9	50.	50.	0	7	•	ō	•	0	9	0	00.	0
1	:		.	50.		0	•	0	9	2	3	Э.	0	00	0
10.9 0.0 0	1- 20	410-	•	0		-4	2	0	9	9	0	?	0		0
10.9				70.	8 > •	-	•	0	2		0	3	0		0
10.902 .01 .00 .00 .00 .00 .00 .00 .00 .00 .00			7.2	20.	30.	0	, 3		0	٦.	0	2	0		0
1- 301 Url- 1 0.00104 .01 -1.540000 .00 .00 .00 .00 .00 .00 .00 .			10,9	~ 0.5	-	c	٦.	°	9	•	0	0	0		0
1= 301 UAL= 1 0.00104 .01 -1.540000 .00 .00 .00 .00 .00 .00 .00 .	!		•	~	.01	C:	3	o ·	•	਼	9	0	0		3
3.6	1- 30	1 UML		·	70.	•	ာ	c	3	•	0		0		0
11.3 -01 .00 .00 .01 .154 -00 .00 .00 .00 .00 .00 .00 .00 .00 .00				10.		~	٠	0	1.5	3	0		0		0
11.301 .99 .00 .01 .1540001 .00 .01 .00 .00 .00 .00 .00 .00 .00			•	٥.	. t.		3	0	1.5	•	•		0)
15.001 1.5409 .00 .00 .00 .00 .00 .00 .00 .00 .00			•	c.	>	٠,	3	0	1.5	٦,	۰.		c		0
1= 303 120= 1 0.0 .01 .090000000000	!		•		Ç.		Э.	0	1.5	•	•		9		0
8.2 .01 .03 .00 .00 .00 .00 .00 .00 .00 .00 .00	•	120-			•	3	.	0	Э	9	0		0	0	0
0. 00. 00. 00. 00. 00. 00. 00. 00. 00.					£0.	~	•	0	0	3	ے		0	0	9
0. 00, 00, 00, 00, 20, 00, 00, 21, 20, 20, 20, 20, 20, 20, 20, 20, 20, 20			ċ	20.	2	\sim	?	0)	Э	0		0	0	0
				10.	2	-	•	0	3		0		C	00•	٠ د



TRAN REFERENCE OF TAIL REPORT

22 10/05/76 PAGE

00000 00000 00000 00000 00000 00000 00000 0000 0000 0000 0000 000000 STEAK STEAK STEAK 20000 20000 20000 20000 55555 2222 8888 00000 00000 20000 00000 HENDING 00000 20,200 00000 00000 00000 80000 00000 2222 U.S. NAVY . ACIR PLATFORMS . FATIGUE ANALYSIS . MLW 105.0 FER 99999 33333 20000 ~~~~~ 2 2 2 2 2 14444 14444 00000 22222 00000 22222 22222 3222 22222 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 3 2 2 2 32333 -3.57 -7.59 -11.61 -15.55 1000/ 117.54 13.84 5.34 4 07 -3 65 -7 51 -11 56 15.03 14.03 18.01 18.01 5 64 11 15 16 10 17 11.67 7.51 7.55 5.58 24.14 24.14 24.19 24.19 20000 2000 2000 2000 2000 2222 00000 2222 00'000 0000 0000 0000 0000 24.21 24.21 24.21 24.21 24.21 FURCE FX AIPS 0 - N - 0 0 - 7 - 9 0 - N 3 0 0 - M B B 0-744 0-43 FRCM FRCM FAC CUNDITION NO. SECTN = = : -,15 165-714-114 400 201 210 503 511 500 515 205 NUMBER 401



THE STREET STREET STREET

23 10/05/76

00000 00000 00000 10000 4 W W 4 W # N N N M WWW. 20000 22222 00000 20000 30000 00000 30000 00000 00000 90000 4444 7 7 7 7 7 00000 20000 00000 00000 00000 ----MMMMM 00000 33330 33333 22222 22222 99999 70000 11111 22202 44444 00000 3 4 4 4 4 MANAM 00000 00000 2222 16.53 17.42 34.40 51,37 22. 22. 24. 24. 24. 22.00 12221 12. 44.7 74.47 0.44.05 0.05 BUNERAL RA 11111 00000 11111 11111 11111 ***** 36.1.3 ***** **** 25.17 25.17 25.17 25.17 0.0 7.11 7.21 CIG FICT



10/05/76 PAGE LUAD CUNUITIUN NU.

F. P. LEWILLIA	₩ 1014	FURCE	ROBENT		A SHEAN	LINCE CO	TOKATON	XIAL	OTNE	20.00	> 4	~	COMM
NUTTER PRO	2 4		2 × 1 × 1 × 1	84171		FZ KIPS	X	OTREGO	*	2 2 =K81	31RE 38	STRESS	CNITA
1 - 100 A 464		,	•	-		•	-		1		: ;	•	
		2.72	95.0	5.35	9 9		21.1	•					
	1001	`.	57.6	2,92	13	_	7	. >	.0		10		· c
	15.2	2.72	11.00	25.	•	-	7	•	0		0		0
	60.5		-13,15	-1.87	70.	0	-	Э:	0		101		8
505 105- 1	0	-	11.	-	00.	9		9	9		90	00	9
,	8.8		01.	10	3	00	10	3				0	000
	7	٦.	20.	-	03.		Э	. ?	•	i :	00		0
	11.4	٦.	\$0°	.31	00.	•		3			•0•	0	0
	Š	11.	.00	3	00.	000		~	0		00	00	0
500 105- 1	0.0	2	13	4.33	90.	• 01	7	9	70		10.		0
	5. X	7		•	Э,	0	-	Э	0		50		CO
	4.	1.25	.0.	•1 • 1 •	92.	10.		***	10.		.0	• 01	₹00
	7	1.23	D	•	9	0	~	90.	90		.01		0
	'n	1.23	20.1		900	? ,	-	30.	90		101		0
506 165- 1	0.0	07.	. 4	1.61	40.	0	87.	•	•		00	00.	0
	¥.	07.	\$7.		70.	•	4	5	್ಕ		8	00	00
	•	£ 1	50.1.	؞.	Э:	•	90 G	ء •	਼		3	0	8
		9 4	77.1.	0 ° 0 ° 0 ° 0 ° 0 ° 0 ° 0 ° 0 ° 0 ° 0 °	7 5		10 st	V 6	1		9	000	N 6
		•		i.		• '		•	2,			200	•
606 JLS- 1	0.0	-67.04	.7.65	0	. 14	••39	•	٦.			10.		\$00°
	•	-27.04	-14.53	5.	0.14	3	•	-	•		10		9
	0	-67.04	-21.51	90.01-	7.	98.	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	61.	0		10.	.01	000
	•	40.72	79.62		# :	•	•	~	•		10.		
	•	70.72		-	*1.		•	-	•		101		010
664 200- 1	0.0		79	-18.42	77.	0	٠,	Э	7				700
	5.1	-1.78	35	69.47		100	-1.38		00.		10	10	002
	10.1	۲.	77.	-1.54	•	0	٠.	0	, 0				00
	15,2		Ď	96.95	7	•	٠.	-	٥.				00
	20.5	- 7	81.18	14.65	귛	00.	٠.	Э	•	,	10		0
710 21- 1	0.0	. 76	3.53	14,15	Ţ	~	•	2	•		10.		000
	0,3	~	-4.75	57,33	57		40.07		.03		10	01	100
	12.7	۲.	-64.84	100.52	'n	٦.	3	٦.	•		100		Э
	14.0	•.76	04.55.	143.70	Š	-	•	•	•		10		0
	_ 65,3	۲.	86.87	186,58	3	• 17	3	3			10.		Э
711 71- 1	0.0	•	#5.11	7.04	<i>_</i>	.52	-	-	9				2
•		20.0	W. 7	-35.34	•	55.	2.5	-	•				0
	v	-48,22	•	-17.71	45.	54.	-5.19	• 1.3	50.		5	10.	900
	•	n	٠,	90.061	1	73		•	•				•
	•				•	3/-	:	:	•			•	0

计计口电记录 计工业计划 医医电压阻压 人名英丁奇

No. 20 Company

8
-15.02
3 7
1111
49.74
- M
92.60
. 6
~
2
-57.72
_
0
-20°17
-
7.00
5.19
128.53
-12.AB
0 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7
S
21.66
æ.
10.07
<u>.</u>
-93.61
£ .
22.41
٠,

							1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		-			
- 1	1810			İ				1		>	~	, 24
SECTA SECTA	т ч 5 с г 5 с г	7 7 7 7 8 9 8	2	N	X 4 4 1 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	/ 0 X C X X X X X X X X X X X X X X X X X	20 X 30 X 30 X 30 X 30 X 30 X 30 X 30 X	AXIAL STREES		81 KE 88	BIRESO	
25- 706 200- 1	0-0	7.6			70		-		0.3			
	5.5		14.41	. 5	0.1	2	: ~:	>	60		0	0
	11.0	۲,	24°9-		•	→ :	7	9	0	40.	10.	00
	7 7	2.75	74.5¢	000		\$\$. \$\$.	1.12	2 2		200	200	5000
20- 656 Jlo- 1	0.0	-47.08	7		90	~	9	-	c		6	-
	1.5	-27.03	-72.78	~	· 3	- 15	?	: =	9		0	• -
	0.5	-46.47	14.14		~ '	0	•	∹	•		00.	5
i	• •	140.42	10.50	-14.51		9 P P	3 3	> o			90	200
1 901 3100 1	5	-	47 886	1	· -	•	` .	•			! !	•
	200	1.56	147.40	102.17	1.52		8 30 000	20	> • • • • • • • • • • • • • • • • • • •	4	9 0	3 2 0 0
	5.5	·s.	01.000	71.7	•		50.2	, ,	Ö		100	•
	5.5	•	90.87	36,56		10.	30.2	9	0		70	0
		\$	649.50	0	2	9	38.2	3			104	0
653- 703 JLG- 1	0.0	46.47	٥	÷.	v	٦,	5.7		0		50.	-
	1.8	44.47	~	9	0:	S	5.7	-	0		0	5
	5.5	87.07	60.55	76.4	~ :	•	2.5	-	0		€0.	
	۷.۲	70°40 40°40	23.72	145.67	0 0	10.04	25.78	~ .	5	V 5	N 10	010
	ļ	!			!	:	•					•
6- 706 JL6- 1	0 -	55.43. 10.43.	10.04	3 1	55.0	5 : S	65°M	•	0	10.	10.	110.
		26.85	20.00	28.5		3 4	20	•	2			
	5.3	06.97	-32.55			9 6	•	: -	• •	20	• 6	• -
	7.1	-25.90	-12.77	0.7	-,73	C			50.	8	- 05	010
1- 702 157- 1	0	€.	1.50	-3.07	9	•	96.	~	•		10.	
	4.7	20 1	545	4.26	3	0	96	~	٩.		10.	~
	• :	e.	3 -	08.5	• ·	٠	9.	→ .	٠,		0	0
	200	8.0	2.40	9,02	77.	200	\$ 5	515		200	20	910
01- 704 157- 1	0.0	.30	15.27	46.54	10.	7	.74	20.	N	0	20	-
	4.7	46.	6.U2	-4,31	- u2	. 16	7.	20	21.5	0.5	0	900
	3.	. 3.5	.	.2.2.	50.0	7	, 74	20.	0	20	20.	0
		55.	Ð.	7	•	•	. 74	20.	_	.02	70°	0
	20.	. 32	94.15	4.67	2	힣	~	205	-	10	10	0
01- 801 JL7- 1	0.0	2.3	•	16.94	-	.11		3	•	90	40.	0
	-	Z .	45.0°	20°E9	37.	500	0	.03		0.5	20	9000
	700	66,55		72.67	~ `	900	-6.91	.	7	.01	0	0
					•	•	3	=	•	•	•	¢

CARAN TRACER ORTALL REPORT

T

CONTRACTOR CONTRACTOR (CONTRACTOR CONTRACTOR

energes, esperies excuses

A CONTRACTOR OF THE CONTRACTOR	PAUG PAUG PAUG PA PA PA PA PA PA PA PA PA PA PA PA PA	A MARKA	HOHENT NZ NZ	A PER PER PER PER PER PER PER PER PER PER	FUNCE	TORBION	AXIAL B	ENDING	81RE 88	SHEAR	STEAR	0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
. •	2 T		25.	4			12	2			20	נייב 10.
7	3 3	-5.40	-10.65	10.01	100	-0-4		10.		300	0 5	9 q
33			7.43	£ 4		20 4	2.5	8		5	0.0	
, 	,	75	36164	250	71	0	→	V		70.	0	•
3	.0 -3.0	70.1	5.57	12		0.1		•			200	00
	3.0		2.7	>	0	? ?	: -:	•	:	õ	o	9
7 9	4.1 -3.03 b.8 -3.03	1.44	2,90	70.4	.01	1.06	116	900		100	20.	001
0	•	2,5	23	٠,	•	-	Э	0		a	0	3
7	·°.		72.	3	O		0.1	3		10		• 3
J :	0,	•	121	.	0	-	Э:	0		0	0	0
2 5	70. 1.0		> > · · ·		0.0	7 7	9 0	50.		- 0	- C	0 3
	1			• 3				, ,			: 0	•
, 3	7				•	•	, ,	20			•	
	2		1.1.	, 3	0			9		0	30	•
 2 E	~ .		75°	3 E 3 3		9 9	200	, o				000
	•			: :		1						
, 3	u ~		7 0	3 3		0 10		20.			o c	3 0
پ ر	0.5	26	97)		3	•	۰, o			10	•
寸 :	~ (-1.99	70.	€0.	50.	010	70		5	0.	00
		\$ 0.5°	44.46	70		D.	-	0			10	•
J 10	2 3	7-	26.92	46.0		~		~ 0		20.	20	5
Ş	3		- 20	3		`~	• ~	>. ⊶			000	, ,
. S .	50.5 a.55	-3.74	10.04	12	200	2 8 9	12	900		100	50	000
>	,0 63.4	• 0 ?	_	~	•	6.1	~	0		80.	0.3	•
-	1. 43.4	7.	æ	J.	61	1.0	•	~		10	0	3
J .	2 63.4	. 18 1.	7:	٦:			~ •			- C	100	0
3.5	23.42		27.08	7 0	1005	21.0	33	200		30	000	010
5 :	0		90.	01.		12.	•	••13		20.	20	3
, 3 	7		,,	> :		100	2	2		30	0	9 0
7		,	30.		•	12.				0 0	000	•
				•	•		•	,		•	•	•



28

PAGE

STRAN TRIBER OFTAIL REPORT

- MLM 105.0 FEE - FATICUE ANALYBIB LUAD CUNUITIUN

-
2
0
•
10.
3
۷
-
4
_
4
_
_
_
3
L.
30
Σ
Ŀ
I
z
4
×
_
•

	9		>> <	- ACMM PLA	TFORMS FAIL	IGUE ANALY	1 J T T T T T T T T T T T T T T T T T T	105.0 FE	ــــ لعا		2	•	
EX GRUUP	1	FUSCE FX	HOMENT	MUMENT /	BESTEAK FUR	ACE/	TUKBION	AXIAL T	BENDING 8	SIPESS	SHEAR	BEEAK	COMB
9	1.		Balvevi		KIPS	KIPS	IN-KIPS			KSI			CHE
804 146- 1	3.	~.	1.94	80	• ·	•	50.		513		0	10	10
:	•	-	784	10	2 3	20	0 0	-	a 0		00	100	9 5
	1.7.1	2.14	em.	-	300	0.0		07.	20		50	50	500.
	v	∹	-10	7	•	9	•	~	-: 90		0	. 10.	0
901 JLB- 1	•	2	0.10	4.9	~	0	1.1	0	0		0		00
	Ŧ.	~	5.40	3.7	-1.54	0	1.1	\$0.			0		0
	• =	~ ~	3 1	,	> :	•	Ξ.	Э :	0		0		00
	36.4	3,29	-3.05	20,88	2	0.00	11.13	5.5	900		20	90	3 0 0 0
903 200- 1	•	•	-3.27	3.6	.27	0	0	-	7		C	6	-
	16.	5.5		12.0	-		3	-			0		• •
	•	2	1.10	-21.22	20.0	10.	1.07	51.	21.		0	00	015
	44.7	٠	~	3.6	~	0	3	-	•		10.	10.	5
	•	5.6	٥	2.4	7		3	~	-4,		10.	. 10	5
803 148- 1	•	3	-, 35	_	20°		7	٥.	0		0	10.	0
	•	7	135	_	20.4	0	7	3	٦,			10	00
	<u>.</u> ,	•	1.00	•	20.		~	•	?		0	10.	0
		7.5	1.00	25.1.	~ :		. 75	N 1	10°		100	50	₹00•
	j	•	6.36	•	100			2)			10	0
604 106- 1	1 0.0	0	· s	~			~	.	0		10.		0
	5.7	•	~ .	3	Э,	9	'n	~	0		10		ိ
	7	•	~	7	つ :	•	٧.	3	•		100		00
	45.5	40		. 15	9 9		9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9		~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~			000	000
			4		:		, -		. '				
	•		37.	35.					• •				100
	<u>.</u>		77.	~	3	. °	-		10.			0	0
	•		3	•	.	•	-	9 :	10.			0	0
	•	-	•	7 1	> }	>			100			200	•
805 146- 1	•	•	4.35	3	•	0	-	•	•			00.	0
	٠.	•	5.30	~ 1	000	ç	15	3 :	9			- 000	0
		. 4	63.4	•	> =	2 9	- -	•	•			9	0 :
	45.4		77.	. 0.		000		9 9				9 9	0000
		7	٦		1 7	נו		. •			! . :		•
		7	25.62	90.0		000	7.5	,	9 6		200	0 0	0.00
		5.4	10			-	E i	•			10	10	55
	÷	7.	3.		• 10	~	7	~			10.		8
		77	77 076			1	•	•				•	

				T ALTA FLAIF	מינים		E-10 - 070:	103.0 755	-			
	UIST				1	i !	15		3		7	
	2 2 2	7 K		7 X X		F 2		CTRECO	8 UNION		0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	30 CA114
	<u>•</u>	k •4.	E E	L .		-						
03- 906 200- 1	•	S . 0	6.55	0.01	20.	0	~	87	90.		•	•
}	• •	•	3.97	٦,	20.	9	ď	926	50.8			┙.
	•	, d	• •	, ,	Э:	2 0	'n	0 1 V	3		•	5 6
	2.65	10.51	14.6 14.6	5.51	v ~	7 70	. 24	D SC	90			\$ 10°
				, '			ľ					
04- 605 106- 1	0 1	70.1	£7.	>N.	•	000	9 :	3	20.	00.	30	3
		10	. 1	- ~	000	000	> =	3	100		i	100
	17.1		.21	t i	• •	0		5	20		• •	0
		9	3	0.10	000	0	Э.	.00	-,02	90		9
04- 606 146- 1		~	.15	4.28	40.	10.	~		90.	10.	.01	400
	5.7	٦.		1,55	70.	•	~	-	0	10	10	9
	٠.,	~	•	-1,24	30.	0	N.	٠ •	0	10	10.	900.
	1 / 1	\$. \$ 5 . 5	10.45 10.45	15.41	3 3		87.	010	604	0.0	0	200
		•			• į	•): •:					
	Э,	<u>.</u>	٦.	2.06	0	20.			•		10.	0
		/2	200	1	> ; =	70					10	> 0
	• •	• -	``	7.7	> 2	NO .			•		5	3 6
	44.0	-	-3.62	5.7		20.	. 32	6	10	0	0	600
1 -007 106 -01	0	Z.	Ω	0	7.24	•	•	-	•	10	0	-
	1.	5. A	-5.18		•	70.	•	-		0	0	•
	•	5.7	Š	~	10.	70	•	~		00.	•	-
	, d t t t	#5.56	25.5	ָרָ פּ		9 :	80 a			10.	## C	012
	•	D P	20.63	•			•	-	C11.	10.		
00- 400 JLB- 1	.	Ð	11.5	5.4.	~	00.	-20.91	٧.	•	.03	•	~
		10.10	27.73		21.		•	570	50.	20		5 6
	, ,	. 40			•	57			•		•	5 5
***	52.4	-16.25		1.87		20	2	7		10	103	
10- 910 -2- 1	•	.73	61.10	120,19	56.	.01		0	• 05	00	0	0
		۲.	22.40	15.88	55.	10.	4,10	00		00	00	200
	•	• 76	43.04	26.40	55.		٦.	0	£0.	00.	•	0
	, 44 s	. 10	90.45	45,34	~	.0.	∹	3	ç	00.	•	3
	2	70	- 50.12	₽o.	~	10.	~.	9	-,01	00.	6	•
11-911 P2-1	Ö	28.5	111.94	-35.10	••43	•	~			.01	.01	0
	10	-24,21	60.05	-12.77	•,43		•5.13	. 11	-,03	101	.01	,000
	· .	7	60.10	10.0	•	•	∹	•	•	10,	10,	0
			•	00 67			•	•	•) (•

CARA SESSES OF A SECTION

NUMBER OF	i i	UIST		Ŧ	1	į	!	1			-	7	
915		7 7 2 7 2 3 2 3		TOTE T	/ ↓ √ × × × × × × × × × × × × × × × × × ×	TANEOS	FURCE/	NOINTOL NAINTOL	BXIAL	BENDING BIRESS	GIEAR	BIREAR	C Z Z Z Z
- 912	SECTA	-	AIPS	I Nex I Pu	INEKIPS	27 X	NIPS	SATYONT	:				
	1 -74	0	0	-124.05	0.1			Đ.	-	0		0	_
:	:		• 4	7 ·	2.4	9 3	9 9	10.01		50.		01	1007
		; ;	•	,	56.0							20	9 0
		4.	A.	40.24	>1.4	3	3	0	-4	0	0	0	00
1 - 902 16	1 -69		9	~	~	•	10.	•		Ö	0	0	0
		•	3	D	^4	э •	0	S	•	Š			0
		•	0 0	-1,32	2.5	3 :	0	S	•		0	0	9
		67.4	9 9	\$2.	5.04	20.	10	57	2 2	0.3	60	000	200
- - -			7	•	:	:	•						
***	•) ;	V	7	7	# # # # # # # # # # # # # # # # # # #		70,1	2 .	3 4	0	.	
		-	. E		*	3	0	Š			10		90
		9.07	*		~	. ~	0		-	0	0		00
		~	£	\mathbf{v}	~	2	•	v		0	10		0
1-1001 JL	7		C	.	^	٩	0	ď	=	•	ď	6	5
•			0		7	, J			•	•		0.0	9 0
		16,2	50.	•	51.34	50.	.01	6,51	03.	70.	3		200
		• ·	0	3	3.0	V	॰	.5	•	٥.	10.	0.1	C
		•	•	11.31	7	∃ ∤	0.10	Ţ	9	C.	20.	* 05 ·	9
1-1002 1	80-1	•	7.	٦.	9.7	.		~:	~	0			-
		•	7.	_	-2. HV	•	O	7	7	٩		0	~
			3:	•	-	.	0	٠.	٦.	٠,			0 :
		\ • • • • • • • • • • • • • • • • • • •	3 3		- C			1	0 4		0	.	3 6
				•	•	•		•		_			•
1-1004-1	80.	•	ć.	10 C	 ∩	•		3 3	 -	0			60
		• •	٠.	· -	. ~	כיב	· 0	•		. 0			. c
		31.7	20.2	1.77	4 2 4 4 6 9 9		0.01	26		2000	88	000	900
2- 905 10				54.	2,30	3	0	4		0			9
		÷		ţ	.75	3	0	4	∍	0	00		0
		\$		۵,	80 '	Э.	9	4		0	00.		0
		67.4	7 7	0 × × × × × ×	3,91	א ע ס ס	000	. 4. . 4. . 4. . 4.	3 3	40°	000	200	000
2- 904 10	1 -60	•	٥	, 4 S	3	2	•	~	•	0.			ô
		٠.	0	Y	120	00	0	7	.	9			0
		1307	000		•	9	30.	92.	0 0	00	9	0	000
		•	•		00.	> :	•	, .	•	•			0



TENNE SUNGE

TRAN MEMBER DETAIL REPORT

	Activity 5	C187	9.00.0	T T E E E	7.2 4.1	A SHEAL	/	200		0	7 915	2 7 3 10	7800
	i	2 Z	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	901×171	94148VI	2 × 3	7.7 KIP	S T X T X T X T X T X T X T X T X T X T	1 30 B		3 60 6		CHECK
10	**	0.0	0	.52	.23	00.	਼	.12	•	0	00	00.	3
10		a	0	070	.24	000	9	₩.	2	0	000	000	3
10		7.5.	0 0	£7.	4 V	9	٠ •	→ •	9	•	0	00	C
10		67.6	0		45.		•)	10.			0 0
	164	0 0	·	. 5	2.61	00.		70.	_		0	00	3
10		6.0	-3,55	3.65	4.20	• >	0	70	. ~		00	0	: 0
10		15.7	-3.55	2.37	1.92	1	0	.07	-		30	00	5
10		20°6	* 3,55 * 3,55	1.1.1	1.57	> =	0	70.	7	9	000	000	56
10. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0	-	! •		!				!	:	> :		2	,
1,	180-	3	07.7	ς γ •	1.51	Э	0	09.	-	.01	.00	00.	00
11.0		9 = 1	4.40	10.	11.1	000	000	980	-	100	- 00	00	0
1		</td <td>D 7 . 3</td> <td>\$ ·</td> <td>7.</td> <td>•</td> <td>0</td> <td>00</td> <td>-</td> <td>.01</td> <td>00.</td> <td>00.</td> <td>S</td>	D 7 . 3	\$ ·	7.	•	0	00	-	.01	00.	00.	S
10		51.7	9 :	1.56	15.	9	0	00.	-	.00	00	00.	00
10. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0		7.27	4.40	1.01	00	00.	0	000	9	101	00.	000	=
10	31.9	0.0	•	-36.03	35,02	.26	27.			90	20.	20.	0
2 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		8.1	0	-6.00	13.48	97.	.21			50	10	0.	0
Sign		10.2	.	p - 6	25.	. •				100	10.	.01	0
1			> 3	80°3	-2.74	•	•			70.	5	10.	0
10			Ç.		●,	•:	•;		5	,06	10.	100	100
10.0	S 180-	0.0	-	09.2	2.98	.01	•	-, 92	M	.03	00	00	5
10.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0		10.0	-	47.7	1.90	200	-	26.	950	0.4	8	00.	5
104 1 0.0		41.	∹	1.71	***	30°	•	26.	~	70.	00•	00.	5
10.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0		7.15	7	1.17	\$ 0 ·		•	26.	9.00	10.	0	00.	5
5 104 1 0.00605050900 .00 .1300 .00 .00 .00 .00 .1300 .00 .00 .00 .00 .00 .00 .00 .00 .0			-	۰ ۵	01.0	50	•	26.	1 20	100	00	00	010
15.7 = .06 = .040 = .09 = .00	-601 5	0.0	• 0	55	•.29	000	0	-	_	•	00	00	00
15.7 = 00 = 01		6.0	• 00	07.	60.	00.		-	3		00	00	6
20.0 00		15.7	90.	7	11.	000		-	3	•	00.	00.	00
1 0.0 2.84 .43 4.21 .03 .04 .12 .05 .01 .00		0.0 ₹	•0•	77.	.32	00.		-	•		0.	00.	0
13.7 2.84 1.72 1.03 1.01 1.00 1.00 1.00 1.00 1.00 1.00		- 47.4	96.	20.	154	000		-	-	20.	00	- 00	0
13.7 2.84 -1.21 1.75 0.03 -1.49 1.2 0.02 0.01	6 169.	0 6	2.84	£4.	4,21	٤٥°	0	3	~	50	. 0.1	101	0
13.7 2.84 =1.21 = .71 .03 = .49 .12 .02 .01 .01 .00 .01 .00 .01 .00 .01 .00 .01 .00 .01 .00 .01 .00 .00		6	2.84	45.0	1,75	50.	0	3	-	0	10	0.1	3
20.6 2.54 =2.03 =3.17 .03 =.01 =.49 .12 .04 .01 .01 .00 .01 .00 .01 .00 .01 .00 .01 .00 .01 .00 .00		15.7	2.84	-1.61	71	50.	•	7	~	0	10	0.0	9
-1 0.0 =3.46 .10 1.99 .02 =.02 .03 =.14 =.02 .00 .01 .01 .01 .01 .01 .01 .01 .01 .01		40°	2.54	.c.03	-3.17	.03	0	3	-	0	10.	10.	9
- 1 0.0 -3.48 .10 1.99 .4202 .031402 .00 .00 .00 .01 .01 .01 .02 .00 .00 .00 .01 .01 .02 .03 .04 .01 .02 .01 .01 .01 .01 .01 .01 .01 .01 .01 .01		77	2.84	-2.85	-5,63	E0.	0	4:	~	CI	10.	10.	8
-3.45 - 10.	•		-3.48	.10	1.99	•		9	~	•	00	9	0
-3.45 -40.40 -10.53 -40.5 -40.5 -40.5 -40.5 -40.5 -40.5 -40.40 -40.40 -40.5 -4		•	- 5.4B	\$1.15	, 38		•	9	-		00	00	3
13. 00. 00. 20. 41. 20. 50. 50. 50. 54.55 40.55		15.7	-3.40	04.5	-1.23		•	Э	-	•	00	8	-
		0.07	- 3 · c B	10.5.	54.5	•	•	7 0 '	-		÷ <		•

00000 0000 9000 00000 0000 SHEAK STRESS 60000 00000 33033 00000 N 10 2 2 22222 60000 22222 00000 00000 00000 70000 55555 00000 55555 STRESS HENDING Y 20000 0 C O O O 20000 W W W W W W 00000 00000 V W W W 444 MLW 105.0 PEE AXIAL STRESS 33233 00000 20222 20000 - ACMM PLATPUMMS - PATIGUE ANALYBIG 9 4 6 4 6 22000 99999 N 2 2 2 2 2 22222 3 3 3 3 3 20000 20222 2222 107.85 67.31 26.77 13.77 178.33 152.17 866.01 539.86 2.22 1.57 1.57 2.22 2.37 36.73 38.42 45.42 51.47 MUMENT MA N V V 1.22 2 . c 1 2 . c 1 2 . c 2 2 . c 2 2 . c 2 2 . c 2 12.00 111 03 54 06 71 103 105.05 105.05 105.05 105.05 105.05 105.05 2 7 0 0 0 W 7.03 2.07 1.55 1.03 HOMENT 2000 2000 2000 5.33 *5.33 *5.33 *5.33 1000 0 - N M 3 (Tr SKCUT AND WEGTN 21.9 100--002 200-916 911 9001-006 4001-406 920 1001-1001

(

THE STREET STREET STREET

ţŸ

(3)

į	UIST										>		
TERRET GROOF) 2 4	FURCE	MOMENT	MUMENT	/BAREAR		TURBION	XXAL	BENUING	8	SHEAR	•	CUMB
•	2 4	91 X	84188	841481 841481	N 2 1 4	74	4	STATE SO	Y	Z 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	STAFES	3344	1120
	:	ı		•	•	•				3			
- 102 A16- 1	0	10.	40.	• •	70.	00**	00.	•	00.	0	õ	00.	.003
	0.0	0	50	4.5		°	3	3	0			0	0
		9	•	61.		0	0	00.			0 ·	00.	0
	• · ·		•	30.		•	•	•	0	0		00.	0
-	•	•	50	72.		0	9	7	0	3		0	0
- 104 416- 1	•		3	**	=	•	•	=	•	•			1
	3.0	0		200	5	2 0	> <	2 3	> <	> :	5 6		
		-00	>	91)	•	2	2 3	>	3 C		> C	. c
	•	.01	9	200	>		. 0	3	¢	•	• 0		0
	•	1000	. U1	*, 32	20	00	00	00	9	0	0		3 6
								 		•			
- 401 DKL- 1	o :	30°	\$! •		10.	70°		•	•		0		0
	~ •	~ •	•	92		20.	4	9	0		00		0
	٠.	3 (3	¢ (₹.	•		0		Э
	•	-	•			0	٣.	3	٩.		0		9
	•	_	•	1.76	Э,	0	~	2	0		00.	00.	00
- 103 #18- 1		0	2	10.0	5	5		•	•	•		;	
•	9.6				•	2 0	> :	•	•	> :	9.0	0	ŝ
		0			07	2 0	> 0	•	2 (3 9	> <	~ (3
		0	-	25.			•	•	•	>	> <	,	2 6
	•	•	•.16	45.	00.	00.			200	M	•		000
•										•	•	•	•
1 100 100 1	0	30.	00.	10.	000	9 •	2	00.	0	0	00	00.	0
	•	3	00.	20 a	•	0	2	Э	0	•	C		9
	• :	•		•	9	00.	00.	000	00.	09.	00	00.	000
		•	70.	10	•	0	•	9	0	•	00.		8
	•	000	10.	\$0.	•	00	2	Э.	0	0	000		0
- 105 HUG- 1	•	0	00	00	3	0	_	- =	•	•	Ġ	•	
i	3.0	10.	3							2	•	•	3 6
	۲.		20.	\$0.	07	?	0	. 3		• 0		00	· c
	•	•	00.	70.	3	0	00	3	ຸ ີ	0	0	00	0
	3	0	000	500	> ⊦	oj.	00.	00	0	10.	00	00	001
- 105 m16- 1		0.0	. 21	23	9	C	=	=	•	•	ć	•	•
	5.0		-	-17	3	. 0	2	9	•	•	•	3	3 3
		0	20.	-112		30	00	3			000	, c	, ,
	•	10.	\$D.	00.	٦.	0	3	000		0	00	00	6
	4		\$0.	•	3	0	9	Э	00	0	00	00	000
- 205 UML- 1		00	-		- 3	•	4	•	•				
	20	0	3	20.	99				•			000	000
		00	·					> =					
	11,5	20.	٠.		•	9							
						•							



36 10/05/76 PAGE

THE CALCULATION OF THE CALCULATI	0 1 4 0 1 5 1 5 1 5	30 M G	ALIAN I	YOMEN! /	BESONE AN		TOROTON	AXIAL	BENCING	STRESS	A HUE	SHEAK	003 8 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1
1	14	AIPS	SAINENI	INEKIPS	K 1 PS	KIPS	Nex 1 P&			K 8 1			CHECK
104- 105 num- 1	0	0.	.01	20.	ာ	00.	•	9	0	0	0	00	0
	3.0	0	3	30	3	00	00	9	00	8	00	00	000
	۲.	10.	00.	0) >	0		Э	٠.	•	0	0.	0
	7 0 °) •	70.	000	30°	÷.	00.	9	0		0	0
	Z	10.	00.	C !	つ	0	-	3	0	•	č	700	00
104- 100 218- 1	0.0	70-	00.	~	٠,	0	0	2	¢	0		0	0
	3.6	e.	٦,	90°	•	•	00.	2	0	Э	00	000	C
	٠,	÷	50.	۳.	•	•	0	?	0	0	0	C	0
	0 0	70.	£ .	5. E. E. E. E. E. E. E. E. E. E. E. E. E.		00	60.	000	00	.03	00.	00	₹00°
	•	•		•	<u>-</u>	•	0	•	•	Č	06	00 -	C
105- 106 m10- 1	0.0	90.	£0.	_	•	00.		•	C	0		90.	C
	3.6	00.	20.	0	3	Э,	Э	٦.	C	0		00	О
		00.	61.	.16	00.	00.	00	000	20.	.02	00.	000	.001
	•) •	22°	₽ .	•	0		÷.	0	0		00.	0
	14.5	00.	87.	⇒ :	⊃ !	0		3	0	Э		• 00	3
100- 200 DKL- 1	0	.01	~	.33	9	10.	9,1	7	0			00	C
	5.8	01	14.	•	Э.	0	0	2	٠.			00	O
	5.	10.	Ď.	•		0	1.6	·	0			00.	0
	15.0		1.61	200	9 5	0 0	0.7				0 0	3 6	000
			•	j	• •		•	•	-	i i		1	2
201- 202 #18- 1	0.0	9.50	70.	.70	. 01	00	•		0	.07	00.	00	=
	9.	200	3	J ()	93	3		Ç	70		c	_
	~ • • • • • • • • • • • • • • • • • • •	v		٠. •		9 6	ာ :		਼	3		o .	0
) J	u n		000			5 5			0 :	• ·	0 :	100
				•			•		•	?		5	c
201- 204 m18- 1	0.0	10.	24	~	9	3		00.	٥.	.07		0	0
	9.0	70.	.,22	3 '	Э,	0		000	=	9		00	0
	•	9 0		7	> :			C (5)	٠,	• ·		C	0
	. T.	0.									9 0	9 0	200
				. ,	•	. •	, '		•			•	
1 -140 100 alba	•	•	3.10	- r	•	•	•	o :	9			0	6
		0.	1.41	11.51	51.5	50	9	000	20	!			
	-		90.5.	H. 5	~		7	9	0			. 0	0
	•	0	-5.45	5.1	-	0	7		0	1		0	•
201- 503 120- 1	•	~	£6		3	0	~	3	0			0	0
		٦.	-	₹.	9		7	•	2			0	0
	5.01		. 1 5	1.12	0 2	0	15.	. 0.	. 0.2		00.	00.	.001
	, .	-	0	• :	Э.		Ä,	•	=			0.	C
	٠												



PAGE

	1810										>	•	
MERHEN GHOUP	T X C Y	FURCE	MONENT	MUMENT	/ SHEAK	FUNCE/	TURSTON	XIAL	BENDING	STRESS	¥	¥	CUTA
Q .	الا د د د د	× :	¥ .	74	> 1	74	×	R. C.	>		STHESS	314ES#	Y 1 1 1
N. 1936			BATHON	RATERI	RAT X	CATA	PATHENT			X		/	C H E C
203 -10- 1		N	. u.	•.26	9		000	. 0.	•	* 05	00.		>00€
			700	0.0	•	200		5 5			00	30	
	. ၁	N	1 0.	72.	• •			2	20		, c	9 0	o
	•		90.	.37_	3		00	0	· •	•	00		3
204 +08- 1	•	90		70 -	•	0	3	00	0	J	9	C	9
	9.5	0	10.	70	3	0	00	0	0		0	0	• >
	~	00.	2	20.	?	00.	•	9	C	•	00	0	9
	•	3 : 0 •		7 0•	•		00.	9	00.	00.	80.	00	000
	14,5	00	10.	70	3	00.	60	000	00		0	00.	C
205 #08- 1	0.0	.01		10.	99		00.	•	0	00	00	0	000
		•	10.	0	>		00	3	Ç	•	0	0	S
	7.8	• 01	10	£0	22.	000	00.	00.	00.	9	0	20.	200
	•	0		*00	Э		9.	٦.	ç,	٠.	0	9	9
	;	• 01	10.1	900	00		00	3	9	9	•	C	00
205 -18- 1	0 0	. 10	-, 64	•2•	27.	20.	00	_	-	•	C	90	0
	9.5	٦.	•	>-	~	Ö	93	•	C	2	0	30	0
	~ (9 .			•	20.	00.	a	0	.01	0	0	0
		0 50	•	1	>		9 6		•		e e	9	.001
	'		•		•					 	•		3
505 UML- 1	0		•	•	11.		~					• 01	0
		200	0 -	-	~	-10	~ ~	> :	0		0	7	0 0
				-	-	•			> <			•	3
	15.0		37,15	18.70	 .	. N	5.14	3	0.70		200	0.0	000
306 120- 1	0.0	٥	97.	2.3	•	•	~	•	c		00	00.	
		10.	•	-1.03	10.	00	., 63	00.	70		00	00	S
	c:	•	3 : •	Ų,	•	Ç	7	7	•		00,	00.	000
٠		ş (•	n 1	•	•	٧.	.	•		00	0	C
	•		٩.		•	●: ⊃ i	Ä	•	•		00	00.	c
205 -08- 1	•	.01	1	₹0.	00.	00.	3	00.	0	00•	00	90.	C
-	•	100	20.	00.	30	20.	•	Э'		٩	0	00.	9
	•	T 6 *) : •	•	0 0	3	•	Э.	٠	•	00	00.	0
) ·	3	3	N • • • • • • • • • • • • • • • • • • •	•	•		3	9		00.	2	000
	•			•			2		•	•	00	000	0
200 min. 1	0.0	10.		.,31	>	00.	000			•	0	20.	C
	3.6	.07	00	30	2	30.	Э	∍	0		0	00	00
		• 0 7		.13	•	20.	00.	000	00.	0	00.	00.	.001
	3	\ 0°	01.	• \$0		9	0			• 03	C	50	0
	^.5	``	9	95.	70.0	9	00		c	C	c	C	c

.

(î:;s)

CONTRACTOR OF SERVICE - CONTRACTOR - CONTRAC

		(C) X	H H H	UHENT FZ	T XATE	1:2:	O X X	XIAL TRES	G STRES	≻ ₩₩		CCHB
	• 0	2	8474	2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2	2 °	20 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1					E S
	İ	0	2	-3.7		52	* * * * * * * * * * * * * * * * * * *	• •	•	70	0	C (
1, 1, 2, 1, 1, 2, 1, 1, 2, 1, 1, 1, 2, 1, 1, 1, 2, 1, 1, 1, 2, 1, 1, 1, 2, 1, 1, 1, 2, 1, 1, 1, 2, 1, 1, 1, 2, 1, 1, 1, 2, 1, 1, 1, 2, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	_	• ·	7.	7.1	7	~	æ.	•	٠.	20.	0	0
10. 10. 10. 10. 10. 10. 10. 10. 10. 10.	2 V.	, c	 	~ C	7 7	\sim	9 9 2 2	? ?	~ ~	200	0 0	00
1		7	7	, ,	•	. 5		. :	•		•	
			, , ,	17.0			֓֞֜֜֜֜֜֓֓֓֓֜֜֜֓֓֓֓֜֜֜֜֓֓֓֓֜֜֜֓֓֡֓֜֜֜֓֓֡֓֜֡֓֜	•	•	; ;	•	> :
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	: - ~	2		75.2	• •		1.2	2 2	•	, 4	•	٥ د
1		4.3	`.	28.4	3	•	2	?	•	70	0	0
	. !	E.3	2.0	43.6) # 	•	1.2	2		04	94	0
		-	41.7	N	3	-0	12.0	2	10	70	40	C
		7	7	5	. 7	•	12.0	• •	20		30	, ,
	~	٦.	-	6.4	7	•	12.0	9	0	30	10	0
10		~	5.3	110.6	7.	Ф	12.0	Э	0	30	70	0
114.15 -15.16 -1			٧.	104.9	~	•	12.0	3	0	0.4	70	C
14 15 15 15 15 15 15 15		114.1	5 1 6	1	3	•	5 0 3	4			C	•
14		114,1	33.2	56.5		7	44.5	3			•	J ∩
114.15		114.1	15.1	-41.5	•	٠,	44.5				0	1
114.36	,	110.1	? ~	126.6	ŗ.	4	7. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5.	4	0	0	. 0 s	N :
114.36	_		•		•	•	•	•	•	· 1	•	~
114.34		14,3	1.5	1,2	2.6	1 , 2	•	Š		.03	0	~
114, 36	'	14.3		8 60	2.2	1.2	9,0	'n		50	Э	\sim
114,36 = 22,42	_	14.5		7.	7.7	1.2	••	Ŋ		.03	0	\sim
117.00 50.15 34.14 .06	_	14 . X	•	3 .	7.	1.2	•	s.		• 03	0	•
117.00 50.15 34.14 .82 -1.21 -31.77 .46 .02 .02 .02 .02 .02 .02 .02 .02 .02 .02	_ '	14.3	, ,	~	7.7	~	0	Ň		50	C	~
117.00		17.0	~	~		1.2	31.7	3	0		20.	٠,
117.00	_	17.0	٥	4.0		1.2	31,7	3	0		O	~
117.00 = 10.05 = 5.42		17.0	2	÷.	Ð	1.2	31.7	3			0	•
117.06	_	17.0	٠.	3.4	۵	7.	31.7				70.	\sim
117.06 16.54 20.95 =1.07 1.42 30.76 =.55 =.01 .02 .02 .02 .02 .02 .02 .02 .02 .02 .02	_!	17.0))		1D	7	31,7		0		70.	~
117.08 35.40 35.40 30.14 = 1.07 1.42 30.76 = 55 = 03 0.02 0.02 0.02 117.08 74.91 64.91 = 1.07 1.42 30.76 = 55 = 03 0.02 0.02 0.02 0.02 117.08 74.91 64.91 = 1.07 1.42 30.76 = 55 = 0.05 0.02 0.02 0.02 0.02 0.02 0.02 0.02		117.0	6.5	•		3	0.7	7	.01		0	~
117.08 55.40 50.19 =1.07 1.42 30.76 =.53 =.03 .02 .02 .02 .02 .02 .02 .02 .02 .02 .02	_	117.0	۲.	5,5		7	7.0	S	C		0	20
117.06 74.91 64.41 =1.07 1.42 30.76 =.55 =.05 .02 .02 .02 .02 .02 .02 .02 .02 .02 .02		117.0	5.4			₹.		J.	•		C	0
117.08 94.41 70.44 = 1.07 1.42 30.76 = 53 = 06 02 .02 .02 .02 .02 .02 .02 .02 .02 .02		117.0	4.	* 3	J	7	.,0	٠,	Ċ.			20
48 -5,80 58,05 .30 .00 -1,81 .12 .34 .03 .03 .03 .03 .03 .03 .03 .03 .03 .03	- '	117.0	1 .	3) - 	7	1.0	Ş	0			•
20. 20. 22. 21. 19.1		7	X	3	-		1	-	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	į		
00. 50. 50. 51. 51. 51. 50. 51. 51. 51. 51. 51. 51. 51. 51. 51. 51		3	•	•	٠,	•	•	• -	• n	9	> :	` :
	. ! D. 4	. 3			7	, c	9 4	• -	. -	9 6	> 4	5 6
		. 3	֓֞֜֜֜֜֜֝֓֓֓֓֓֓֓֓֜֜֜֜֓֓֓֓֓֜֜֜֜֓֓֓֓֓֓֓֓֜֜֜֓֓֡֓֡֓֡֓֡֓֡֓֡֡֡֓֡֡֡֜֡֓֜֡֡֜֜֡֓֡֡֜֜֡֡֡֜֜֡֡֡֡֜֜֡֡֡֜֜֡֡֜֜֡֡֜֜֡֡֜֜֜֡֜֜֡	•	٠,	, c	•	• -	- <	9 :	> <	:
		•	. ~		٠,		: .	• •		•		3

STRAN SETBER OFTABL REPORT

RESERVATION CONTRACTOR

passes and a manufacture of the second secon

	T810										>	7	
TREBAN GROUNT		TORCE A K	HUMENT MY	MUMENT MA	/*************************************	FUNCE/	TURSION	AXIAL	HENDING	STRESS	STEAR	BIREAK	COMB.
SECTN		8214	SOTY-NT	SAL KENI	32 12 X	41P8	Sdixeri						CHECK
1 -501 7	0	7	-0.57	58,49			1	~	*		0	101	~
	3.6	-7.40	99.4.	43.84		.03	2,32		-,22		10	0.	.023
	7.0	.7.40	-5.55	0.10	۶۶.		٠,	~	0			.03	_
	7.1.	7	79.7.	1.5.			~	Ÿ	•			0	~
	1.5.	. 7.40	•• 55	-20.13	55.		٠.	v	7			500	0
1 717 10	0	-8.31	-47.53	109.57	2	- C	4.2	3	00		-	-	0
	1.5	~	71.46.	7			4.2	•	•				· c
	3.0	·*,31	-31,05	-1111.66		1.84	92.40	- 3	•	1		0	900
	•	٠,	4.14	-221,34		•	4.2	. ₹					0
	1.0	31	55.54	-325.20			4.2	•	~				0
22 200- 1	0 - 0	7.52	14.03	7.05	77	01.0	7	٦	J		į	4	
,		7.54	5,43	40.53	•	•	•		9.0				
	70.01	7.51	-11.47	17.85	60		. ~		• -		- 20	50	
	s	7.66	-20.03	52.00	57.	- 20	2.3	N	1 10		20	20	. 3
		7.50	-30.50	70.55			2.5	20	. 4		200	700	0.00
			!		•) •		•		+		
05 105- 1	3	•	78.84	00.41-	٦.	0	ŝ		.13			.01	-
	2	•	2.30	77.9	╼,	او	Ĵ		2			5	0
	٠.	•	7	1013	•	2	Ů,	→ .	90.			101	0
	1		2.C. C.	16.29			55.	7				5	2 0
		,			,) - B) Di						;
04 105- 1	o o	.15	\$4.	*2.23	20°=		20.		00.		00.	00.	0
	2	. 15	2	•1.20	•	10.	20.4		0.04		00	000	9
	•	۲.	S .	92.	70°	70.	20.	20.	.01		00.	00.	100.
		61.	6,3	6	•	100	70.		\$0.		00	0	0
	711	21.	,		30.	10.0	2	5	90.		00.	00	Ç
05 105- 1	0.0	90.	-1.03	46.4		.01		90.	70				0
	5.8	94.	00.		9	101	-		•			0	0
	7.0	99	17	-1.03			~	00.	•			0	ိ
			9:	25.1-		10.	.18		0		.01	70°	500
	12.6	86.		1.16		10.	619	90	•				c
05 165- 1	0	S	-3.04	-10.41	20.	.03	2.0		_		0.1	10.	C
	5.3	S	45.54	+4.8.	40.	\$0.	2.0	3	00			0	0
	4.	2.54	C	.6.87	•	• 03	50.5-	\$ >	90.		10.	10.	900
	7	ທຸ	3	-5, 10	30.	£0.	2		\$0.				0
	,	ŗ	2.1	-5.33	•	603	ت ٧		.03				0
03 JLS- 1	•	-44.40	50.00	-107.44		~	000		9		-	-	-
		3	20.5	ćh.	3	3.2	06.0	•	•				۱ 🗠
	2.0	00.85	-66.39	7.		A6.2=		• •	50.		=	=	0.54
	•	22.E7	-117.82	Ξ.	;	\$. V	200	•	7		_		
						1		•	•				١

THAN MEMBER DETAIL MEPORT

(C)

7

HANDER MENDER MEDITION OF PERFORM SERVICES SERVICES OFFICERS OF THE SERVICE DIFFERENCE OF THE SERVICE DIFFERENCE OF THE PERFORMANCE OF THE PERFORM

10 10 10 10 10 10 10 10	HENSER GROUP	1010	FURCE	AUMENT	SUMENT.	- X	UKLE/	TURBIUM	≤	BENDING BT	8838	7 4	SHEA	
10 10 10 10 10 10 10 10		1 L	A # 4	0.	စ	» d ×	4 1 A	X X = 7	21	>	2 Table 2	7	#E3	CHECK
10 10 10 10 10 10 10 10	-002 624		¥0,	-107.62		_	-	7	•			6	-	
10.1 1.4 4.5 1.4 4.5 1.5 4.5			¥ .		-42.87	. ~	•	4				07	, 0	360
10		1001	¥.	10.35	-12.61	~	-	4.3	~	•		• 05	\$0.	~
10		15.2	T :	52,78	-5.74	٦.	35.	4.5	٠.	•		*0	40	.032
10		500	z •	70.78	5.74	~.		£.	7	•		- 20*-	- 20• .	•
1	- 505 105-	3	•	17	10.	Э	C	٦.	3	.03		.01	0	C
1		, s	•	11:	900	Э	0	~	3	0		10.	0	9
10		•	S	0.4	67.	•	30.	∹:	9	M 00		70.		0
10		15.2	S O		1.30 2.40	3 3.		77	3 3	8		10		000
1				7			į	•	•	•		•	;	1
1 1 2 2 2 2 2 2 2 2			7.04	25.50	20.74	•	* 1	2 3	'n,			3 6	7 0	120
11.4 7.04 7.04 17.44 1.05 1.04 1.05 1.05 1.05 1.05 1.05 1.05 1.05 1.05		1	.7.54	3	25.60	•	70		. ~	0		50		7
15.2 1.94		11.4	17.54	5.40	17.46		***	•	7	~		10	50	0
1		15.2	•	7.84	49.77	•	0.4	•	7	~		80	60.	3
1	506 165-	9	200.1	07-2		7	0	2.5	3	0		Č	20	5
1,		3.2	1.00	K7.5	\$6.	~	0	~	• 3	0		205	20	
11.4		•	200	5.75	•	.=	0	?:	3	•		20.	20.	100
10 10 10 10 10 10 10 10		┛,	35.	7.54	_	٦.	0	2.3	3	-		20	20•	5
0	-	r	06.1	9.56	Œ	~		×.	3	•		76	۰ ۵	••
1.5 111.2	6- 606 JLS-	•	111.20	•	54.20		7	-3.40	~	9		20.	205	0.038
2		1.5	111,20		43,15		3	5.90	•	0		20	90	~
0. 111.20 154.50 00.89		7°C	111,20		20.52	•	3.	-3.40	~	0		20.	-02	.034
# 2 10 1 10 1 10 10 10 10		9	111.20	134	> X • 0 0	₹.	4	06.8	~	0		50.	20°	4
5-1 10.12		•	111.60	201	69.75	4	3	9.40	-	=======================================		201	20	3
10.12	-002 720 -	0	0.1	16.05	70°86	10	-:	•	12.	S		90	90	050
10.1 10.1 4.15 -4.46 .60 -0.0 4.92 .27 .03 .00 .00 .00 .00 .00 .00 .00 .00 .00	1	5.1		10.48	47.00	\$0.	۳.	•	126	~		96	90	~ >
13.6 10.13		ο,	-	4.15	97.7.	Ю,	~	•	.27	\$0.		•0•	90.	5
- 710 VI= 1 0.0 4.17 -5.50 -105.00 1.54 .50 -12.05 .02 .06 .02 .02 .02 .02 .02 .02 .02 .02 .02 .02		v O	•	7.24	-70.01	7	20	• •	72	, a , o		* 0	# M	500.
- 711 Ple 1 0.0 114.59 - 455.05 - 15.9	710 710		4.17	05	10.441	34.1	5	3	- 1	•				6
12.7 4.17 12.77 -4005.43 1.59 .56 -12.05 .02 .02 .02 .02 .02 .02 .02 .02 .02 .02		•	4.17	20.04	-205.72	35.1	Š	. ~	• 0	•		9 0		
14.0 4.17 126.41 =527.15 1.54 .56 =12.05 .02 .02 .02 .02 .02 .02 .02 .02 .02 .02		12.7	4.17	11.26	60.000-	1.50	-	~		•		20	- 20	300
- 711 Pie 1 0.0 114.59 -45.45 42.59 -1.59 .58 -12.05 .02 .02 .02 .02 .02 .03 .03 .03 .03 .03 14.59 -45.55 315.57 -1.65 20.03 .52 .20 .03 .03 14.0 .03 14.0 -1.65 20.03 .52 .20 .03 .03 14.0 114.59 -421.55 315.57 -1.65 20.05 .52 .29 .03 .03 .03		20.71	4.17	140.41	-547,15	1.54	.56	ิ	ာ	~		20	20	5
- 711 P1= 1 0.0 114.59 -42.59 -1.60 -1.65 26.63 .52 .03 .03 .03 .03 .03 .03 .03 .03 .03 .03	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	s	4.17	1/1,05	-647.47	1,59	.50	∿	>	~		20	÷05	-
6.3 114.34 =159.74 1/9.08 =1.80 =1.65 26.63 52 .20 .03 .03 .03 .03 .03 .03 .03 .03 .03 .0	- 711 11-	5	7	47.47	42.54	=	•	0.0	••	0		.03	0	. 025
24.7 114.39 -295.55 315.57 -1.00 -1.65 20.03 .52 .29 .03 .0		ø	7	-159.74	1/9,06		0	9	s	~		50	0	3
9.0 114.59 -421.50 452.00 -1.65 -1.65 26.63 .29 .29 .03 .0		∿	=	<45.55	315.57	:	•	0.0	v	~		20.	.03	.032
		•	=	-451.54	40.450		4	4	ı	•				•



90000 117000 00000 024 020 029 20000 9000 00000 20000 99000 22460 W 2 0 0 0 2222 99000 00000 20000 90000 20000 20000 PAGE 2000 22.22 M W W W W 72.4 9 2 2 3 AN LAL BINESS 0 0 0 22222 2 2 2 2 2 0 0 0 0 0 0 2222 115.36 115.56 115.56 115.36 *115.50 *115.50 *115.50 115.97 115.97 115.97 115.97 3 3 3 3 3 1.77 00000 36.77 4 0 0 4 V 8 8 8 8 8 2 4 9 0 8 SHEAK FY KIPS 2 2 2 2 2 2 -311.36 -366.45 -415.14 -457.86 270 24 250 24 254 24 324 34 25.45 80.91 81.45 80.64 -445.11 -524.14 -543.73 367,30 355,55 379,11 598,14 79.42 60.50 21.50 22.65 -555.44 150.70 115.17 10.25 155.ce 191.4E 1260.09 1255.5e 190.44 715.06 755.14 -241.64 -503.47 -317.47 -325.64 24.41 2245.07 321.59 47.05 78.04 78.00 94.37 163.55 159.56 159.56 155.01 117.08 1117.08 1117.09 10.14 111.56 7.50 2 2 C C CKCCP AND BERTA LUAD CUNUITION 651

STRAK MERBER ORTAIL REPORT

PAGE 43 DATE __10/05/76

> U.S. NAVY - ACHK PLATFORMS - PATIGUE ANALYSIS - MLM 105.0 FEET LUAD CUNUITIUN NU.

		FUXCE FX	MINERAL	ACMENT .	T.				DENDING STRESS	* 5	SHEAR	CC18
97	1	AIPS	Salvent	SALANI		SAIN	INSKIPS	4 2 3			E .	. H
25- 706 200- 1	•	-14.83	70.78	~	-	-	4.3		34.	.02	0	-
	♬.	24°11°	65.54	•	500-	٦,	7	٤.	•.37	50°	- 03	
	•	01111	7		> :	•		? '	5 1 • •	5 0	C	2 (
	41.4		-110.44	11.24		1.50	4.30	39	99.	60	30	
25- 656 JLB- 1	•	111.52	2	0.0	-	100	3,4	~	.17	10	C	70
	_	111.50	Š	5	*	•	4	. ~	-	0	0	•
	5.0	111.24	5.	3		2	3	~		0.		4000
	•	111.11	247.90	50° 45	59.	.03	3	9/.	010	20	20°	0.0
	-	110.96	2		-	•	ે	-		20.		₹
51- 701 JLB- 1	•	\$	4.3	24	4.5	5	90	?	~	12		
	•	S	5.0	421.2	7:7	7	0.06	7	٦	-		- 015
	۲. ۲.	. 4.51	145.65	307.0	-5.63	97.	Э.	•00	.,21	. 14	77.	0.10
	•	15.21	- : - :	7.10	7 .	7 :	ء 0	• :	: ۳	51.		0 3
	•	ſ	50.631	r.	٥	3 '))	-	•	51		0
55- 705 JLO-	•	-104.52	-328.12	21.9	٠,	30	129.9	~	ĸ	90	Э	3
	•	104.6	ر د د	0.00	•		124.4		~	60	60.	3
		3 :	-227.41		69.2	. 8.8.	76.621-	.,73	#2·-	010	01.	770
	•	0 0 0 1	7	٠. د	•	'n.	124.4	~ '	7	0.	01.	9
	•	-104.51	7	6	3	e.	169.9		~	====		5
56- 700 JLB-	1 0.0	110.98	253.02	51.99		-	~	8/.	.15	20.	.02	900
	•	٠ د د	s.	2	3	- ,	•	~	-	0		3
	•		D	Z	~ ° ° °	•	÷.	9/		0		10.
	•	•	v	100	•	٠.	•	•	0	70		3 1
	•	-	00.70		-	v	·	_	0	50.		~
01- 702 157-	0.0	~•0	オア・オー	12,19	-	-	2.5		~	90	90.	~
	4.1	9.0	15	6.7	Э	0	2,3	~	~	0	.03	~
	3	2 0	¥0.7	9	\mathbf{v}	70.	٤.5	•		70	*0	S
	2 D	10.64	4.00 V 0.00	.5.92 .53.08	35	70	2,52	53	59	900	90	030
01- 704 157-	0.0	-1.25	-22.71	0.7	Y	52.	1,0	0	7	90		3
	7	•	ъ	~	Э		0			0		5
		-1.25	-	2.0	910		-			50	2	: 5
	1 4.1	-1.24	\$0.0 Q	٠	~	.11	. ·	2	-	50.		0
	•	•	2	7.9		900	· •	90.	45.0	100	100 -	.027
01- 801 JL7-	1 0.0	10	60.13	-17.48	•	50	•	. 12		.12		
!		8.55	20.02	250°0	٦.	•	7.0	-	~	40.		0
	707	4.57 1.57	-1.11	200	3 :	31	56.24	. 12	.36	50	• 05	0.0
	, , ,		70.77		•	1	3	•	٢	•		•

PAGE LUAD CUNDITION NO.

										>	7	
AERBER GROOM		FURCE	MOMENT	ENI	/SHEAR FUHCE		TURSTON	X I A L	BENDING BINESS	7	EAK	CUNB
SECTA		AIPS	Sal xevi	SHINONI	DG X	SdIN	SATA	7	- I & y	3 - x C 3 0	- 1	CHECK
01- 606 200-	0	-18,34	70.40.	-110.71	-1.46	.73	-3.77	7	•	• 10	• 10	999
	\sim	-18.34	4.7	42,90	.01	133	-5.77	7	•	\$0.	\$0.	000
	SO.	-16.37	o :	63.31	9:	•	-3.77	3	•	100	10	.051
	20.05	-14,36	10.54	-118.77	1.63		-5,77	10 10 17 17	• 16 • 71	00	A 80 0 0	950
2- 705 157-	_ >	-	70 7	21.4	9 9	•	2.29	•		C	.07	300
	. 3	-	1.35		05.	•	2.29		10		50	200
	3	7	-2.24	. 7		2	2.29	5	.22	50	. 50	036
	- D	11.19	5.06	m J	, c	900	2.29		, 26 18	90	60° 80°	036
2- 704 107-	0.0		-2.10	•	3	0	22.	_	-	10.		5005
	3	=	•	*		0	27	. 01	2	0	0	003
	•	-:	56.	70) D	0	. 22	Э.	70.	0.0	10.	0
	7 9	 	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	. 51		20.	223		• • • • • • • • • • • • • • • • • • •	30		700
2- 705 107-	0.0	-1.34			3				47.	6		420
		-1.33	•	5.0	02.	9	: =	=	. 12	0	90	.012
	7.	-1.51	1.76	13			. ~	=	.31	10.	10.	010
	2 2	05.11	91.7	2.60	52.5				~ · · ·	9 6	9 6	- 4 - 0 - 1
		!))		•	•					
3- 705 157-	1 0,0	-7.15	~	~	07.	90	-	-,37	-,51	40.		970
	7.3	٦.	50.8	~ '	02.	60	⇉.	~.	-30	90.		037
) 1	-	9 1) i		∹.	•	٠,	9 0		900
	20	2.7	8,55	20.02	2			3,7	\$	2 2	65	190
-002 108 -50	1 0.0		50°500	•	1,00	9				-	5	-
•		3	7.7	,	7.	. 22	•			100	50	750
	45.1	. t	~	٥	07.	100	~.			100	.00	S
	20.2	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	17.58	47.73	-1,05	90	2 2 ° C	4 4	-,26 -,55	90		041
3- 803 JL7-	1 0 0	7		67.5	20	•	5	47 · 10		-	9	570
•	~	3	2	1	200			1.28	0 7		90	010
	3	3	Š	07.4	115			-1.28	.~.	0.4	70	
	2.1.2 2.1.2	0 7 ° 0 ° 0	167.95		37°	1.62	\$0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	11.28	**************************************	9	80.	500.
	} 	_		•		•	-		•			
4- 705 107-	1 0 0		70°=	S -	5 T	9		12	151	, o .	, 0°	20
	3	•	15.5	<u>, , , , , , , , , , , , , , , , , , , </u>		• •	⊸ ′ −	• -	A0.	40	80.	200
	7 - 7	· ~	5 p •	Ţ	11.		7	2.7	010	- M		
	1	•		٠					•			

STRANGE DETAIL REPORT

アカスト	FURCE	MI)MENT	NO NE VI	×	UNCE/	10K810N	XIAL	9	STRESS	SHEAK	2 SHEA	•
2.		מן און צון	8d X = 2	24 ×	7 1 X	2	ESS	>	2 • K S I	STRESG	, ,,	• > ×
0	•2•3	14.46	•12.	•		1	:	. 34			90	.022
4.7	2	11.56	00°2	010	9	100	-	- 20		93	. 03	
• •		20.1	•	•	~ ^	9 H	~ -	-		20.	200	
20	-2.3	-20.20	H 50		15.	69	21.	39		50	50	420
•	1.6-	٥.	7.5	•	9	58.	3	~		20.5	0	_
•	1.0	1.1	-	~	•	29	7	-		70	₹ 0 •	0 3 8
• •	0 1	- :	~ .	3 :	0.	29.	3	•		0 0 5	20.	0
		60.03	10.11	0 x	31.	59,	4 4	52.		20°		0.00
0	\$2.5	•	_	1	3	~	*	4		į	á	٠.
16.5	. ~	-11./4	12	21.5	55.	05.1		10		•	, C	2 2 2
65.1	32.5	٥	4.2	20	•	1.5		•		16	10	• 3
37.6	32.5	Ŋ	٦.	L. C7	•	1.5	90.	N		₹ 0	20.	0
500	35.5	7	ō.	60.0	3 0 ⋅	ž . ž	10	133		- 605	\$0.	0
	5,50	7.6	-105.47	~	٠	9	7	**		21.5	-12	•
•	5.50	97.6	3423	21.0	7	0 4 4 0	~	N.		200	0.4	ç
•	2.50	230.40	0 6 4	•	~	9.40	~	.35		80.	0	0
61.5	65.65	167.69	107,00	05.	1.36	00.44	7.5	25.		60.	• 07	990
•	0 0 1	73.	•	34.	•	•	Y			• 10	01.	^
) • O	4.1	5	10.1	•	•	11.8	\$0.	• 26		10.	.01	.013
_	4.1	12.4	9	•	•	11.00	102	. 25		100	0	110
, ,	 J :			•	•	2 ·	20.	52		10	10.	. c 1 c
7 0 7		10.00 10.00	400.50	000		17.00	2 2	2.5		100	5	P 40
			•	•	1	•		! ! 				
•		17.7.7.	73.6	•	0 20	•	3 4	200		200	9	~ ~
, ,	114,5	D . D S J	59.1		. 50	7	97	.25		7	~	0 0
21.3	11 C WG	1500,50	244,89	1.54	95.	26.27	9 4	22.		200	2 6	960
• •				•	n e]: 3 				† • ;		, ,
•		•				•		•			10.	• 0 > 0
14.2		4 58 . 45			3 2	10000				10	5	0 0
	-117.0	3	5 70			2	47	•				, q
¥.	-117.0	1001	ਤ	`.		9.0	47	2			5	033
•	1	~	1.4	71.	0	9	70	95		70 ,	20	7 1 0
`.	20	7.8	5.0	0		•	0	38		0	10	5
-			17.05	. 40	0	-1.05	20.	. 25		50.	20.	.012
•	6	7	2.5	.27	•	•	2	*0		0	0	C
٠,	7									,	•	

STAIN REPORT OF TAIL REPORT

ではなる。

				•								
	UIST				į	i		!.	10 10 10 10	>	2	
NUMBER 6400F	7 2 3 5 5 5	9 2 2 3 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	Z D T		**************************************	/ /	release Ar	AXIAL STRESS	BENDING STRESS	STRESS	STERN	
	-	A 17.0	SdI x=vI	INewips		RIFE	INSKIPS					CHECK
501- 604 148- 1	0.0	00.4	-5.48	£	30.	9	-3.21		27.38	10.	50.5	000
	5.7	66.40	15.80		60.	.01	-3,21	-,33	-, 56	0	0.3	039
	11.4	46.48	.3.00	3.4	15.	0	-3,21	53	••21	90	*0	3
	1.1	<u> </u>	-4.75	•	. 34	0	-3,21	., 55	90.	0	90•	0
	64.8	-4.97	-1.84	• •	.47	0	-5,21	• 33	740-	00	- 001	0
801- 901 JL6- 1	0.0	-13.66	15.47		2,12	Ž	19.		•	.07	100	10
,		-13.65	.7.05	-124.1	₩0.	•	-	~	07.	90	90	
	10.2	-13.63	-23.15	3	•10		05.610	27.	~	20	0.0	010
	24.3	-15.63	-54.47		-1.12	•	-	٦.	.13	0	90.	0
	52.4	-13.62	-50.71	54,46	-1.08		7. o.i	~	Ç.		- 101	3
#01- 903 200- 1	0	-	34.04		10	47	14.50	45	4		•	900
	7		77.7-	t	•	52.	- D - S - S - S - S - S - S - S - S - S				•	0 4 7
	8.62		28.40	m		0.0	20.5	95		20	20	040
	44.7		20.2	2	* 4	6	5.67		٠-		9 0	170
	9.45	Z1.58	37,45	7	72	3	5.67	15				000
:	i								١.			
805- 803 140- 1	0.0	1.66	50.00	-21,38	. 4.	0 <i>2</i>	2.49	8 5	•31	9 0	0.	.017
	7.65	1.66	5.12	10	77.	•	•	3	0	*0	700	0
	7.7.	00.	27.00	Ž 1	•	10.		•	⊶ •	7 0	20.	-
	* * * *		45.4	10.62		60.	•	0 1	97.	90	20.0	0.00
	•		•	`			•		•	- 60	201 -	•
802- 804 104- 1	0.0	.01	07°-	0	00.	•	~	••00	~. 02	50.	.03	0
	5.	10.	20.5	S	22.	•	5,	00.	•	9	- 20.	C
	7.	10.	~	95.	0 :		7.	00		7 0 °	70°	500.
	- 7		66.	٠,	9 6	•		9 :	•	200	20.	0
				₹.	•	60.	•		•	20.	20.	C
802- 805 106- 1	0.0	-1.24	-2.45	=	7	0	2	~	41	\$0.	50.	6.24
	7.7	-1.24	20.5-	-	51.	10.	۲.	∹	٠.		.03	5
	7	.1.23	•	٠,	ુ.	0	~	₹	~		50	5
	***	1.66	0 50	1.57	4.	100	2.	•	.0.	M (6	50	900
		. -		,			•		•			
1 -021 500 -500	0 '	y	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	3	0 :	•		•	• 20	10.	50.	\$05>
	, , , , , , , , , , , , , , , , , , ,	שים מים ו	0.01	•			•	•	12,	10.	10.	\$20°
				- 5		•	•	9.	<u>.</u>	0	0 :	120
	2		27.00	70' 6				•	-	5.	7 •	0 1
!	:	•		•			•				>	-
803- 903 368- 1	0	-51.34	-7.42	-21.98		-1.45	-15.55	73	£0.•	•	•	.057
	֓֞֞֜֞֜֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֡֓֓֓֓֓֡֓֓֡֓֡֓֡֓	21.15	70.0	7	77.	500	^:	`	513	20.	70	100
	707	51.15	23.15)		-			7.°	20.	20.	200
			١			•		۰			9	



(:::

THAN HEMBER DETAIL HEPURT

10/05/76... PAGE NAVY . ACHN PLATFURMS . PAIICUE ANALYSIS . FLE 105.0 PEET LUAD CUNDITION NO.

-/ TURSION AXIAL BENDING BIREGO BARBAR BARBAR BARBAR BARBOS Y Z BIREGO BIREGO STREOS S	. 50° 50° 50° 16° 4	9			0° 70° 25° 60° 50°	00 500 500 500				0. 80. 91. 95. 40.2	31 Z.04 e.36 e.26 .02 .02	7 -1,34 .23 .23 .03 .0	0, 50, 00, 00, 00, 00, 00, 00, 00, 00, 0	7 e1.54 e23 e12 e03 e0	80° 25° 25° 26° 7	40 04 04 03 2		0, 50, 04, 05, 66.8	50, 50, 15, 21, 03, 03	0, 00, 54, 65, 60, 0	2 76.07 .09 .05	5 - 70° - 70° - 20 - 20 - 20 - 20 - 20 - 20 - 20 -		76.67	0, 10, 31, 50, 81,51= 3	5 -16,18	5 -12,18 .02 .10 .01 .01	50 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			31 20-44 .40 .03 .03	
SALE DECEMBER 1	7.	5					•	423	17		22.	15	0.	· · ·	. 15		~.	000	T. 0	50.	1.5	.54		-4.1	1.121	1,14	1.121	-1.12		0	92 1.61	
ACHENI AZ AZ AN AN AN	94 -17.0	191 10	\ 0.1 · · · · · · · · · · · · · · · · · · ·	10.70 40.37	£.00	201 920	7.0	15 -11 -10	200	 11	8.96 15.82 7.42	-2.08 -15.55		07.0	15.60		55. 55.	. 10	•			131.07 61.70	•	144,41	•	40.	•	105.65	! :		74.17	
T X X X X X X X X X X X X X X X X X X X	-39.57	-39.64	00.00	6 - 59,75	1.1		: -	1,12	7	· •	• •	T :		3 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5		4,55	45.6	. 62.59	42.59	65.59	03,0U	95,98	05.01	0 3, 04	4,17	4.17	4.17	4.17		11.000	114.38	
NUMBER GROOF FROM NUMBER AND END END SECTO FILE	•	3 .	• :	200	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Λ.	- r	8.52	0 - 1877 408 4018	7017	10/1	865- 636 146- 1 0.0	• • • • • • • • • • • • • • • • • • • •		2.27	803# 901 200# 1 0.0	**************************************	•	3 3	•	800- 900 JLG- 1 0.			38,0	#10- 910 PZ- 1 0.0		10.	2002		> 10 -	10,2	

STARM THEFFE DETAIL THEORY

CONTRACTOR CONTRACTOR CONTRACTOR

			•					3	-				
7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	BIO	E IOLE		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		France Co.		'3			2	•	
		_	-	7.7.	¥ 3 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	7 J	E RE		2 2 X X X	E30 0HE 678	FSS SIE	כ כ	
SECT	⊢	AIPS	INOKIPS	INSKIPS	SQ X	N L P S	Server		X	SI		E3 /	ü
12- 912 2		-117.	,	7.0	-	•	6.0	3	~	•	~		•
		-117.0	314.85	~	16	-1.66	30,92	47	-17		2	. ~	0 20
	•	< -117.07	150.67	·	-	•	3.0	. 3		. 0	~		•
	•	-117.0	3	5.5	~	•	6.0	3	•	•	~	~	0
	36.4	-117.0	-177.05	2:	•16	e.	5	3	-	•	2	!	Э.
1- 902 184	-	6.5.9	9.64	6.1	3	9	2.5	-	•	-	. ^		900
	•	P. 5.	3	*	•	9	. ~	: -			•	• '	100
!	15.7	·	4.50		91.	70.	-2.55	• 10	.21	. 0		, 111	021
	ָה מי	6.5.0		-1.	55.	0	٠,	7	•	0	•	•	013
	4.75	•	45.	3	3	•	2.5	~		0	· · · · · · · · · · · · · · · · · · ·		027
1- 904 164	0.0	67.01.	-4.14	5.5			2	3	•		-		Š
		-10.5	70.6	7.0	01		2	3) ×	•	•	• •	3 3
	13.7	07.	90.5	14.60	•	.0		43				! !	•
	$\mathbf{\mathcal{I}}$	-10.5	-3.05	4.7	v	70.	2	3	•				0
	41.4	. 5	22.1-	-51.94	99.	0	9	3	•, 35	0			20
01-1001 JLY	0.0		66.16.	9	***		4	:	•	•	•		•
1	0		-26.52	974	•	, 0		, =	be	•	- 5		3 6
	10.01	-	-24.00	2	90	50	33.60	00					
	•		-11.50	-60.	•	.13	33.6	9	0				S
	35.		4.47	24.7	-1.54	-	33.6	>	0	0	6 9	:	0
1-1002 100	0.0 1.	10.04	27.12	Œ	-, 32		4.2	9	•	-	•	•	*
	10.6	15.6	/7.	£	7	-	~		•			• •	50
	41.1	16.0	1001	-	٠٥٠	20.	3	 	=	0			036
			•	3 3	61.	-	4.2	00.	0	•		•	0.5
		00.01	15.45	•	v	-	\sim	•	N	-	0	•	Š
C1-1004 150	•	0 -18.87	00.00	S		•	2	•	0	•	•		70
!	-	¥ 7 .	60.	٥.	~	₹0 •	, →.	٥	-		•		0
		# # # # # # # # # # # # # # # # # # #	•	•	Э	0	۶.۶	•	~		0		0.0
	~ · · · · · · · · · · · · · · · · · · ·	. 1	3 :	•	97.	000	75.67	60	60.	•	•	•	770
:	J	•	•	•	٩.	-	•	٠	~		0		3
902- 905 169	•	0 -3.41	1.14	•	•	0	S	7	~		0.		3
!	٠.	-3.4	∿.	•	57.	•	5	~	٥.		7		5
	•	3	75.54	٠,	•	•		~	-	•	•		5
	7.7	•	10.00	T C T	V 5		10.7	7 .	71.	۰		•	910
	•	•	•	•	•	•		•	•	0) 		5
.601 106 -2	0.0	•	•	-1.44	10.	0.0	54.	•	10.	•	6.		6
	•	300	50.0	3	2	215	29.	200	*04	0	0 2	- :	200
		•		, c		•		• :	•	•	N		0
			1.70	: &			N 40	? :	•	•	·	•	9
	•	•		•									

Column C	1	**	r 193	₩ \$ 2 4	25 25	 	ж е Э	←		9 A G R	,	
10 10 10 10 10 10 10 10	Column C		. S. NAV	Y . ACHK	FURMS . FAI	TOUR ANAL	Ju - 816	05.0 FE		· · · · · ·	9//60/9	i
Column C	03= 909 1994 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TENT TOTAL	ACMENT AY ANOKIP	# 2 H	S T T T T T T T T T T T T T T T T T T T	CE	URSIO HX N=KIP	XIAL TRESS	ENDING STR	SO SHEAR SHEAR	SHEAR BIREO	# 5 5
	01- 00- 10- 00	01		2.		•		0 :	\$ n .	9 6	9 6	
10 10 10 10 10 10 10 10		İ	ļ	2	4 2 2	900			0	200	900	
1	03-1004 180-1 100	67.6		N 1	•	9	3 1	3	~ ·			
10	03-1004 180- 1 0.0	000	\$1.			• 0	`.	ለ እ	0 Z	: :	•	9 5
1	03-1004 180- 1 0.0			7.5		00			<u> </u>	55		3
10	0.0 1 1 0.0 1 1 1 0.0 1 1 1 1 1 1 1 1 1	10.		4.1		0		2	-	00	9 0	2 C
10. 10. 10. 10. 10. 10. 10. 10. 10. 10.	0.5	0.0	•	3,9	~	•	0	•	~	0		70
01-1003 JLV-1 10.0	05-1003 JLV- 1 0.0	 -	İ	0 7 7	~ :	9	2:	•	7	0	~	2 .
05=1005 JLV= 1 0.0	05-1003 JLV-1	· ·			? :	2 2	2 2	• •	~ ?	0 0		7 7 3 0
04-1005 JLV4 1 0.0	0.5	46,8		9.2	V	0	2		7	0		5
10 10 10 10 10 10 10 10	0.5	2		74.8	~	1.1	6.3	9	-	0	0	8
1	04 905 100 1 0 0 - 51.7	100		40.7	3 -	7	?	5	9	0		0 0
04	04) • • • • • • • • • • • • • • • • • • •	8.7	: 7	7	3	3	•	10°		0
04	04= 905 180= 1 0.0 = 51.73 = 55.55 = 64.43 = 0.05 = 0.3 = 5.2	7.4	46.5	12,1	∢.	٠	6.5	2	•	#0.		00
04	04 0.0 0.	0.0	¥ (2.6	ગ :		~ ~		•	9 6		0
04	51.7 =51.67 =2.71 =1.29 = 0.08 = 111 3.2 04 = 905 109 = 1 0.0				2 3		4.	 		20)
04	04- 905 109- 1 0.0 994 1.95 -6.09 -1.1501 -1.4 1.40 1.50000000 1.5000 1	15.	7.7	7.5	3 ~	• •	. J			20		00
13.7	15.7	0.0		6.0	-	•	3	7	. 23	9	0	2
13.7 20.0	13.7 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20	6.6	-		3		7	9	. 0	20	8	: 8
27.4 .94 = .00 = 1.57 = 24.73 = .90 .04 .79 = .44 .00 .20 .03	27.4 .94 .1.57 .24.7350 .04 1.750 .04 1.7505	•		٠.	~ •	•	3 =	9 :	0	100	50.	80
04	04= 906 109= 1 0.0 -11.23 -1.57 -24.7350 .04 1.7 15.7 -11.25 1.00 -4.2511 .04 1.7 20.4 -11.30 8.55 13.0002 .04 1.7 20.4 -11.33 11.42 11.04 .04 .04 1.7 25= 906 109= 1 0.0 12.8252 -14.5611 .060 25.491112.82 8.40 3.5811060 27.4 12.82 13.01 12.8511060	7.6		4	'م- د	0		ŠŠ	- N			
0.9 = 11.25	15.7 -11.25 1.80 -4.25 -11.0 .04 1.7	0.0	ī	24.7	٠,			3	.27	,		3
13.7 = 11.20	15.7 -11.20 5.15 6.5711 .04 1.7 20.4 -11.30 8.55 13.6602 .04 1.7 27.4 -11.33 11.42 11.0411 .060 15.7 12.82 8.90 3.5611 .060 20.4 12.82 15.01 12.6511 .060 27.4 12.82 15.01 12.600	17.	į	4.0	2		~	3		20		03
27.4 -11.33 11.42 11.04 1.79 -447 -418 .01 .02 .04 1.79 -447 -418 .02 .02 .04 1.79 -447 -418 .02 .04 .04 1.79 -447 -418 .01 .02 .04 .04 .04 .05 .05 .05 .05 .05 .05 .05 .05 .05 .05	US= 906 1090 12.82 11.42 11.04 .04 1.7 US= 906 1090 12.82			3° 5	~:		~'	4	•	20.		0.5
US= 906 1090 1 2.82	US= 906 10.0 12.82 =.52 =14.56 =.11 .06 =.6 13.7 12.82 8.90 3.56 =.11 .06 =.6 20.0 12.82 13.01 12.80 =.11 .06 =.6	; ;		0	•		. ~:	. 1	• •	70		3 3
7 12.62 6.90 3.56 -11 .06 -05 .53 .10 .01 .01 .02 .05 .53 .10 .01 .01 .02 .02 .53 .10 .01 .01 .02 .03 .04 .01 .01 .03 .01 .03 .01 .03 .01 .03 .01 .03 .03 .03 .03 .03 .03 .03 .03 .03 .03	7 12.62 6.40 3.56	0.0	ζ	14.5	~		٥	^	0.	10.	0	6
7 12.86 8.90 3.50 8.11 .00 8.02 53 .10 .01 .01 .02 .02 .03 .01 .01 .02 .05 .20 .01 .01 .03 .03 .03 .01 .03 .03 .03 .03 .03 .03 .03 .03 .03 .03	12.42 13.01 12.6011 .00	~ ;		3	-	0	•	.	0	10	0	02
20° 10° 10° 03° 22° 30° 40° 11° 6037 75° 30° 30° 30° 30° 30° 30° 30° 30° 30° 30	12.42 18.52 21.75	7	•	٠ • •		9 0	• 1	5 4			0	2
		27	18.5	1.7	: -	9	9	n s	u r		0	ŝ

:

AND REPRESENDED SECRETARIA BERRESEN

N									,				
100 100	- 1	1) }			-! > ::	~	
100 100			9 X Y	- 2 - E - E - E - E - E - E - E - E - E	E 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	**************************************	7	- - - - - - - - - - - - - - - - - - -	X I A L	NOING SIRES	TEENS TEENS	STRESS	CN14
110	•	-	3	Q X	714	<u>.</u>	7	Z X E		TO X		:	CHECK
1100 5 100 1 10 0 0 11 0 0 0 1 1 0 0 0 1 1 0 0 0 1 1 0 0 0 1 1 0 0 0 1 1 0 0 0 1 1 0 0 0 1 1 0 0 0 1 1 0 0 0 1 1 0 0 0 1 1 0 0 0 1 1 0 0 0 1 1 0 0 0 1 1 0 0 0 1 1 0 0 0 1 1 0 0 0 1 1 0 0 0 1 0 0 0 1 0 0 0 1 0 0 0 1 0 0 0 1 0 0 0 1 0 0 0 1 0 0 0 1 0 0 0 1 0 0 0 1 0 0 0 1 0 0 0 1 0 0 0 1 0 0 0 0 1 0 0 0 0 1 0 0 0 0 1 0 0 0 0 1 0 0 0 0 0 1 0	0-1004 180-	5	18.99	· •		ッ.	0		•	→ (20.	•
1005 100-1			•	05.5) h	• 3	2 9	-	D, 4	3 . –		- 6	3 6
10 10 10 10 10 10 10 10		31.7		1.47	. 200	7		• ~		• 0		•	9
100 100		46.2	•		on'	2	03	-	60	—		0.5	~
	-1005 180-	9	1. A	23,26	23.h	.16	٧.	3	-	~	0	0.0	000
11 11 11 11 11 11 11 1		10.0	_	\$7. .	2.0	2	~	, ±	~	0	0	0	450
100		41.1	-	10.0	3	70.6	70.	4	~	0	C	10.	•
10		\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	-	• •		N X	• 1.5 × 5	3 3	-		7 0.	7 0.	0.050
		1	• 1	•				•	•	151	201		- Can -
10 10 10 10 10 10 10 10	441		·.	-68.10	•	~	7	2.3	\$0.	-		\$0.	100.
			3.58	07.5	٠.	٧.	~ :	2.5	20.	-			3
910 P3= 1 0.0 4.17 P0:29 741.44 1:90 -:53 -:12.16 0.02 31 24.4 4.17 P0:29 741.44 1:90 -:53 -:12.16 0.02 31 24.5 4:17 -:50.0 1 14.75 -:50.4 1.90 -:53 -:12.16 0.02 31 24.5 4:17 -:50.0 1 14.39 -:70.2 1.90 -:53 -:12.16 0.02 0.03 24.5 114.39 -:70.0 1.17 0.0 0.00.7 -:00 -:00 0.00 24.5 114.39 -:70.0 1.17 0.0 0.00.5 -:00 0.00 24.5 114.39 -:70.0 1.17 0.0 0.00.5 -:00 0.00 24.5 114.39 -:70.0 1.17 0.0 0.00.5 -:00 0.00 24.5 114.39 -:70.0 1.17 0.0 0.00.5 -:00 0.00 24.5 117 0.0 0.0 1.17 0.0 0.00.5 -:00 0.00 24.5 117 0.0 0.0 1.17 0.0 0.00 0.00 24.5 117 0.0 0.0 1.17 0.0 0.00 0.00 24.5 117 0.0 0.0 1.17 0.0 0.00 24.5 117 0.0 0.0 1.17 0.0 0.00 24.5 117 0.0 0.0 1.17 0.0 0.00 24.5 117 0.0 0.0 1.17 0.0 0.00 24.5 117 0.0 0.0 1.17 0.0 0.00 24.5 117 0.0 0.0 1.17 0.0 0.00 24.5 117 0.0 0.0 1.17 0.0 0.00 24.5 117 0.0 0.00 24.5 117 0.0 0.00 24.5 117 0.0 0.00 24.5 117 0.0 0.00 24.5 117 0.0 0.00 24.5 117 0.0 0.00 24.5 117 0.0 0.00 24.5 117 0.0 0.00 24.5 117 0.0 0.00 24.5 117 0.0 0.00 24.5 117 0.0 0.00 24.5 117 0.0 0.00 24.5 117 0.0 0.00 24.5 117 0.0 0.00 24.5 117 0.00		707	70.7	20.00	• •	- 1	• •	•		~ <		0 0	96
910 P3= 1 0.0		36.4	3.54	20.5%	. 4	•	יי			, 0			, c
	2		֓֞֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֓֓֡֓֓֡	07 44	**************************************		,						
) T	•		7 - 655	2 2	•		> =	7 0	: =		; ;
24.3 4.17 = 110.4		10.2	-	-15.06	370.89	100		7	20		0	20	200
		24.3	~	100.74	185.62	2.40	•	2.1	20.	0	0	20.	00
1= 911		•	-	Ξ	. 34	05.1	•.	2,1	\$0.4	0	C	70.	0
2 912 P3 114.39 = 922.02	1- 911 -5		. 3	4.04	3		2.64	5.	3	1	0	\$0.	.037
2-912 P3- 114.39 -255.40 -157.45 -1.07		J. J.		0.264	2	-	5.64	5.5	46	~	0		Э
2 912		10.2	• •	255.4	3 '	.	A.64	5.	9	-	0	• 0 •	0
2 912		75.6		277.01	6.V.		• •	יי פיי		-	0 0	0 0	
2e 912 r3= 1 0.0 e117.0d			!		•	P.) ·)))			•		
1=10CZ 20C= 1 0.0 = 23.01	2- 912 r3-		-117,00	680.56	50.00	7.	2	3.0	•	2	0	20.	5
24.3 = 117.00		1.0	7.	7 - 1 - 1			יי יי	•	•	٠,	0	200	2 (
1=10C2 20C= 1 Co. = 23.01		7	117.08	37.54			2.2		• (•	•		2 5
1=100¢ 200= 1 0.0 = 63.01		~	-117.08	177.0	10.2		2.	3	•		0	- 96	1026
1004 200	1-1002 200	3	0		4.7	v	-	•	•	~	0	10	
1004 200-1 0.0		4.0	0	۵. د	`.	.	~	•	•	7	C	0	050
1-1004 200- 1 0.0		•	9	2.0	3	Э		•	•	۳.	0	.01	3
1=1004 200= 1 0.0		•	9	7	11.2	v	7	•	•	•	0	.01	500.
1=1004 200= 1 0.0		•	•	۲.	70.	•	_	•	•	-	Õ	. 504 <u>-</u>	3
22.37 =12.04	1-1004 200	ô	2.2	-29.40	٦.	~	0	~	Š	~	0		.036
0, 42.01 =12.04 45.50 .11 .09 4.62 .18 .15 .0 .0 4.22 .14 =13.40 7.00 .42 .09 4.42 .58 .05 .0		0.	٠. د	-20.17	7.	3	9	~	v	N	0		9
0. 50, 50, 53, 50, 53, 50, 50, 51, 51, 52, 51, 52, 51, 52, 51, 52, 51, 52, 51, 52, 51, 52, 51, 52, 51, 52, 51, 52, 51, 52, 51, 52, 52, 52, 52, 52, 52, 52, 52, 52, 52		200	~ ·	77.71	~ 1	→ ¹	~ (٦,	s s	- 0	9	70.	6000
			•		•	ú	•	Ä	5	^_	Y		> \



(27.3)

U.S. NAVY - ACHH PLATFORMS - FATIGUE ANALYSIS - MLH 105.0 FEET LUAD CONDITION NO.

SACCE AACC AACC AACC	7 M	70.07 7.47 4.47 4.47 4.47	ACTENT TANKA	404ENT RZ PRESTER	/BIEAK FY FY	FUKCE/	TURBION NA NA NA	SALAL GARAGO	NG STRE	SS SHEAK SIRESS	SHEAK	
1000	-	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		٠ ،				9	40		1	ָרָ בְּילֵינָה בּילינ
- 1	0	7	25.1-	5.61	13	0.0	-1.37	101	60.	40	0.1	005
	16.0	\$.	-6,23		3	0	~	3	•	20	0	0
	0.42	7	*****		9	•	~	Э.		20	. 0 s	0
1	34.0	99.	-15.44	454	11.	0	٠,	3	•	.03	0	C
	0.0	70°•	-10.54	ಿ	00	*0	7	3	.31		a	5
	0 %	02	60.00	0.4	•	9	7	3	7		9	. 0
	10.0	₹05	57.	~		30°	3.18	00.	10.			
	0.07	~ 0 ~	37.0	10.	•	60.	7	2	~		0	3
	32,0	- 20.	17.45	97	2	60*	7	3	7		0	5
:	0.0	-1.31	-15.57	69.35	7	0	-	9	90	10	0	-
-	9.0	-1.27	-4.14	-)	0	-	3	1	05	0.2	5
	16.0	-1.23	40.7-	~	3	90.	-	00.	-	20.5	0.5	. 0
	0.47	•1.19	3.57	0	Э	•0•	_	ે.		20.	0	6
- 1	34.0	-1.15	70.4	******	3	0	-1.43	•	-, 25	103		015
200-	1 0.0	24.17	-46.25	1	-	.20	4	9	m	70.	0	3
į	0.0	44.17	-21.34	~	7	02.	7	Ð	91.	0	0.5	6
	10.0	64.17	33.8	-10.15		• 20	11.40	70.	.07	20.	20.	\$50.
	0.47	24.17	20,00	S	7	• 20	3.	40.	0	20.	0	~
- !	\$2,0	64.17	24.50	0		02.	3	20	-	50.	0	•
140-	0.0	1.44	77.5	•	• 10		3	D > •	.25	0.	50.	•
	0	1.042	27.0	-	3	0	3	2	-	20	504	60
	70.0	1.46	3.55	5.24	000	£0.	-1,32	30.	.12	20.	20.	000
	0.42	1.44	•	٩	\$3°	9	٠.		7 0•	70°	20.	3
- [\$2.0	1.42	-2,55	-10.H3	010	ୁ	٠,		N	0	. 603	0
•	1 9.0	-3.52	-10.40	97.48	~	90.	2.6	•	•	70	70	•
	0.1	-3.55	14.5.	ſ	-	90.	٥.	ુ :		0	0	0
i L	10.01	-3,58	5,65	14.09	00	90	-2.05	5		0	0	5
	0.07	-3.61	13,71	٦.	~	90.	٥.5	٦.	٥.	0	0	5
	32,0	*3,64	41.76	17.9-	271	900	Ç.	7	-	20.	20	-012
-007	1 0.0	-18.97	-10.47	30	3		4	S	10	, 60.	20.5	-
	0.0	-18.47	50.	Ð	Э	-	. 3	•	9	0.0	0.5	1
	16.0	18.97	15.51	14.9		.1.	3.40	05	20.	70	. 02	030
	0.00	10.01-	31.45	10	3	-	3		7	20	0.0	3
	32.0	-18.97	47.59	O	э		3	5	•		•	4

TOTAL STATES STATES SANCTON SERVICES CARRESTS CARRESTS NATIONAL SALESSANDING CONTRACTOR OF THE SALES OF THE S

PAGE

		1810										>		
A PROPARE	700x3	1 2 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	FUNCE F.	MORENT	HUMENT	EAR	FURCES/	TURSION	ALIA	9640146	81HE 98	MEAN	HEAR	C. L.
	SECTA	F T .	SAIN	INekips	SdI wew!	X I P &	AIPS	IN-KIPS	9 ME 38	-	, , , , ,	814638	/	CHECK
101-106	100.	0.0	.01	<o. td="" •<=""><td>~</td><td>9</td><td>•</td><td>00.</td><td>00</td><td>00.</td><td>•</td><td>00</td><td>00</td><td>. 662</td></o.>	~	9	•	00.	00	00.	•	00	00	. 662
:		3.6	10.	50.	~	000		9	3	00	•	00	00	Ç
		~	.01	10.	~	00.	•	00.	00.	٠.	10.	00	30.	000
		•	0	-	70°	20.	00.	00.	9	9	00	0	0	000
-		7.5	10.	70.	-	00.	00.	00	3	80	20.	90	00	100
101-104	116. 1	0.0	°.	¿0	•,39	20.	.00	00.	9	0	0	. 8	00	₹000
		٠,٠	00.	\$0.0	25	00.		00.	00	•	20.	00	00	100
		7.6	20.	20.	11.	00.	0	00.	00.	0	:	00	90°	0:0
		2 5.0	3 0	200	.1.	2 2 2	3 0	000	35		000	• •	ر ع ه	0000
							!				<u> </u>			
101- 201	UAL. 1	O 1	3	80°	70.	3.		77	3	2		8	30.	303
	 			200	•	5	2 0		00	000		83	000	300
		•	> (•		•		•	5 6		0	00.	0.00
					•					9		90	90	300
					61.1	•	>			200		009	201	000
102-103	1014	0.0	00.	¥ 0 •		000	00.	07.	000	00	.01	00	00	¢
		5.4	oc.	9		00.	0	00.	9	0	0		00	8
		\$ ° ~	20.	43.	¥0.	03.	0	00.	99	00.	.01	8	30.	000
		7 • • • • • • • • • • • • • • • • • • •	000	` .	•	09.		00.	000	00.	10.	00.	00.	0
	-	5.91	90.	50.	92.	00	000	00.	9	8	02	00.	00.4	0
104- 104	1 -204	0	00.	20.	70.	00	00.	00	00	200	00	00	70	000
		3.6	200	00.	0	00.		00.	9	00.	60	9	0	S
		7.2	200	00.	20.	000	20.	00		00.	50.	00.	90.	_
))	••00	99°	0	9	•	00.	00.	00.	00.	00.	00	
:		14,5	30.	22.	•	2	00.	07	3	000	•	90	900	ŝ
102- 105	- 004	0	10.	00	10.	00	90.	00.0	9	C	9	c	0	
		2.0	6.	200	000	22	0	00	9	C		C	0	
 	i 	7.2	10.	33.	2	33.	20.	00	3	00		000	00	000
		0.01	10.	3 •	20.	00.	?o•	00.	00.	0	0	0	00.	000
		14.5	10.	3.	£0.	22.	20.	00.	9	C	0	8	700	000
103- 105	110-1	.0	.0.	-15	2.	20	0	03	00	0	9	00	90	6
,		3.0	10.	,	31.	5	00.	0		0	0			100
		7.2	10	50.	*0.	00.	0	9	9	G	0	90	00	000
		700	\sim	70.	.03	20.	00.	00.	9	0	0	00	00	000
-		14.5	10.	15.	50.	09.	0	00	0	000	00.	00	000	000
105- 205	טאנ- 1	0.0	00.		15	00.	90.	4.0	00	00		00	90.	000
!		8,2	90.	20.		000	00	97.	•	00.		0	20.	0
		5.7	-	93.	97.	000	0	97.	2	00.		00.	00.	000
			٠.	7.	02.))	90°	\$.	00.	00.		00	3 C •	000
!	i	7			17.		•	9	3	00		 -	00.	၁ ၁ ၁

SESSES PRODUCES PRESENTATIONS OF SESSESSION

			U.9. NAVY	Y - ACHH PLATE	144 . BEAL	I LUE ANALY	118 · "L"	105.0 FEE					
	1910	Ì	1	4	ı	:	•				-	~	
* >)) 1 / 4 4	A CACE	7,776.7	1016×1	EAH F		NUTONILL ST	X JAL	RENDING	STHESS	SHEAK	BAFA	3
346.14	2	RIPS	1 Yek IPS	SdIveNI	247	Salv	Sel Heal		-	, KSI.	914638	2 !	6 CPEC.
1 -00- 501	0.0	•	3	16.	•	•			0	00	90	٦	٥
1	5.6		00	0	•	•	9		0	99	00	00	3
	₹,	0	•	0	•	9	3	•	0	0	00.	0	၁၁
	14.5			70	3 3 3	000	9 0	000	00	000	000	000	0000
100		=	3 4	_					•			•	
•			• •	• 0	, 3		•	• 3		o		> <	ور د د
		10	50	90	07.	90	8	8					000
	•		BC.	-	3	Э	•	0	C	0	00	0	00
	77		50.	2	3	9	•	00	00	0	06.	- 00.	3
100 -10- 1		0.	.01	*0	00	•	0	9		0	.00	0	0
	5.0			₹0.	000	000	0000	00	00.	00	00	0	3
		0	•	\sim	>	2	3	Э		3	00	0	000
	÷	20.	~	~	3	200.	•	9		•	00.	0	3
	•	0	-	2	0	•	6	00		2	30.	00	>
400 UAL- 1	0.0	10.	. 18	*2**	00	•	27.0	00	0		•	_	9
	5.0		7	-11	00	00.		•	•		9	9	9
	7.5	10.	3	70.	200		. 70	. Э	0		00.	•	9
	11.5	• 01	00.	.01	00.	00.	. 74	0	90.		00.	00.	000.
	15,0	10.	_	90	•	•	, 14	ə	0		000	C	3
202 -110- 1	0.0	-:-	\$0°	. 41	20.	90.	00	•	00	0	0	00	9
	5.0	= .	Э	~	00	0	0		C	50.	00	0	9
	۲°,	.,11	7)	1,11	•	00.	000	9	00.	.01	00.	90.	Э
	0		^	5 0 •	27.	0	000	•	0	000	00.	90.	3
		11:-	525	9.	•	90.	00	•	9	0	00	C.	0
204 -18- 1		£0.	-	10		•	3	?	00.	٥.	00	000	_
	3.9	•	111		00	00		00.	95	02	00	90	100
	-:	• 03		~	•		•	3	0	?	0	0	S
	•	50°		50.	•		3	?	00	0	0	0	5
	•	•		011	•	•	.	-	001	.	00	000	3
301 UAL- 1	•	03	-1.40	2	67.	0	3.5	2	•		00.	00	-
	•	500	3 4	ر د ا	00	20.	5.5	3	•		00	0	3
	:_	•	•			2 (•	•		9	0	0
	15.0	\$ 0 ° •	50.5		2 2	3 0	45.50		V 0		9 6	•	000
	•		•	•		٠.) - 					•	
303 120- 1	0 1	5 0.	02.	10°	000	00.	£.	9	20.		00	0	• 001
	ċ	50	•		00.	•		00	•		00.	00.	300
	• =	•	•	•		•	→ •	•			0.	0	T 6 7 .
	•		12.	•		•		9 :	E .		0	00	20 0 0 0 0 0
	ú	•	1			•		9			•	•	

WHEN THEORY, ORTANG TRPORT

) reserved the second s

17.

(r. !.

				I ALTA TEAL	P DEFOLIA	TRAIDOR MARARIAT		103.0 FEE	_				
	0191					:		,		i	>	7	:
SUBSER STOR	, N	2 X :	I A E S	12.21	¥	74	CAN NAT NAT	AXIAL BTREGG	BENDING Y	7 HE	Ī.	BIEFE	C C C C C C C C C C C C C C C C C C C
35.0	•	SATA	DAT YOU	2012	2017	2	BATYON			a Z S Y a a		/	T L
- 205 -10- 1	o 4	===	20.	11.	000	300	00*	.01	30.	20.	00.	00	.000
	2.5		2	40	9 9	30		> =	9	•			> C
	10.0		20	.17	00	00		•			• •		
	14.5	11.	10.	. 2b	00	000	0	3	00	.03	•	00	, 200
- 204 -08- 1	0	00	00	70	9	00-	00.4	00	9	-	•	-	0
	3.0	00	· •	100	00	000	9	9	C	. ၁	0	2	9
	~ :	00	00.	00.	00	90.	00.	3.	•	. 3	0	0	ŝ
	0 :	0 :	•	10.	0 7	90.	0 ·	00.	000	• 00	00.	900	000
	37 i	900	00.	20.5	00.	200	000	3	0	0	00	00	0
- 205 mus- 1	0.0	10.	00.	.01	39.	0.	00.	9	00	ာ	00	00	000
	ر ا	10.	000	0	000	•	00	000	00	00	00	00	000
	~ ;	70°	3		20.	200	00.	3	00.	0	00.	0	900°
) i		3	9	9.	•	00.	0	00	Ç .	0	00	000
	3	.01	>	300	00		000	9	00	0	000	00.	000
- 205 -18- 1	0.0	.01	.11	72.	00.	00.	0	09.	00	20.	00	00	.001
	3.5	70.	.12	• 15	000	00.	00	0	0	0,	00	0	100
	~ ?	70.	~ 0•	3 6	3 :	00**	00*	00.	00	.01	00	20.	.001
) d	•	70.	20.			9	9	•	0 :	00	0	3 6 3 6
	• I į		•,	•			>	3			000	200	200
- 303 DAL- 1	o• o	20.	\$5.	76.		÷0.	•	3	0		00	00.	200.
	ا د د	20.0	5.41	2,52	200	600	•	Э:	210		00	00	200
			70"."				•	> :			0	9 9	000
	15.0	70	-15.20	12.10	3	00	2 2 2		0.5			200	100
300 120- 1	0	.03	01.	3	3	00	5 0,	2	c		00	00	100
	8.5	0	10.	~		20.	50	9	0.0		0	0	100
	٥	\$0.	10.	0	.01	200	50.	Э	0		00	0	000
	3,	40.	\$1.			3 ·		9	10.		00	?	100
	26.0		63.	0001		000	- SO	3	•			90.	100
- 205 mus- 1	0.0	.01	30°	.01	00.	•	09.	•	90.	00.	00.	00	000
	5.0	. 03	000	000	2	•	00.	3	C	0	00	0	0
	~ ·	3.))	0	9 : • • •	30°	000	00	00.	00.	0	90.	000
	> :		•	70°	3 : •	•	00.	•	0	00.	0	00.	000
	C	10.		3	00.	•:	00	9	Q.	10.	001	0	900
- 200 m18- 1	0 0	. n3	20.	.10	2.0	• 00	•	•	00.	20.	00	00	.001
	3	20.	20.	0	3	200	000	00.	000	00	00	00	000
	5.7	50.	\$0°	90	ŝ.	30.	•	•	٩.	.01		0.	9
			40	•	<		٤	:	•	•		•	

C. W.

A LIBERT COLOR RECOLUTION A COLO			U.S. NAVY . ACHK		PLATFUMMS - FAT	TIONE ANALYSI	אן א	105.0 FE	E _		· ·	•	
A LAGER CACCET A LAGER											;	•	
MANAGE 6400T MA	1810	:				ļ	;		ļ	1	¥	7	
205- 206 mls-		M C C C M M	101621 14	ACAENT AN		URCE/	7070YDL	A	BENDING	STRESS 7	STEAT STAN	STEPE STEPE	COTB.
- 206 mla-	<u>.</u>	AIVS	Sal x=n†	IN-KIPS	KIPS	KIPS	INSKIPS			K 3 I			
		.07	03	M 0 •	3	9	00	00	0	9	00	00	000
£7.4	3.5		80.	0	00	00.	Q N	ာ	9	3	00	0	
	7.3	10.	•.15	50°=		•	000	000	00.	.0.	000	00.	.001
•	10.9	.07	₹.	15	000	0	00.	000	ę.	•	00.	00.	.001
	14.5	100		2	000	9	00	00	9	•	00	00	001
205- 501 140- 1	5	.01	01.	30.	9	•	7	00	0		. 0	0	0
	\$	0.0	50.	~	ာ	•	7	•	0	,	00	00	0
	•		90.	.72	· •	.3	7	000	-		8	0	00
T N	ć	100	7	1.00		0.	. 63	9.	.0€		90	00.	.001
	12,4	10		3	-	0	~	00	- 03-		00	-00	0
206- 506 UAL- 1	3	00	40.10	70.0		C	-	00	•		ć	C	C
	£	c	?	200	100	000	35.1					9 0	000
	7.5	20.	4.41	4,25		ာ		00	. 0		00	00.	3
-	11,5	00.	70.7	67.9	•	70.	7	3	C		00.	00	.001
	š	20.	60.0	N 74	•	*0 *	۲.	00	20.		000	.00	100
301- 305 165- 1		37	•	•		9	-	3	c			0	c
		34	92.	: -	•	0	: -	20					, 0
-	14.5	34	77.			00.	~	20.	; O			00	, 3
	41.7	75.		54	000	00.	12	0.0	10.		00	00	.001
	ر دد.٥٠	. 34	•14	*1.	•	20.	∹	20.	Ο,			00	C
301- 300 123- 1		370	47.	11.50	•	00	-	2	0		6	•	c
		C		-1.20	•	0			0				
	14.5	70	97.		200		15	9	3		8	00	100
	41.7	70.	3	04	•	90°		Э	0		0	00.	0
	64.0	30	77.	31	00.	01		9	0		00	000	Э
301- 401 041- 1		0	95.4	-16.97	7	70.0	17 O O	2	¢			c	č
	7 . 1	0	7	~~	7			0	0				, с
	14.2	90.	50.	12.97	7	•		93.	30.			0.10	2
, , , , , , , , , , , , , , , , , , , ,	4	2 2	2	27.94	20 1	700	3 M. O.	9	300	,	50	0	200
			•		•	•	•					101	>
303- 300 145- 1		•.26	.17	1.95	10.	•	~	10.0	•		00.	00.	0
	7.2	• • 50	-	.97		00.	010	10.	-0.		00	00	200
	14.5	92.	. 15	o !	Э,	•	~	?	•		00•	00.	0
	<1.1°	• 50	~			9	~	.0.	٩.		00.	0.	0
	0 6 6	92	- 16	30.1	> 1	0	∹	.	•		000	000	C
303* 403 URL* 1	0.0	• 01	-15.56	12.59	-		20	00.	0		10.	10.	c
	7.07	10.	-5.07	06.10			Ð	30.	0		10.	0	¢
Ţ.,	V :		6.00	97.41	. 1.	7:	29.	0 :	\$0°		10.	• 0 1	100
	7 (F. V.		51.00	7101			• 1		0 9		10.		0 (
1	•						•		•				>

WINAN INIBER OFFAIL REPORT

_											•	•	
200	- XOX 4	FUNCE	MUMENT	MUMENT	P NA MINOS	UKCE/	TURSION	IAL	BENDING 8	TRESS		ZEZ	CUMB
-		M M M M M M M M M M M M M M M M M M M	No I X = X I	•	> 0.1 ×	4	X	STRESS //	-	2 **81	81 HE 88	STRESS	CHECK
	0.0		7.74	3	_	7	90	9	, <	: :	-		9
		0	05.2-	101.	2	-, 12	10.4	3	0			5	
~	7.7	0	-12.54	.8.51	;-	7		00.	0		0		0
•	1.4	0	-22,38	-16.94	-	14	•	000	70			5	200
-	8.8	9	-54,41	-25,34	-	~	•	3	Ο.		0		Ş
164- 1	0.0	5,36	18.04	10.24	50 50	14.	2.7	50.	0		.0		1001
	 	5.30	20.35	-1.70			22.7	20			10	0	000
	2.5	-5.30	34.08	-15.75		10.	4.7	.02		t			200
	7 ·	5,36	10.54	-25.75	5 0 2	•	-22.14	20.	.0°		10.	10.	₹00°
		5,36	51.54	-57.74		19.	24.7	20.	70,		101		₹00
	0.0	* 5.25	<1.57	-45.76	. 6	47.40	•	2	-,02		10.	10.	0
	1.1	-5.75	15.43	-14.66		•		20				0.1	200
	٤.3	-5.25	70.0	-3.50	0	07.	•	•	0		70		ŝ
	7.5	-5.2>	4.55	7.54	•	•	•	•	•		01	010	3
	9.7	-5.25	-3.79	18.65		•	10.08	→	9			0	100
114-17	0	20.74	41.65	11.81	5.	66.	-		0				-
		07.94	72.77			1 ~	6	67	0.5				
	4.5	67.94	47.66	24.01	*5.	.22	13	12	20.				613
	3	07.94	20,40	•	65.	.22	7.9	.27	9		10.		5
	•	97.0	55.14	44.22	•	2		.47	- 0.2 		100	10.	-
511 71-1	9	C	-10.42	58.80	¥4.		1.3		02		101	.01	_
	• 1	Ç.	-14.00	32,95	24.5	٧.	14.5		, °.				0
	- 4 :	•		27.04	24.		3	•	20.		10.	.01	. 015
	.	•	14.52	Z1.14	5 to 5	'n	14.5	•	•		7 0		_
	۰	1	64.13	13.63	7.	V!	3	16.	20.			10.	
500 JL4- 1	0	-63,55	-68.33	-17.80	90.		~	• . 45	0				_
	=	24.50	-14.64	-8.78	٩		'n	\$2.	٥.		10		5
	~ :	24.50	Э,	62.	•		٦.	45	00.				-
	9 4	60.00	v	> 1	60.	70.	15.68	. 65	00		= :		210
	i		•		9 (.			-
7.1.	•	Š	3	-7.95	.76	1	S	67.	00.	•			
	1.1	63.55		07.81-	•76		-16,56	67.	.01		10	10	0
	•	٠.	t V	143.84	?	-	76.5	67.	7 0.		0		7
	•	Š	3	439.25	97.	۲.	12,5	57.	* 0 *		0	Э	3
:	•	S.	20.00-	.49.73	. 10		12.5	62	500		0	0	
165- 1	0.0	-1.70	1.85	-20.16	~	00.	.63	90.	~		10	10.	_
	2.3	1.70	1.63	-15,38	7	30°	.63	\$0.	~		101	104	S
•	0 :	01.1	7 ·	10.d.	97.) (9.	90		10.	10.	500
	? · ·		7	70.7	•	•	50.	0 :	9		.		0

į

0000 23300 000000 90000 22222 30000 22000 00000 20000 00000 002 54298 44500 105.0 FEET 33333 22222 I 727.7. 77777 ----- FATTOUE ANALYBIS 20000 N N N N N 00000 22022 7777 ACMK PLATFORMS Y A Z 22.22 24.00 24.00 10.00 10.00 MUMENT 000 2 2 2 X FUPCE FX FX BYS 2 W 2 W 2 FRUM FAUM FAUM 200× 204 001 503

2002 000 000 000 000 000 000 22222 00000 55555 9 9 9 9 9 9 80000 22222 9 9 9 9 9 9 9 0 0 0 9 4 0 0 0 9 90000 N N N 3 A 0000C 20000 2242 0 2 2 2 2 55.50 00000 3 3 3 3 3 33:333 2 2 2 2 2 V V V V V 44444 2222 1.00 57 2.00 2.00 2.00 V 0 0 V D 1 N E 0 E 2000 34.05 54.05 54.05 54.05 33333 20000 202

CARAN TRIBER CRIANIC REPORT

Besiden (1985) Proceeds (1986) Secretary (1986)

SER SYRVER OF STATE

	1810										>	2	
BEN GROUN	₩Q¥.	FURCE	RUMENT	MUMENT	TARESON !		TURSTON	XIAL	BENDING ST	£88	SHEAR	¥.	COMH
SECTA	- - - -	4 H 8 7 H 8 7 H	31 X = 27	841 K= 21	> 1 1 ×	94 Y	DAXX DAXX DAXX	WINE WO	>	2 2 X	TRESS	x :	
1 0007 574	0-0	3		4	!	,	3	-			•	-	4
	2.5	. 10	. 1		9		. ?	• ~	, -			0	•
	ີ່		7	7.7	93.	~	•	•	70		. C	. 0	3
	15.2	5.51	-	3.80	ę,	0.30	1.93	. 14	010		20.	.02	.011
	5002	Š.	-34.59	<u>.</u>	5	~	⊘ .	-	119		•	0	-
505 105- 1	0 0	.30	.13	-,23	3	00.	_	.	c		.00		_
	•	•		Ð 3	3	200	Э	2	٠,	:	·		_
				7	٠	20.	9	· •	•		00		C
	11.6	3 3	> ~ ~ ·	1.04		9 9	0 0 0 0	70.1	20°		00	000	700
	•	•	١.		•		•	•) -				;
500 105- 1	3	2.34	30.	-	~	•	1.5	Ø > •			.02.	2 0.	0
	5.0	٠,		0	. 12	•	1.5	90	0		20	70	9
	~ :	2,34	1.31	1.92	2 .	**************************************	-1.57	9 3	20.		20.	÷05	700
	3	?'	∴ :	3 0	•	•	^:	20 i	0		20	200	0
	7101	?	•	>	-•1	•		50	-		204	201	0
506 165* 1	•	1.1	09.	1.01	10.	0	٥.	٥.	9		10.	010	Ç
		•	00.1	-	10.	70.	1.04	4.04	-, 02		101	01	003
	٠.	-:			^ ! •	9	<u>ء</u> (٠ •	•		10		0
	•	:-	2000	71.0	> :	•	•	•	•		5		0 :
	•	•	•		•	•	2	•	•		1	:))
606 JLS- 1	0.0	-01.78	7.5	-14.50	. 49	•	•	7	•		. 02	20.	0
	•	7.	7	٠ ; د	v	ဘ္ :	~:	3	O.		200	20	•
	•	- r			v	2 0	`.'	3 :	•		70 •	9 6	9
	• •		-36.00	150.37			5 7 7) 0	V	V 1
		•) ; •	 	l i) l		•	•				•
624 200- 1	c •	÷.	24.65	36.56			÷,				• 03	• 03	
	1 • 1	6 4	, .	6.0	•	-	~ .	-	٦,		500	561	5
	• • •	•	7	•	•	•	:-	:-	•		70	2 0) (
	7.07		16.67	7 4 7		90	•		200			9 0	•
	. :		, ;	• •			•	•	•	١.		!	,
	> 4	ר מ	37.66	• •	•	•	•	၁ :	•			0	0 (
				2 0 0	• -		D 4	•	•		> <	9 6	3 6
	, ,	• •	-76.45	5 2 2	•	. "	•	•	: -			> c) c
1	65,3	`,		7.1	-1.18	. 30	10.01	-,02	9.1				000
		a 4	5	9	-	•		•	•				
	• •	• (2 7		C	2000		, i		7 6	2 0	2 3
1	•		72.22	7	•	• •		•	•		9 6	100	5 6
		0 4 0	34.7	•	7	: -:	74.3	. ~	: -				~ ~ ~
	٠			•	•	•					,	,	,

0 0 0 0 0 0 2000 20000 2000 2000 2000 2000 3 3 3 0 0 3 3 0 0 0 4 4 0 6 8 00000 00000 00000 00000 0000 0000 0000 000000 STEAK STRESS 10/05/76 44444 00000 00000 00000 0000 9 0 0 0 0 4 4 W W W 00000 20000 00000 V = W = V SHEAR M - M M - 0 2 2 2 2 2 9 9 9 9 9 9 20000 0000C 00000 PAGE STRESS BENDING WW. 0 1 2000 24977 2002 30000 - FATIGUE ANALYSIS - MLW 105.0 FEE AXIAL STRESS FEFFE 2 2 2 2 2 22222 22222 2 2 2 2 2 2 3 3 3 3 3 2 4 6 5 5 4444 11.2.58 11.2.58 12.5.58 12.5.58 *65.09 *65.09 *65.09 65.47 65.47 65.47 63.47 TURSION OGI X-VI 90000 2000 22222 20777 20000 11.45 2221 2000 2004 2004 2004 2022 2572 22.22 A DIM A D 2222 8 d 1 X ACHE PLATFURMS 45.55 45.69 49.57 11.98 13.11 17.98 13.11 114.70 178.15 178.59 -51,47 -72,55 -43,58 -114,63 199.64 219.00 231.90 237.21 -154,98 -171,81 -185,17 25.00 25.00 25.00 25.00 25.00 U.S. NAVY -139.54 70.00 191.45 135.40 135.40 115.03 114 CCC 111 SY CCC 111 24 KY 27 EE 27 6 EE 75 EE -71.80 カユーメース 101.77 03.55 03.55 03.55 03.55 0000 0.80.6 F. X B. 8 0 0 0 0 0 F101 F20 F10 LUAD CUNUITIUN NU. GRUCCE BRCTA 200-760-1017 653 621 140 703 570 701 METALK -779 603-

0000 00000 027 025 025 024 024 059 057 089 059 022 007 007 007 005 57 005 57 00000 00000 00000 00000 20000 00000 2 4 W 4 9 20000 -0000 55555 00000 00000 00000 00000 00000 -----N.N.M.N. 00000 PAGE BENDING STRESS 2222 22001 10000 27.00 C.S. NAVY . ACHY PLATFORMS . FAILGUE ANALYSIS . MIN 105.0 PER MAMMM EEEEE 3 3 3 3 4 V W W W W 22222 3 3 3 3 3 3 3 3 3 3 4 120 1000 1000 1000 1000 70 70 70 87 F 2 K 1 P 8 020222 O E P P C 11.07 7 2 2 2 2 24.00 7.37 52.89 1172 34 116 95 51 91 1144 74 1165 67 1166 65 1166 60 SAI YOU 110.71 560.70 14.66 1100 Ve 1175 Ve 1177 Ve *141.65 *144.67 *157.08 101.40 101.74 101.74 20.00 52.73 0 2 2 2 2 ... 4V6 - 0 0 2 N M ~ CUNDITION NO. 7.0 00/ **5**0.7

(4)

					T ACBA PLAT	4	TIOUE AMALY		105.0 FE	- 4				
		_	ł		i		!	1	1	}		!		
A FRANKS	100x3	¥ 2 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	FO PORT	MOMENT		EAR	UKCE/	TURBIOS	XIAL	E .	ESS SHE	3 T	٤	•
10.10	Stiln	F 1	841X	Sel Xevi	SHI X-NI	Salk	SdIv	Set Year	K 1	7 7	× :		2	CHECK
01- 606	200- 1	0.0	0	5.1	9.1	01.	-	5	~	57.	•	•		₩.
1	 	14,5_	0	7.	25.0	~	~	S	\sim	-	0	K	•	01
		1.65	٦,	•	¥.	٦.	000	\$		~	•	-		9.50
		2 2		52,41	52.29	56.	161	1.52	, r	42			200	.020
02- 703	1.97- 1	9	_	56.5	Α.	92.		4.7	•	•	G	•	-	5
			_	7	•	9	1	`~	*	~			ō	1
		•	_		6.2	· >	M	4.7	~	7		1	0	20
		15.8	0.10	21.97	-7.60			87.79	.32	1 3 6 1	0 -	•	60	\$ C 34 C
90% -20	10/01		^			0.0	•	-	=	36				
•	•		22.	-3.60	20°	9 9	77.	7 9	20	62.			, M	
			\sim		£	13	0	•	. >	· N				5
		•	.22	•	£	00.		-	Э	N	•	. ~		-
		ť.	2	•	0	3	2	-	၁	0	•			3
2- 705	107-1		.45	5,63	3	N	• 10	3		_	۰	3		0
!		•	J	1.0	5	⊃	014	0)	719	0	2		9
		•	3	·V.	2.0	?	3 ·	10.		•	•	•		
		77		70°5	27	70.	200	·	3 : 0 :	71.	•	~	20,	600
-		c	36.		-	•	- 44	•		V	•	-		5
3- 705	1 -151	•	۲.	50.00		7	S	s	.20	10.	•	•	C	3
		4.7	3,70	~	7			4.58	021	20.	-	-	00	1204
		•		-1.4	2.5	Э	٠.	Ţ	\sim	0	•	•	0	-
		•	٠.'	٠. :	•	ۍ (د •		S.	01	20.	•	~	201	~
		•	•	3/0		-	Ų.	J.	. 60	/0.	3	,	101	•
109 -50	200- 1	0.0	٣,	~	5.7	20	2	•		27.	0.	•	۰	.031
		۶.	٣.	5.6	1.0	3	20	2.0	2	~	0		0	5
		۲.	٠.	>	T.	?	0	2	~	m	•	•	10,	2
		200	9.57	20.10	50.30	9.00	30	20.2	\$\$ \$\$	- 6			m 3	.016 .024
208 -50	JL7- 1	0 0	٥.	30	5.95	90	1.74	2.7	10	-	· .	•	6	70
		7.1	2.0	7	154.	-	7	4.7				~	20	্ব
! 		14.6	56.65	;	x	15.		-4.75	3	.28	•	-	50	
		61.3	٠,	۲. د	43.5	-	•	2.7			°.	•	•	770.
;		Ē		•	2		, ,	k. 7			0	- - - -	60	3
4- 105	107- 1		Š	Ď	4.70	-	~	٦.	5	-	٥	•	40	-
		•	٠.	2.0		Э	→	٦.	2	~	0	2	, 02 1	5
		>	SB	-6.16			50.	7.14	\$0.	28	•	-	10	7
		•	Š.	٠.	₹.	3	-	7	•	7	7	•	.0°	0

~\`.\

2000 2000 2000 2000 2000 0000 0.57 0.25 0.07 0.22 0.51 5000 7000 7000 7000 .022 00000 20000 20000 00000 00000 5555 6666 STEAN 70000 00000 00000 00000 00000 -K 8 1-STRESS HENDING W = = = = 20116 3 M M O O 0.00 22000 2-14-5 U.S. NAVY - ACHR PLATFORMS - FATIGUE ANALYSIS - MIN 105,0 FEE AXIAL ชชุมพู 3 3 3 3 3 3 3 3 3 3 W W W W W 77777 24444 2000 2000 2000 2000 2000 2000 2000 35.12 51.25 51.25 51.25 51.25 3 3 3 3 3 2222 2 2 2 2 3 2 2 2 3 3 2 3 3 4 9 1.69 O W C C C 10 V W V 0000 2 2 2 2 2 1.52 84 84 37 9999 7777 377,29 361,64 345,98 330,33 221,84 221,31 100,78 15.76 -37.44 -68.74 -159.99 11.00 82.29 117.66 154.41 -342,37 150.70 150.50 10.55 25.75 19.51 67.57 -104.68 -173.13 -150.06 \$20.56 \$15.10 \$05.64 240.67 -253.12 19.00 10.40 -31.67 03.55 03.55 03.55 03.55 03.55 44000 ->1.67 2000 × 1 1 4 CUMPILION NO. 6×CLP AND SECTN 2 15/ **→**00**~**

 (C_{i})

					U.S. NAVY	T - ACHK PL	ATFURNS . FA	IIGUE ANAL	YOIG . REE	105.0 FE	 نعا		i I		
1	+	!	UIST				!!		!			;	>		
10 10 10 10 10 10 10 10		200	F 7 5 5 5	4 X F	E S P E	2 4 4 5 5	TAMENTERS T		L S X	XIAL	BENDIA V	74ES	HEAR	BIEAK	CCAR
10. 1	رم. ا	SECTN .	•	7	7 X X Z	14.	<u>a</u>	9	ATY S			184			· ·
1	300		•	~	3	17.	•	~		~	•		0	0	
1	-		5.7	5.28	10.42	15.	9	2	7	∿	~		50	0	
1			7 .	5.28		ø,	7	٠,	7	v	•		03	0	
1				200	13.48	v	~	~	~	~	N		0	0	
11. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	ļ		Ĵ	- 6716	-65,54	Į.	~	7	٦,		₹.		20	0	
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	106 -		0 0	0	~	5.9	2.0	0	3	_	C		c	C	
1	ļ		200	•	27,22	3		7		•	•) c	5	
2			10.2	٥.	16.18	4.0	7	-	Ţ	-	•		10	0	
2			3,	٠,	20.00	7.0	3	7	ż.	-	-		0	0	
2- 005 100-1 10.0 2- 005 100-1			·	•	7	7	7		\$	-	0		- 90	0	
2	1- 405	20	0	12.	7.0	3.7		9	3	•	٥		•		
2- 004 100- 1 0.0 - 12.44 - 144 17 - 14	ļ		7 7 7	~	1.1	C X	N N	0	t i	•	-		> C		
2- 004 100- 1 0.0			4.4	່~ໍ	10.47		2	. 0	4	. "	•		0		
2			r. 77	2.5	4.6	4.3	٦.	•	7	3	-		0		
2	1	į	50,00	7.	13.0	2.7	٥	12	7.	3	4		0	3	
2	\$ 0 Q	2	1	^	=	2	_	-	1	•	r			•	
11.4				1.00	•	•	• -	• -		•	. c		o c	, V 4	
17.4			11,4	-1.20	•	:5 :5	1	. 🗝	2	2	•		۰ò	•	
### 10			17.1	~	•	9.0	3	-	2	٦.	~		0	0	
10 0.0			8.77	•	'n	M. 3	3)	-		2	~	1	\$0	C	
11,4	40.8	8 0	0.0	٥.		-	9	2	₹.	2	~		9	0	
11.4			7,65			⇒.	Э.	0	~	2	0		C	C	
605 100				•	10.5	~	Э:	0	~	?	~		10.	C	
= 0.5 100			4 7 7	•	77.2		> :	9	~	3 :	٦,		10.	.01	
2- 805 104- 1 0.0	i			•		3	Э.	0	~	3	٠ <u>.</u>		~	C	
11.4	400	i D	0.0	. 58	•	×	~	਼	0	3	~			50	
17.1 .59			5.7	000	121	5.	9	9	3	3	0	1	~		
5- 635 146- 1 0.0 -4.28 55.13 10.00 .0523 2.032025 5.00 .00 .052020202020202020			7.	0 4	95.5	۰, د	.	٠	9	Э	•		_	0	
5= 6.3 146= 1 0.0				ם ח	77°C	2:	₹.	> :	9	A (- (0	
5= 6.25 148= 1 0.0			•		1	ij		⊃;		604.	N			0	
11.4 = 4.28	5- 8J5	# D #	9	4	•	0.0)	2	٠.	7	S		0	0	
17.1 = 4.20 = 10.2 = 17			<u>.</u>	22.	,	ď.	٠,	Ž.	3	7	?		3	0	
5- 905 JL8- 1 0.0 55.47 1.40 17.0548 .0308080808080808			٠,	0 7 7 7	•	'n	Э:	٧.	•	7	•			0	
- 475 JLde 1 0.0 55.47 1.40 17.0548 .05 .00 1.40 17.0548 .05 1.40 17.05 1.40 17.05 1.40 17.05 1.40 17.05 1.40 17.05 1.40 17.05 1.40 17.05 1.40 17.05 1.40 17.05 1.40			: ~	50 V 51	, v		> >	-	, 9	Y ^	-, -			10°	
5= 475 JL8= 1 0.0 55.97 J.20 17.0548 .05 .00 .00 .00 .00 .00 .00 .00 .00 .00					! 	,	,	i.	•	•				•	
0.2 33.84 93.05 -40.09 -4.11 -4.10 17.05 -4.8 -0.8 -0.8 -0.8 -0.8 -0.8 -0.8 -0.8 -0	\$ (a) \$		o .	x, 4	1.17	7	D 4	3:	٠ د		0		00	0	
			ب د ز د	۲.			۸.		2	•	,		500	0	
O ACC SCO CENT CONT. THE CONT.			•	•	77.20		• •	? -) -	* :	- :		N :		
			2	, ~	10.04	4	٠,		•	1			A P	۰ د	

	-
	×
	9
	•
	2
	x
	د
	~
	•
C	-
	w
	۵
	*
	<u> </u>
	•
	I
	I
	z
	4
	×
	_
	•
	-,

		1010									,	•		
MEMBER	ביטטאס.	101	FURCE	MOMENT	MUMENT	BHEAK FU	URCE/	TINSTON	XIAL	HENDING STR	ESS SI	8 - BHEA	CCAR	
1 1 1	BECTR	2 - - -	8 1 1 4 8 1 1 4	94 T Y = 2 T	SdI YeVI	> ± ×	F 2 R 1 P 3	30 X 1 X 1	STRESS /	×		SS STRE	SO CNITY	
3		 	1 .	1		: 		: :	: •		:		; •	, ,
		0 0	20.0	20.20	07 1	9 -		£ 4	200	.	0		3700	
!	!		•	-20.25		2	. 0	20	200				~ ~	1
		44.7	_	-17.04	. S. E.	-	-			•	Ö		, -	
		24.0	43,73	45.74	\$. 19	•	9	æ	1.23	0	0	~	1
. 408	108-1	0.0		***	4.74	_	_	-	3	-	č		5	
,	,		-	45.05	24		•	• -	• •	: -	•		9	
		11.4	•	72.20	-2.40	, 2	2			; =	0		•	1
		17.1		97.1.	4.25	90.	9 0 •	. 11	40.	100-	0	20.02	900	
		K4.8	•	4.41	5.69	-			3	2	0	0	-	1
000	1 -071	0.0	5.50	-24.74	۰	-	20	0.0	97.	3	70	•	20	
		5.7	5.57	-1/.56	2.2	.13	-	. 20		~	0		. ~	
		11.4	5.54	•	5.1	9	-	20		. 12	0	•	5	; ;
		1.7		D 7 .		5	25°	9.	• 26	9.	0	£0°	0.50	
 		66.09	9.0	•		>	つ ;	0.00	900	70.	0		P	: :
. 606	1 -0-1	0.0	3.5	-26.44	6.18	97	0	•		Α.	5	•	∼	
		7.5	٠. د	-10.45	7	Z > •	• 12	9	-	~	0		3	!
		•	٠, ۱	0.0	4042	0 a	110	•	~ -	ζ.	3	•	3 :	
		66.8	5,55	24.73	70.21-	9 9	62.	7 7 7 0 0		077		40.	200	
	į				1 .	1	: '	,	; :			!		1
	1 -007	و د د	٠, ٠	66.54	666,75	20.		3 :	30.0	•	0	•	5	
		• ,	•	9	n s		> 0	7 . a	•	٠,	0		2 3	1
		• ;) - ·	•	9 5	1	•	. -	•	•	กา	
		20.0	· ~	21.03	-57.42	75	0	64.7	75	34	90	100	0.87	:
900	11.80	0.0	1	2 . 05.	50.11.0	•	2	41.4		•		•	-	
))	,	,	3	37 100	-75.80	7.5	790-	441.30		6 1 4 8 6 1 4 8	50		100	
		•	£	.87.70	97.80	•		41.5		7		0	5	1 1 * 1
		3	00°07	-31.65	-57.60	v	0	41.5	•	•		•	.052	
		v	-40.35	95.67	12,89	2	•	41,3	•	7		0	P	1
910	1.5.	•	~	57.25	14,7	.73	0	3		_	١.	0	0	
		•	~	55.84	43.7	6/8	•	3		~	0		6	1
		•	-5.45	24.54	172,85	.73	0	10.60	50°	900	•		700	
		•	~	53.18	F	.73	•	۳.	•	٠	•	•	0	
!		·	v	51.86	<u>م</u>	• / 5	0	2	•	0	0.		0	;
- 911	.4.		٥	``	5,	67.	~	7.	7	-	0	•	_	
		3.1	¥	175.71	-52.07	64.	-1.16	-14.23	. 27	90.	0		017	1
		•	0.89	0		67.	-	3	~	•	0		5	! }
		•	0 %	54.5	~ .	7 T	7	.	~	•	•	•	5	
			3		,		•						•	

0.T

and the state of t

LUAD CUNUITIUN NU.

6 K C C K	F KCA	FUNCE	HUMENT AY	MUMENT M2	*	. ~	TUMBION	AX1AL STRESS	BENDING !	81RE58 7	SHEAR	BIEAR	CONT.
SECTIAL.		SATE	D41 X = 7 1	INekIps	21x		INSKIPB	;		K 8 1			CHECK
	3	3.5	-536.50	-141.23	~	-:	12.6	\$7.	-		.01	0	5
	e.	3.5	-250.90	177.73	7	7	12.0	\$2	-12		100	0	-
	•		102.51	-164.23	-:	-	12.6	52.	0		*0	3	3
	64.5 56.4	62,54	99°6	-150.72	3 7 7	1 1 6 1	-12.67	< 5	90		100	100	014
	! •		•			•	! !		•		•	1	;
~ • * •	0.0	1.35	•	-25°02	>	0			~		10.	0	5
	7.0	1,35	-5.03	-19.52	3	0	4	>		:	.01	100	-
	15.7	1.55	-4.07	-11.34	61.	10.	4	•			2 0 •	0	3
	0.0×	1,35	15.1-	2.58	٧	0	٠,	Э	0		20.	0	0
	21.0	1.55	•	21.80		0	*	00	124		101		013
164.	9	0	5 X 4 S	- 2	9	o	-	^	•		,	c	2
		7.01	51.9	12.810	7	•	-	62					٠,
	15.7	7.04	67.7	_	7	0.	-	67			92	. 0	: 5
	40.0	7.00	1.60	2.84	~		7	V	0		20	0.5	6
	- 67.4	7.09	70.	45,27	-, 52	-	1.14	v	200		- 03	03	• 0 < 5
114. 1	0	.07	_	-06.35	~	7	7.0	2	0		0	0	0 0
	3.	10	10.45	9		_	1	9	. 0		90		0
	10.2	00.	. 🖜	108.34		200	20.19	8	***		70.	20	000
	60.3	•00	7.00	۲.	90.	•		9	-		603		0
	36,4	<0.	-5.17	-19.21	1,42	Q	0.1		20.		0.2	50	0
1800	0.0	_	97.78	12.7	3	C	94	3	C		-	-	3
•	10.0	90.41	61.19	١ ٧	20	0			•				y n
	-1.15	11.07	50.1-	-15.07	50.0	30.	2.52	07	13		10	10	020
	51.7	-11.05	67.1.	3	-	0	٠,	₹.	۰,		0		0
1	46.2	-11.08	-5.66	19.74	Š	0;	٠,	7	-		0		₽
100- 1	0 0	~	3° 3	13.54	7.	•	~	3	-		.03	50	~
	10.0	12,30	モナ・	11.54	-	0	4	45	-		0	508	02
	7	~	24.1.	-19.22	70.		1.59	. t	.17		10.	0.0	.048
	51.7	12.37	4.17	•	7	0	~	. t	0		2 0.	3 0 5	Ň
	- 46.8	~	11.50	18,85	V.	0	~	4	٠.	ķ	50.	50.	Ň
1 -401 506	0.0	\$4.	61.0	14.16	~	3	٠. د)	-		70.	70	0
	3°	6 0	1.67	\$7.	-	20	3	0	0		0	C	3
	15.7	. H.	2.40	æ	٠٥٠	70.	-1.02	£0.	→ 0•		10.	3	Э
	9.07	\$6.	ž	-10.67	Ō	0	• •	Э	-		٥.	0	0
,	67.4	30	7.25	19.1.	Э:	70.	1.0	9	- 15		0	10.	60
104-1	0.0		3.05	.73	9	•	5	9	c			=	5
	6.0	-	٠,	9	9			3				, c	, =
	15.7		70.	51	00		Š	0	•		•	0	0
	4°0%		J.	10.	00.	01	•.58	.01	- 05		10	6	00
		•						,	•				•

THE THE PROPERTY SAMES

PAGE LUAD CONDITION NO.

PROUND NAME	E TO X L	FUNCE	M()MEN	MUMENT	1	UKLE	TORBION		1 5 5 N) I	~ [COMM
NUMBER AND	2	ĭ		71	.	24		STRESS	2 ^		SIMESE	CA117
21348	. F	A 1 P S	Sal Heal	SALK-NI	X I Y	A I PS	INSKIPB	/				CHECK
2- 405 104- 1	0	.73	1.23	05.4	.12	90.	. 25		, 23	2 0.	70.	0.1
	•	64.	56.	05.	90.	0	125	92	0	10.	10.	9
	15.7	•	ο.	3.05	ء •	•	\$2.			00.	00.	0
	\$ 1.2 \$ 7.5	36.	# # # # # # # # # # # # # # # # # # #	0 5.0	90.4		5 Y S	ر د د	~ ~	70	. 0	000
	-	1	d –	•	•	•						•
3- 405 164- 1		7	11.18	5.0	3	0	~	٠.	~			03
		-: •	٠		3 11	•	~	٠,	-			0
			• 1	1	> :	9		~·	•			~ ′
	27.4	31.8	33.	-5.51	> >	3	2.5	. 53	90		00	720.
-1002 180- 1	9	~	•	-12.66	. 21	9	•	3	_		6	2
		~	90.2	7.4	17.	0	•		• •			
	41.1	11.26	. 3	, 🕶	03.	10.	-1.50	3.	21.	10	10.	024
	11.7	1.2	2	7.5	• 10	ç	Š	. 41	0		10.	20
	# 6.2	2.	3.53	~	12.	9;	·	0.41	→		20	21
3-1003 JLY- 1	9	•	-100.02	~	10	₩.	20.6	3	15		90	0
	10	•	0	-	3	1	20.0	Э.	00		70	3
	o:	٠.	いまっちか	J :	~; ∙	٦.	20.0	Э,	.07		• 05	6
	52.4	7.50	50°55	00.00		10.1	10.00 10.00	3 3	. .		9	4 5
		:)))) (- -					•
3-1005 180- 1	0.0	21.79	₹.	5.65	90.	~	N	• 10	.27	6 0.	.03	7
	10.0	٠,	٠. د د	Ç.:	20.	-	v.	~	90	20.	20.	9
		` '	•		n 1	•	•	67.			70	770
		•	3 1	֝֞֜֞֜֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֡֓֓֓֡֓֡֓֡֓֡֓	-	- 1	∵.	~ •	70	20.	200	•
		•	•	06601		u	•			20.	C 0	3
1 -601 506 -1		٠.	-1.10	~	.13	0		•	~		.03	_
	2.0	09.	٥.	7	. 00	0	\sim	2	٥.		905	9
	15.7	900	٠.	_	0	0		•	٦.		•	8
	60°0	9 6	19.1	~ 0 · 1	\ 0 · .	0 0	2		. 0. I	2	20.	V 0 0
		•		d.		, l	j:		_			•
1 -401 906 -7		•	26.	æ ·	٤۶.	•	7.2	•	٥ ٠		. O.	ላ.
	, e ;	7.47	60.1-	-	9	20.	-1.25	150	0.3	20.	20 €	- 115
		•	00°0		•	2 (7:	9.	9		10	
	0 · · · · · · · · · · · · · · · · · · ·	•	7 7 7	***	7 6	• :	? ·	7	~ .			~ .
		•			•.	•	7 .		Э.		10.	5
5- 906 169- 1		-7.33	7	9.10	10.	70"-	82.	. 50	• 10	10.	10.	.027
		•	9,7		20.	300		. 50	500		001	~ :
	7.01	44.4	6 1		۲٥°	9	N	7	•		٠ •	N
				ė			1		•		•	•

	i		
ı	_		
			5
	:		PAGE
			A A
	ı		
	* * * * * * * * * * * * * * * * * * *		
	1		
	;		
	ì		-
	:		0
	f		e.
			æ
	į		م
		• •	I 4
	1	d.	E
	•		۵
			æ
			©
			I W
			£
			z
			x
	į		ب •
	i		
i	1		
	:		
	j		
)	1		
			•
	:		
	:		i
	!		1

RANGESTA CRESTORER SOFFEE GRACITOR BLOSSING BANK

									-				
- 1	1810	- 14					- ;	ij			1	~	1
NUMBER BYD	t 2	7 Y	- - - - - - - - - - - - - - - - - - -			. UKLE = 6.0.	75 X X X X X X X X X X X X X X X X X X X	AXIAL	BENDING	3 T R F S 4		STEAK	
99	1	N 1 P S	BATHAT	IN-KIPS	201×	N 1 P 8	SHINONI		-	K81			CHECK
	•		72	- 1	4	•	1	•	•		;	ć	
7	200	12.45	00.7	7 7 7	10.1 10.1						Э (1 0	> <
	41.12	-12.45	11.	16.77	: 3	. 0	9 40	. 3	•		9 0	9 0	, ,
	31.7	N	-1.50	07.0	. 1.	•	8	₹	3		•	. 0	00
	46,8	-12.40	-4.17	-10.61	V	0	40	*	7		. 02	70	1
0-1005 100-1	9	-41.47	9	17.77	-	-	-	=	•		C	Č	8
		-41.46	•	0	• >	•	7	9 19	•		¢	V (, 4
	21.12	-21.83	9.64	60.7	£0.	00	-1.21	6/.	90	: :			050
	51.7	-41.61		14.51	3	•	1.2		0		0	90	3
	717	-41,19	-50.65	2.84	.	~	7.	~	2		0	0	05
900+1030 JLV- 1	>	ď	7	-13.64	50.	٧,	5.4	9	0		0		0
	100	-64.5	45,69	95.84	72	500	45.54	2	90		0.5	- 05	605
	•	۷.	~		3	•	3,5	2			0		3
	3	•		15.44-	07.	S	5.3	ે.	°.		0		9
	32,4	ຈໍ	41,55		_	0	M. W.	3	Ó				0
10- 410 -5- 1		.5.65	-51.47	15.895.	4	•	7.0	•	~		C	0	5
	6.1	*5.25	25.6	34.4	7	~	6.7	•	7		0		. 0
	10.2	-5,25	2	249,90	95.10	12.	10.78	20.	51.		10	10.	900
	64,3	-5.25	20.02	S.	1.3	N	0.7	•	٠.		0	0	0
	36.6	-5,25	0	2 2		~	2	•	0		01	0	0
1- 911 F3- 1		10.80	609.74	S	~.	0	14.2	~	~		20.	20°	M
	1.0	40 . WO.	414,95	240,12	-	O.	14.2	7	~		0	20.	0
	70.0	70°00	220.16	\$ ·	1.15	00.2	-14.28	- 27	. 1 1		7 0 °	2 0 •	.618
		2 (7	7 7 7	፟.	3 (ď	•		200	200	_
	1	*0.	C# 1 A C T =	-	•	2	7 t	V			201	20 4	_
2- 912 PS- 1		5	-545.00	148.81	5 0°	80	12.0	. 25	₽		20.	. ≥0•	N
	2.0	3.5	407.45	145,41	.05	8	12.0	520	~		50	.02	-
	10,2	٠. د	-630.19	10.541	Э	S	12,6	. 25	-		20°	2 0 °	-
	, , , , , , , , , , , , , , , , , , ,	03,55	125.40	140,14	80°	1	12.67	45 45	9 9	•	NO.	N 0	9 0 0
1 4005 5001-1		-	47 02	7 7	1	-	•		-		•		
		֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֓֓֓֓	2 -	40	•	•	•	•	٠.		> 6	- ·	v
	0.01	15.30		22,66	2.0	100	20	4	21		> 0		460
	0.45	5.3	÷1.	-6.36	7	0	9	3	0		0	10	٠,
	\$6.0	~	7.01	24,34	07.	0	0	3	-		20	96	025
1-1004 200- 1		10	0	15.01	4	0	100 per	100	-		•	C	-
	20	D# 71	10.01	-22.57	20	70			51.			20	
	•		-	-19,24)	0	3.6		-		0	20	~
	÷	9.	77.7	45.55	Ŋ	9	3.8	-	9		Č	•	3
					•		•		•		• >	1	,

BIRAN EFEBRE OFTAIL SEPORT

6.1

U.S. NAVY - ACHN PLATFUNNS - FATIGUE ANALYSIS - MLW 105,0 PEET LUAD CUNULTIUN NU.

**************************************	# 00 0 F	N N O	2 4	OMENT	UMENT #2	E P	FUNCE	URSIU AX		BENCING Y	814E88 2	SHEAR	BHEAK	C 1 1 7
:	Stella		Alra	Sd! Yea!	IN-KIPS	Od7x	RIPS	INSKIPS			X		•	CHEC
101-104	1 10- 1	0.0	0	.13	1.67	•	•	•	9	0	-	90	00	0
1		3.0	-10.	•	1.00		00.	00.	00.	000	10	000	00	• 005
			•	•	67.	•	•	•	•	٠.	0	•	0	3
		0.7	0.	~	60°	•	9	2	•	0	9	9	00.	0
,		,	10.	2	96.	2	•	•	•	٩	٩	··· 00°	0	0
101-104	1 90 1	0	0	41.	7		•	3	9		~	90	00	
		3.6	500	12	2	3	9	Ö		00	•	0		, 3
		7.2	•	20.	97.		00.	00	95	0	9	00		000
		000	•	50.	• 1.9	•	•	Đ	ે.	0	0	00	00	0
		14,5	-193	101	20	2.	٥.	ō	<u>-</u>	-00	0	- 00 · ·	00	0
101- 201	טאנ- 1	0	0	7	~		0	3	9	•		90	00	0
		3,6	20.		10		50.	5.41	00	00		9	30	000
		7.5	0	7	•	•	•	3	3	•		00	20	3
		11.3	•	~	٠.	•	•	•	٦,			00.	00.	3
		15.0	20.	8.56	~		0.	•	3	•		00	000	100
102- 103	118- 1	0.0	1 0.		•	•	••	00	00	0	•	00	00	ာ
1		3.0	10.	\sim	~		0	0	9	0	0	0	00	3
		7.3	10.	75.	~	•	•	00	9	30	.00	00		.001
		0	.01	-	3	•	••	0.	9	٩.	0	00	0	0
		14.5	.01	250	Œ			0	9.	•	0	00	000	700
102-104	100	0 0	10	10.	7	•	•	9	q	C	1	•	0	3
.	•	2.0	0		. 3			9		, o		0	0	, c
		7.2	0	Э		•	•	00.		00	•	00	0	0
		10.0	.01	70.	0	•	•	•	Э	0	•	0	0	00
		3	101	70.	0	2	0	3	O	0	3	000	• 00	100
102- 105	1 -904	0.0	03	10.	0	•	•	00	0	0	•	00		0
		3.0	.03	-	្ន	3		00	3	6	•	¢		00
		7.2	50.	٠	100	07	300	0	00.	00.	9	00.	30	.001
		0 :	•	•	~	•	•	0	•	•	•	000		0
		3	60.	00.	~	3.	0	000	•	c.	•	00		o
103- 105	1 00 1	0.0	.02	87.	4¢.	•	•	•	00	•	3	00	00	0
		3,0	20 9	., 34	. 41		0	0	Э	0	0	00	0	-
		~	70.	7	*2·-	02.			9	• • •	.03	00	70	100.
		0	20.		.17	•	•	•	•	٥.	٠.	00.	• •	9
1		7	20.	99.	\$0.		•	•	9	0	٥.	00.	0 u • -	C
103- 203	UAL- 1	•	0	. 6	-	•	••	2.5	9	0		00		5
		•		10.		•	•	7:1	Э	00		0		0
		_	0	•	•1.03	80	10.	-1.37	00	00		00		000
		•		-1.02	3:2	•	0.	1.5	00.	.01		0		S
		Ś	00,	J	2	•		•	•	(

1

.001 .001 .001 00000 30000 000 000 000 000 000 000 \$ 9 M m 3 00000 200 70 10/05/76 22000 20000 20000 88888 20000 00000 20000 PAGE 00.00 M -- N O M B 0 0 0 0 0 00000 00000 00000 - NM S ~ 00000 - MLH 105.0 FEL BINERS 33333 22022 20000 MMMM 30000 99990 9999 25.55 15.37 3000 4444 - FATIGUE ANALYBIS 00000 33330 00000 00000 22222 20000 00000 2000 42 444 22222 22202 2 2 2 2 2 00000 1,000 1,55 2,11 2,66 30 59 30 59 30 59 MUMENT A & IN-KIPS 3 - 3 D N 2242 77000 41 41 41 41 41 41 00000 4444 0 3 3 0 3 2 2 2 2 2 00000 ~~~~ 20.00 0 9 7 0 3 00000 0 0 7 0 3 0 4 4 5 6 0 9 10 9 10 GRCC4 BRCC4 BRCAN CONCITION 200 207 Š 246 203 200 301

	_	
	3	
	C	
	٥	
	•	j
	3	ľ
	_	,
	_	
١	_	-
	•	•
	C)
	2	:
	u	ı
	1	
	•	
	_ L	
	I	
	Z	:
	4	ľ
	2	:
	_	
	•	
	٠,	

2/2

1	1010 1010	FURCE	MOMENT	MUMENT	4 × 4	URCE/	TURBLUN	XIA	HENDING	27.20		7 4	- 1
A 2 C A 2 C	K NO -	# # # # # # # # # # # # # # # # # # #	¥ 12	2 m	× 0	24	2 X Z	STEES	>	7	317638	STHESS	
	•			9						•			
7	0 4	3.3	71.	# J		•	•	0	00	90	8	8	\$000
		. 64	: ~	<u>.</u>	•	20	• •		20	•	> 0	0 0	> c
	10.9	. 62	13	. 53		. •	2		0	.05	8		¢
	14.5	79.	•114	764	?	0	0		0	0	0	0	00
1 -90H		10.	70	-, 11	٥.	0	0)	00	0	0	0	0
	3.6	10		٥.	2	0	0	00	0	0	0	0	0
	7.6	.01	Э.	0	·	•	0	Э	00	•	3	0	9
	0 7	60	7 7 7	3 3	000	000	90	9 9	000	000	000	30	300
		· .			•	-	>		A	>	•	1	-
100 m	•	\$0°	20.	100	000	00	0	3	0	•		00.	.001
	9.0	50	20.	Ç	> :	00	•	.	9	•	0	00.	1000
	•	•		•	> =	•	> <	? :	•	•	0 0	0 :	100
		•		100	• •		•			200	36	90	
		: : :	: :		•		•	•	•				•
1 .012	0 4	. 34	55.0	•	•	•	0		9	9.0		3	
	- 2.7	- 35	60	15.	000			20	00	03		000	0
	601	34	37.	.15			0	2	0	9	0		. 0
	3	. 32	10	300	00.	00	00		00	•	000	00	001
טאני ז	0.0	• 50	-3.17	-	82.	7	~	00	C		20.		0
	90 T	٥٧٠	29.27	÷.	A,	57.6		Э.	50		0	0	2
	^ =	9 1	٠.	• 6 a	v	~ *	٠,	9	~ .		0	0	0
ļ !	15.0	92	120.01	50.05	G 20	37.	64.70		12.		9 0	2 O	000
140- 1	0.0	Š	27.	•	2	0	•	9	•		c	0	0
	10	•		2.6	70	000	0.0	0.0	50		0	5	900
	16.3	.55	LO.	•	3	3	30	3	0		0	0	0
	, , ,	V	77.	V 1	3	•	P :)	9			0	0
	u	•	•	• I) ·	⊇∮	•	•	-			0	_
4000	•	5 0.		20.		00.	•	0	0	.01	00.	00.	00
	•	50.	10.	9	> :	00.	•	0	0	0	0	C	0
	•	0 0		0	၁ :	•	•	5	0	•	0	00.	0
	5	5 0		: :	9 9						30	9	
1				•	i i	•			٠,	•			:
#18- 1	•	41.	• 16	10 E	•	20.	0		٥.	0	0	00.	2
	•	11.	•	72.	•	000	00		0	•		0	Э
	•	<u>.</u> -			5 5	•	0	٠ ١	3 C	70.	0	00	7 CO .
	•	•		•	•		•		•	•		•	_

STREET DETAIL REPORT

							1						
	,					1					> i	~	
ER PND	E N	, K	-	-	L 24	- F 2	20101 111	STREES		3 RC 63 Z	STRESS	01F 6 8 8	COLDS.
SEC +3		841x	Del Hen!	INSKIPS	S d I x	SGI Y	INSKIPS			K81			4.
- 206 mla-	•	M	.15	-, 36	•	0	00.	•		£0.	00	00	C
i	•	•, 30	20.	0		00.	00	3		.01	00	00.	3
	-	• . 56	17.	30.	10.	00.	00.	20.	00	• 05	00.	0	, 004
	•	97.	\$\$.	•	•	0	0	•		0	00.	00•	0
	3	36	.00	1.45	•	00.	00.	•		113	0	00	0
301 120-	0.0	07	•	10	10.	00	~		0		0		00
		07.		2.6	10.	0	7	9			0		0
:	٥	040	3	•		700	1.26	20.	90		100	5	700
	3	07.	62.	7.7	.01	00.	ď		0		0		0
	32.6	07	07.	5,2	10.	90.	~		0		0		Ç
- 306 DAL-	1 0.0	12.	00	~	E FO	0	10.8	0	9		c	20	0
	· ~		•	13	97	00	. 0		05		20		100
	•	~		-	95.	0	10.	•	0		C	0.5	00
	_:	2	~	44.3	. 58	60	10.8	0	ុះ		0	20.	0
	15.0	^ u	S	5.5	58	0	-10.64	•			20	20	
401 131-		ك	F 17	4	•	•	4	•	•				•
) P	• •			> =		O 40	•	•		> c		3 6
!	3		50	3.51		. 0	787	80	• 0				
	41.7	-1.55	•	9	0	00	10	•			0		00
	•	\$	1.20	3	0.3	00.	.87	0	•		101	001	900
406 121		111	•	ń	٥	c	•	=	Č		•	į	
•		7.1			• •			9	ò				, c
	14.5		25.	40.4	03		95.	70	90		10	0	900
		77	1.05	٣.	Э		'n	3	Õ		0	10	0
	•		ç.	C	Э,	0	J.	2	0			01	0
401 OKL-	1 0.0	10.1	7.26	48,22	7	90	10	0	0	•	90	70	9
	7	•	~	\$	3	-	9				70	9	. 0
	3	70.	~		77	~	9.0				70	70	0
	:	•	3		# .	.36	40.82	.01			70	70.	.007
	•	\$ C .	113.04			71		•	7	\ .	7- 70	70	-
500 125-		1.73	-3.00	0	<u>ح</u>			60.				10.	•
	7.	1,73	76.1.	3,4	٠.		~	60.			0	01	3
	3	1.75	19.	1.12	50.	0.01	.37	0	9 0		100	0.0	500.
	;	1.73	0	5.7	.		~	D			0	• 01	ŝ
	•	1.73	1.66	~	<u>.</u>		. 37	65			0	10.	-
403 UKL-	•		0	2.5	•		15.	00.			40		0
	7.		~	6.3	•	-	15,	0	-		9		3
	2007	M 0		65.25	10:	• 79	-15,77	00.	.13		70.	0.	000
	-		2	-	٠	•	5	9			C		_
			•			•		,					

STRAN BERBER DETAIL REPORT

3	010 FXCH	FURCE	NO. N. P. P. P. P. P. P. P. P. P. P. P. P. P.	MUMENT	3	URCFeeee	104010	¥ 1 ×	27.0	> k	74	9
MAER AND	z	×	. ~	. ~	→	24	e x		C3410 011010			r
9		Selly	INOKIPS	IN-KIPS	KIPS		SdIXevI		*****			. ن
6- 406 UAL- 1	°	7	10	3.6	7	3	32.4	•	7		0	0
-	7.	7.	5.0			. 45	32.4	0	•		0	0
	7 . 7	9.0	64.43	55	0.4	. 45	-32.45		• 17	70	30	400
	_:	7	3.6	8.1		57.	32,4	٥.	~		C.	-
	.	3	72,0	74.3	~	57	32.4	٠.	~		C.	5
1- 501 364- 1	•	0	0	5.1	·	1.5	7.2	•	0		0	0
		0	.85.1	7 .	1.6.	1.5	7.2	3			0	C
	•	•	100.3	32,8	201	5	7.6	•	•	•	•	0
	7 3	40.4	12/.55	278.55		1,53	57.27	~ ~		2.	2.	900
j I	•		•		:); -	•	•	•		-	
1- 510 PI- 1	0.0	5,35		60.1	•	•	24.7	0	0	6 0	•	0
	•	~	10 10	7 2 2 7	.	-	24.7	9:	0	60	600	C
	•	. "	7 2	107.00	•	:	`	> :	٠.	•		0 (
			19.37	-411.24	0 0		87.48	0 0	3 0	0 0		000
		. 1		•	•	•	•	•	•			,
5. 505 JL4. 1		-264.75	41.52.44 1.0.1	91 65		N 4 N	-113.26	90.10	90	100	0.	5
	•	7000	7	100		, in	7.5	•	9	100	100	n u
		266.7	22.4	200.6	, Э		113.2	1	•		9 0	~ 5
	3	204.7	5.4	374,7	~		113,2		=	60	60	6.5.5
3+ 511 P1+ 1		5.69	. O	103.8	8.8	1.7	4	•	6		3	4
		60	0	51.7	2	1.7	1	2	900			
	\$. S		15.84	-	-3.60	•1.78	29.49	1.22	70	0.0	90.	950
	•	6	٠ ا	27.4	D :	1.7	4.0	~	7 0 °		• 0.5	S
			27.4	/ · ·	20: PO:	1.7	9	~	.03		<u> 504</u>	S
6- 506 JL4- 1	•	78.9		1,5	3.	2.6	88.4	-	0	0	0	S
	1.1	278.94	89.42	34.82	1,95	89.5	*88 49	1.10	707	90	70	053
	•	78.9		7.5	٦.	3.0	40.00	~	0	70.	0	S
	•		- 4	ָ מַ מַ	.		37 : 20 : 30 :	∹.	9	20.	.5 O .	5
	•	0	C) •	7 D	-	200	301	50.	5
512 Pl- 1	3	219.5	5.9	5.8	6.	~	5.	1.2	•		0	•
	•	79.3	H. S. S.	020	2.0	7	5.1	1,2	Ç	C	90	9
	•	2/9.5	51.1	760	٠ د د	∹.		~	្		C	•
	7 3	12/4,54		1/4,0/1	70°2		55.12	97.1.	51°	•	90	100
	•			•	•	•! •	•	•	-			0
1 - 502 105- 1	°	.,	5.2	2	• 16	2	7.0	-	94.	50.	0	0
1	•	-	3	ò	98.	91.	7.8	•	65.	90	C	03
	•	۲.	` :	T	•	-	2.6	-	.37	0		0
	- ·				1.65	700	60.7	<u>-</u>	3 0	51.	21.	011
		۲.	3	-	•	00	7.8	-	44	4		

PROBER DESCRIPTION OF THE REPORT

NUMBER S	•	5 1 U T	FUNCE	MOMENT	HUMENT	/SHEAR		TUMBION	XIAL	8	-	SHEAR	HEA.	~
01- 504	AND	× × × × × × × × × × × × × × × × × × ×	× 1 1 1	NAT YES	8414-VI	× 1 P &	FZ KIPS	ST X T X	STRESS /	>	2 K 8 I	87 HE SB	STRESS	CHECK
	65- 1		3.2	•	6.	9	19.		~	٠.			0	0
		•	-23,24	53.3	5.8	3 :	.53	~	1	•		0	0	-
		٠.	v	¥:	56.3	•	3 . 3 .	-	٠.	Μ.		۰.	о.	5
:	,	15.1	20.0	14.50	-86.02	11,17	25	3116	11.	79		21		070
501- 601 J	JL5- 1	•	19.5	Ω	0.8°) ·		4		7		~	N	0
	!	•	9. S	125.		3,2	5	. 4	7	C	:	~	~	5
		•	2.61	~	75.5	4.5	S.	6.4	-	-		7	~	5
!	,	• •	19.51	70.58	-706.65	11.11	29.50	00.70	3 7	45		19	19	020
	1 -00:	•	5.1	97,23	10.8	۵.	1 . 2	9.	•	•		~	919	80
		2.1	-	3	¥.	7	0	•			,	-	71	Ŧ
		3	5	₹ 6 .	55.5	1.47	08.	-6.66	90	. 33			=	540
		•		*** ***	٠, ۱	δ.	Š	0.0	•	-		0	.07	90
i		• >	5.	45.4	56,7	٧.	~	•	•	0		0	*0 •	~
502-503 1	1 -50	0.0	£	5.15		-	-	7	Ň	m		0		080
	İ	5.8	T,	3.7	2.0		2	7	Ň	0		90		5
			50°C		٠,	• 17	., 23	97.6	67.	9.20		* 0 *	5 0.	.02
			£ :	, ,	13.7	•	2	3	N	N I		40.		0
		r	r.	33.0	-	₽ .	Y	•	•	n		0		20
502-504 1	105- 1	0.0	.53	50.40	5.1	•	0	3		N.		0	• 03	10
			.53	٠.	٦,	• ·	0	•				0	603	0
		•	r v	• 4		• •	> <	2 9		-		9 0	3	9 6
!		15.2	55.	6.23	2.76	3	70	1.03	3	2		90	0.0	0 2 2
1 505 -205	1 -50	•	٨	-	-	,00	_	7		ď	-	-		C
	•	6.5	12.0	96.1.		55.0	0	4.0	36	80		0	0.0	100
			٧.	•	7	3	0	7	~			0	10.	03
		11.4	2.0	•	•		0	₹.	~	•		0	10.	2
		Š		4	S)	~	Q .	4	~	-		-	. 113	S
503-505	165- 1	0 0	4.2	36.1	24.7	~	-	7.7		3	٠.	0	905	-
		*	2	28.9	8	7	~	7.7				0	\$0.	5
		ᅷ.	ع : د	٠,	7	7	~ 1	7.7	3			0	• 0 •	~
		15.1	14,26	15.15	カト・コー		75.	7.70		9 3		0 0	0 0	400
: .	!	•					•	•	•	•		•	•	•
503- 603 J	JL5+ 1	0	225	· .	-289.51	57.6	~	-206.97	1.57			. 24	, Z	.082
		•	1 6 7 7	****	11390	•		* * * * * * * * * * * * * * * * * * *	•	•			- 123 -	5
		•		> 0		•	• •		•	0 1		v	7 · · ·	~ 1
		•	225.1	286.1			1 2	208.0		•			* C	•

	•											
,] 	U.S. NAV	T - ACHR PL	TFORMS - F	ATTONE ANALY	1918 . MLW	105.0 FE	E +			· · . [
:	0181	į	!		ļ	:	1			*		! !
	7 X X X X X X X X X X X X X X X X X X X	F C C C C C C C C C C C C C C C C C C C	OMENT MY	UMENT RA	I WE I	74	CION NECENTARY N	•0	DING STRES	E T	HEA TRE	CONB
200	•	8414	SAT KONT	0 1 4 0 Z 1	Pd X	SATY	DATX NOT				/	CHECK
3- 625 200- 1	.	6	79.7	0	4.42	0	10.2	-	0	. 14	1.	.109
	ř		2 1	9.07	28	•	701	⇉.	₹ •	- 12		9
	•	•	9	91.0	7 °	Ÿ	V .	┇.	- :	•	0	9
;	20.3	7 0 (4)	•	6.53	52	33	10.28	-1.27	. 62	- 50	50.	080
9	•	4			1	•	5	M	4		•	•
107 505	•		. ^			~ ⊂	* 7	7 1	-	7.	710	9
		3.65	20.3	10.47	さつ	50.	24.	0	36		20	030
	_	•	•	~	4	7	3	1	40	90	90	, ,
	•	ç	-6.57	20	. 7H	~	4	1	92	14	14	. 053
- 506 165- 1	• •	5.	3.0	3	•		~	10	•	-	110	.073
		5.4	•	C	?	0	~	40	~	11	-	0
	7.6	-45.41	0	51.20	62	-11	7.74	400	•,33	80.	90.	190
	•	5.4	9.	• 5	~	~	~	20	7.	9 0.	90•	.066
	'n	5.4	-10.02	7.	ď	S.	~	Ð.	٥.	01 _	101	0
- 506 165- 1	ċ	0		8	9/•	0	2	•	99.	•0		0
	•	ç.	•	3.0	. 76	0	1.8	~	22,	0	0	0
		10.0		20°39	•.70	100	-1.62	0.50	928	•0•	90	• 020
	•	•	- :		0	9 3	•	•	55.	4 0		•
	•	•	•	-	6)	∍	~	•	C	90.		•
- 606 JLS- 1	•	-	•	W. A	. e		~	30	~		.07	660.
	•	61.2	Ž.	20 t	3.	•	┥.	•	15		900	0
	•	2.5	~·	52.7	~ ·	•	⊶ .	•	~		\$ 0 °	5
	0 -	201.61				900	-	7 P	520		9 6	900
	-		•	•	•	•	•	•				,
- 624 200- 1	<i>O</i> 4	51.41	70.34	265,75	3.10	. 55	12.70	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	1.55	950	02.	.104
	•	•	, ,	2		•	,,	0 2	c -	710		> <
	,		•	117.8	•	•			• •			> С
		æ.	-31,57	-	.~	•	2.7	3 0	0	- 401	- 10.	010
• 710 PI• 1	9	-	å	-411.36	3.	7	24.6	0	-	10.		0
	6.0	5.36		2	2.41	1.10	-24.08	20	30	10	70	7
	7	۳.	90	3.5	~	٦.	24,0	0	4	200		.016
		~		74.7	₹.	۳.	24.0	9	S	50°		0
	•	~	37.	95.8	-	•	24	0	,63	50.		0
- 711 11-1	•	60	7.2	0.5	3.0	μ.	9.	~	٤٥.	90	90	S
	•	60	315.b	16.9	3.0	3	9	2	12	90	90	•
	16.7	200,95	374	30	79.5.	9.40	00.40	1,22	.39	90.	00.	.073
	•	60	833.1	9.00	3.0	χ,	4.0	~	.57	90	90.	S
		•	1							•	•	



1								
UN NUL. 5 ULST FULCE ULST FU	2 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	1 A 1	m 0 x	-		AGE 76	!	
CULT	- ACHH PLATFORMS - FAIL	SUE.	• MLW 10	S.O FEE		ATE J	105/76	; ;
10	S S S S S S S S S S S S S S S S S S S	F 2	A SULVA	XIAL BE TRESS	ENDING STRESS Y Z	OTEN STERN	BHEAK STRESS	C C C C C C C C C C C C C C C C C C C
# YO, 90 = 10	210,90	***	95.22		# T *		3	•
19.0 = 279.34	1.70	? ?.	5.22	2.5	-~		90	95
CHECK A STATE OF STAT	1.39	0.0	85,22	•1.26 •1.26	•• 31 •• 38	300.	900	075
10 0 0 0 0 0 0 0 0 0	1 1.5594757E-0	. 3023	10 =5.290	742E=0	2 8585854			
1.55 = 18,73 121,54 40,92 18,55	•	S.	~	٦.	•	41.		Ñ
	.5	S	~	7.		-	-	9
623 JLee 1 0 0 0 2223.94	4	Š	•	 •	57	~ .	-	50
623 JLee 1 0.0 -223.49 1.5 -224.15 2.6 -224.15 2.6 -224.15 2.7 -224.15 2.7 -224.15 2.7 -224.15 2.7 -224.15 2.7 -225.15 2.7 -22	1057.60		231,14	21.	•	13	13	032
626 JLee 1 0.0 2244.32 4423.33 4442 653.54 633.54 633.34 6	9.40 40.45	37 C	231.3		2	~ •	-	
626 JLee 1 0.0 201.20 309.30 181.30 -3.50 -3.50 1.00 1.00 201.20 309.30 181.30 -3.50 -3.50 1.00 1.00 201.20 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3	7 7 00 69	3.70	231.5		9			0
20 JLos 1 0.0 2201.20 3009.30 1811.30 2.45 2.65 417.00 1809.37 2.10 2.25 2.10 2.10 2.25 2.10 2.10 2.10 2.10 2.10 2.10 2.10 2.10	63.54 -3.9 53.39 -5.5	3.2	231,35	1.57	52	2.7	2.5	6095
5.0 201.51 485.72 185.23 .54 1.8	81.38 •.4 86.17	0.4	4	D 1	U: U	0.0	9 6	D 4
4.0 201.65 6.1 201.65 6.0 178.21 .56 1.5 51 JL00 1.0 -14.77 203.64 -115.74 2.73 1.5 4.0 -14.77 203.64 -115.74 2.73 1.5 4.0 -16.74 200.07 -115.74 2.73 1.5 4.0 -16.74 200.07 -115.74 2.73 1.5 4.0 -16.74 200.07 -115.74 2.73 1.5 6.1 -16.74 200.07 -115.74 2.07 1.5 6.1 -16.74 200.07 -100.00 -25.12 -07.05 1.00 10.0 25.12 -07.55 140.00 -0.0 -26.00 1.00 10.0 25.11 -050.46 -050.01 -0.0 </td <td>65.23</td> <td></td> <td>3</td> <td>• •</td> <td></td> <td>50</td> <td>20</td> <td>•</td>	65.23		3	• •		50	20	•
51 JLee 1 0.0 = 14.77	25	M	0 3 3	1.63	38	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	200	800
3 200 1 0 0 0 25 13	0.27.44 3.0	• •	32.4	~ .	•		1	PA 1
0.0 25.13 =190.94 =1190.94 =100.94	157.20		32.4	: :	• •			~ ~
03 200e 1 0.0 25.15 -99.55 150.54 -629 -60 60 60 60 60 60 60 60 60 60 60 60 60 6	162.43	3.4	232,45		70	20	96	639
10.9 25.11 =36.48 75.46 1.48 .94 .	56.54	0	5.0	•	0	•	0	~
16.3 45.10 38.83 -48.12 2.24 1.3 41.8 45.08 144.54 -242.21 3.03 1.8 1.5 -24.25 -590.70 -650.01 -3.47 -5.1 3.0 -24.25 -590.70 -6.00 -2.45 4.0 -224.08 -050.00 740.70 -6.00 -1.7 4.0 -223.64 -064.36 764.30 -2.19 -1.7	75.46	7 0	٠. د د		9	90	90.	~ 4
53 JLee 1 0.0 =224.47 =545.80 650.01 =3.47 =5.1	46.12 2.2	~	-8.55		35		9	0 0 0
55 JLO. 1 0.0 =224.47 =545.40 650.01 =3.47 =5.1 1.5 =224.25 =590.70 669.55 =5.43 =2.4 3.0 =224.08 =656.08 740.70 =2.00 =1.8 4.6 =223.84 =664.36 764.36 =2.19 =1.2 6.1 =223.65 =641.57 =41.57 =40.50 =1.79 =1.79	22.21 3.0	€.	¥.	90	9			•
1.5 = 224.25 = 590.70	50.01 -3.4	5.11	234.6	2.5		-		•
2.0 =264.00 =050.00 740.70 =6.00 =1.	69.55 -5.0	2.47	232,0	.5	Š			0
701 200 1 0.0 1.187	40.70	E 1	234	1.57	.61		-	6
5.0 45. 11.04th \$2.15m 78.18 0.0 1 m005 10	20.05	14.	252.6		•	::	::	101
	\$. 11. 5	-	6.0	9 1		0.	200	.07
3 51.56 155.63 11/1.56 1.56 0 51.54 150.66 1110.10 11.50	10.10	۰ ۲	12.00	0 0	660		90.	040

DATE_ 10/05/76 2 LUAD CUNDITIUN NU. 5

U.S. NAVY . ACHR PLATFORMS . FATIGUE ANALYSIS . MLM 105,0 PERT

•	
	1
	PAGE 77
	4
, ·	
,	
	-
	3. G
	e.
	*
	-
	4
6	DETAIL
	*
•	
	ED EL EL
	I
•	z
•	∢
•	6
i	
1	
• :	
1	

1 N N N N N N N N N N N N N N N N N N N	FURCE	HOMENT	<u>_</u>	/SHEAK	FURCE/	TURBLON	X14L	BENDING	STRESS	SHEAR	2 .	CCAB
- 1	NIPS	24 X 4 V 1	SdI W-NI	KIPB	SdIN	Sel X-VI	z ı	•	Z K81	3 1	7 E	CHECK
		D :	6.5	~·	15	10.2	1.2	•			50.	60
	203	100.46	26.15		1.05	-10.22	12.1	70.		- 60°	. 60	0.00
	10 % D.	9	0	3	40	10.2	1.2	N			112	07
	-	1, 1661	<u> </u>		· ·) · · · · · · · · · · · · · · · · · · ·	7.			-	~	C.
	261.44	0000	3 3	•	•	∹.	•	M M				0 0
		61.007	•	٠.		: -:	2	, m	:	• •		0
	201.07	\$	45.64	2.12	-1.64	-13	1.03	30			9	. 097
	200.64	440,15	~_	v.	2,2	-	•	~		0		5
	~	300.57	•	٥.	1.2	10.	~	7		2		0
•	-21,20	v	~	10.0		10.0	7	c		20		0.3
	-41.19	~	₹.	11.5		10.0	~	7		• 20		9
	-61.19	225.91	·	-12.46	01.1.	610.60	5.15	. 30		90	.30	.020
1	-21.18	>	-153,19	13,3	•	9. 0.	~	-		32		0
0	-240.07		~		0	268.1	۵.	~		• 1 •	-	0
	-240.08	-626.15	3	∹		266.1	•	•		-		2
	-240.07	4530.05	٠.	•	•	266.1	4:	Ň		01.	-	0
	240.08	100000	362.77	0 0	51.0	-256.16				2	٥,٠	9 0
1	260.A4	4004	` `					•				
	*	540.07	7.7		~	-	0					•
٠	200.84	302.70		2.43	20.00		1.82	02.		20.	6	. 493
~	•	208.45	165.0	•	4.7	∹	•			0	0	0
i	200,44	99.01	J	3	\$	∹	0	-		10		0
_	60.03	24.00	-	3	-	3.0	•			707	200	0.7
4.7	20.05	14.62	36,39	50.	91.	-3.08	1.07			50	90	080
.	20.03	C . E O	2	3	-	3.0	•			90.	90.	ę
_	50°07	-5.46	۰	•	~	9.0	•	~		.12	. 12	8
-	50.02	•13.36	~ !	v	-	٦. د	•	1,36	,	910	910-	
e.	-3.36	-12,02	٠.	3	Ò	5.3		S	!	60	60	0
_ `	-3.54	35.6	3	9	ō	5.3	7	-		90	90	3
3	-3.31		20,16	7	10.	-5.57	17	50		60	60.	.033
	2.0	79.	٠:	ο,	•	· ·	∹.	-		.13	<u> </u>	_
•	3.60	01.	>	v	0	2.	~	_		•	_	9
	23,18	171,18	ě	•	-	0.0	1	.32		.22	~	N
	25.21	•	÷	₽.	٥.	9.0	~	£		114	.14	90
7	25.25	3	s	:.	08.	120.63	25.	\$9.		= :	=	.045
9 3	62.67	72.30.0	V Z	'n٦	0 4	• •	9 4	J -		-;	7.	50
	*****		֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜		•		774			•		١

KAN KENBER OETAIL KEPORT

30

PAGE LUAD CONDITION NO.

HERRER GROUP			HOMENT	1	2		10H810H	XIAL	HENDING 81	RE SS	EAR	SHEAR	AL
A 20	7 E C	* * *	2 T T T T T T T T T T T T T T T T T T T	24721	> 4 0 0	8d14	AN NEW TON	£ 33	>	2 x 8 7 e-e-			CHECK
	ĺ	ì								i	i,		•
-002 409	0			•257.23	-3.10		7	3	•			2	P
i	16.3		w s	,	? ·	0 0	7		ŗ.			~	5:
	17.4	7	• 1	101	•	9 4	•	•	9 1			•	- 6
	200	E . 3 &	-54.52	-240.M7	2.51	0	07		10.1		11.	. 11	131
	•	•		•	,				. '		,		
-/27 20	o	22.74		Ž	ο,	0 (₹.	7			7.	£ .	.00
!		: ^	25.53	Ç٠	۰	-	?"	•	v		•	0	100
	•	•		0	y -		? "	:-			•	•	• •
	•	27.74	11.11	5.50	50.	.26	2,33	-	22.			50	t #
04 107-	0.0	23	-2.30	•	Э	•	9	9	-		10.	, O	0
	4.7	~	3	7	20.	300	•	2	7		20	20	
	3		3	15.57	20.	90.	1,03	20.			20		000
	14.1	~	1.44	~	20.	• 10	٠.	•	٠.		£0.	.03	8
	E .		8.55	~	9	~	3	2	2			90.	•
-/01 50	1 0.0	S. O	76.5-		٥	0	٥	7	00			-15	5
1	4.7		•	7.1	27.	>0.	20.	25	26		90	90	0.26
	3	0	-1.48	18.34	3	0	٥	7	61			20.	3
		3.0	•	5.2	3	0	٩	?	• . 16			• 0	20
	13.0	?. ~	2.5	ę.		0	•	~	1.06			910	Š
05 137-	1 0.0	•	6.19	ę.		2	2.	٥	٠.		207	.07	7
	•	₫.	-0.12	~	•	-	2,0	Ð	S		90	90	ę
	3	-12,80	-11.64	06.5-	240-	50.	-2.00	10.	-,23			0.	.054
	•	ar i	-12.25	S	•	0	2.0	Δ	m		9 c.	• 0 •	€
		œ.	30.5	5	•	> 0•	ر د	•	۲.		96.	96• 1	~
01 200-	1 0.0	0.5.0	-61.57	243.66	3	.39	•	1.1	•		.21	12.	3
i	12.5	0.77	-11.85	6	٥	~	•	7	•			-	6
	45.1	D	14.70	2.5	3	.15	•	7:1			.03	. 0.	\sim
	50.05	10°33.	54.15	46°56•	04.1	- 02	79.6	91.19	75.		2:	0.5	000
				•	11	i F) 		•	١.	:	•	·
05 JL7-	7 0	202.1	~	73.2	-1.05	Ç.	٠ د	٠ د	•			.17	5
	10.	-202.11	473.00	402.03	6.55	-1.35	86.02	98.8	•79		2	010	173
	V • • • • • • • • • • • • • • • • • • •	1000	CC	200	E :	•	•	9	•			10	2
	•	0 0 0 0	_	5.0	. F	•	?	, e	•			٠.	S
İ	•	202.0	•21.65	•	3.32	3	٠ •	2.0	•			- 121	7
05 107	0	~	3	-		.03	_	. 27	_			9	4
	4.7	3.20	00.5		37	10.	17	22	5				
	7.5	N	v	v		70.	-	.27	S			10.	5
	1.01	~	7	0	077	9	-	2	•			•	2
							٠		v				٧

BIRAN HENBER DETAIL REPORT

ACTIVATE THE BAT	1010	9 741	1 1 1 1 1	MIMENT		/ F /	THESTON	N I A	10	A 2 2 4 6	2 2 3 4 8	1
HIER ALD	, j	1 × 2	¥ ¥	92	3 × 4 ×	7 4 X	0 X X 0 Z I	g .	Z Z	STRESS	81RE 58	CHECK
	-	2		•					: 45	C	. 0	. 470
•	7.4	. ~	-7.46	53.48	•	•		•	62.	101	0.	100
	7 .	٠ د	# D	~ .	F 1	0	٠,	•	7.1	01	~	0
	66.9	113.00	77.7	76.07	1.14		7.01		-1.12	-		250°
		0	7. 44	0			7 77	•	-	1 2	-	Ç
		,	61.74	٠.	1.54	200	37.7	***	377	.0		200
!	10.2		-30.41	7	75	S	37.7	3		90		0
	64.3 32.4	70°57	-15.17	60.05	-2.01 -3.52	-,41	-37.70		-,26 -,16	12	90 1.	. 0 5 Z
110 905 2000 1	0 0	3	7 7	-111-11		-	• •	1	<	 	-	_
	3.	47.55	-15.01		40	75	-12,18	1.25	52.5	0	0	
	4.47	\$	-64.15	~	•	2	16.1	۲.	30	500	C	0
	L . 7.7	2	-51./4	~	•	3	14.1	7		0.	60	0
	29.6	3	85.10	٠.	1001	Œ,	12.1	7	1,22	- 113	-113	100
2- 803 146- 1	0.0	3,11	****	45.55		~• 05	•	.15	.62	01.		•
	۲.۲	3.11	-10.KH	2	3 1	0	3	51.	, 26	90		0
	7.	~ ~ ~	14.61	~ 0	⊸ •	~ ^	•	5.	n r	S 0	0	0 (
	****		17.64	0.0	n ••••••••••••••••••••••••••••••••••••	32.	0.0 0.0 0.0					0.0
		: :				•		:				
2- 804 108-1	o :		-3.25	24.11	00:	្ទ	•	M :	. i.	70	70.	c .
	\ .	55.	2,5	າ 0		9	•	> :	02.	\$0 B		58
		11.	77			> -	•		- c	•	> C	3 6
,	46.8	55.	9.35	30	0.3	9	20	63	.31		96	0 1 4
2- 805 194-1	0,0	-2.61	- 3.18	27.45-	55.	0	1.4	. 22	•	-	-	2
•	2.7	5.54	1 7	1.92		•		. ~		.00	0	20
!	11.	-2.50	-5.65			0	7.	~	~	100	0	-
	17.1 22.8	-2,56 -2,55	N. 00	3.00	5. 0	9 0	87.1	. 42	10	11.	57	010
5- 805 148- 1	5	12.34	10,30	57.67	41.0	46.	***	•	3	6	č	9
	5.7	2	-10,45	-18.58	7		7	28	36	0	10	0.00
	11.4	12, 52	-44,04		7	C	2	s	~	. 02	. 20	3
	17.1	12,32	70.22	3.26	07.	70.			32	2	200	9
		76 + 77	9.6/1	•	•		0	961	136	70.	701	3
3- 905 JLB- 1	0.0	= :	-75.42	S.	-1,25	-2.27	•	.1.00	• 10	010	• 10	
		112.0	-614.40	~ ! o :	•	• :	3 :	•	7	50.	\$0.	0
	7 · · · ·	: ~	60.401	0 7 0 7 0	10.	9 6	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	• •	12.	50.	50.0	2
			1111	:		•	•	٥	5	90	2	×

STRAN TELEFIC OFTAIL REPORT

A TANGGAN SANGAN MAKASA PERSENTENSAN PERSENT

by your extended something by

PAGE 79 DATE 10/05/76 U.S. NAVY . ACAN PLATFONES . FATIGUE ANALYSIS . HE 105.0 FEET LUAD CUNUITIUN NU. 5

MERUEL	100 100 100 100 100 100 100 100 100 100	7 Z	FUNCE	OMENT	UMENT F.2	WY.	Ct ***	UKS10	7 8 8	BENDING SIN		TRESS	SHE AR	CUMB.
	SECTA	•	Ø 1 ←	Palven!	8114e11	Sal'x	× 100	Salveri		•				u
904 - 700	157- 1	0.0	~	2.13	~	2	-	Š	~	S	_	.13	.13	2
1			-5.59			3	9	'n:	4	7	-	; •	0	20
			•	7.00	9	? "	•	Ų,	'n٠	٠,		5 0	٠ د د	20
!		¥ .	.5.69	25.	-15.56	17	72	4.57	5	27		12	12.	031
		c			•	1	•					,	,	
)) t	n =	5 0 0 1 0 0 1	7	'n	-	•	•		-	70.	10.	5
		3	~ ~	300	<u>-</u>	•	~ -	• 1	•	~ ~ ~ ~	-	-	•	000
				•	: ^	•	• -	•	•			7 6	> c	000
		18.8	-17,35	27.50	27,33	15.	19	- 65	0.0	99	-	03	M.C.	0.40
0 4 0 4 0	2000	5	-	1	э	1		3	•				٠	- 7
		16.5	-	12.62	. 3		. D		•	- ^			> c	3 0
!	!			-103.10	٠.		. ~		• •	1 10		0.5	20	
		57.0	17.79	-75.00	32,01	02.	.57	26.	2.04	4.	-	.03	.03	.114
i i i		•	`	97.09	0	٠.	~	~	•	9		70.	. 404	
909 -90	11/1- 1			150,12	N	3.0	~	± .	٥	.33		.22	.22	m
!	1	7	6.5	412.40	3	~	٩	70	٥	•		=		7
		7.7	180.50	455.48	0		79.	-94.41	2.08	.62		60.		.150
			5	511.54	ć	3	•	9.	•	. 47		* -•		3
:	1	ċ		1.57	•	.	2. S	•	٠	-	-	. 20	20	P
10- 610		0.0	~		~	7.		24.		•5•		20.5	20.	~
1	1	7,1	٠,	254,40	3	1.4		3				C	3	\sim
		7.07	5,30	143.61	-1088.65	-1.44	-1.13	2	20.	97.		20.	20	020
		61.3	•	77	Œ	?	-	3				~ 0 *	C	5
		7	~	*1.67°	3		-	24.		•		· - 20•	C	5
110 011	~~~	0.0	6.69	5.5	¥.	•	62.	5.9	•	Æ		603	.03	~
i		7.1	•	055.	965.48	2,05	45	63,44	1.07	09		60	03	.075
		7.71	6.0	3.	0.0	٠	57.	3.4	•	S		20.	.03	7
		2.13	6.00	474.5	L • 1	٥	. 45	2.5	3	4		.03	.03	£
i		3 t t V	0	5.175	~	٥	1 45	0	°.		,	.03	- 603	Ð
12- 812	7.	•	κ.		-43.35	٠.		5.5		*	•		.03	•
į		•	۳.	-	٤.			5.5	1.1	~		0	60.	^
		7 7 7	-270,34	891.77	238.60	.1.00	.51	85.24	-1.11	38		.03	0.0	.071
		•	× .	-	Ĵ,	•		2.2		₹.			۴u.	^
	-	•	~	•	Ž.	~ •		Š	<u>-</u>	3		£0.	- 03	5
01- 802	148- 1	•	-		4.2	-	2	٨.	° 0	. 47		*0	0	- 3
			-		3.7	-	~	2.1	90	•		90	9 C	•
		77.	7.14	05°C	53.75	57.	.,22	-2.19	90.	• 50		90.	90.	.023
		•	-		7.5	~	7	7.	9 0.	7.		•	60.	C
			•		:		•							

N...a

81 10/05/76 PAGE 11.00. NAVY - ACHR PLATFINMS - FATIGUE ANALYSIS - PLM 105.0 FEET LCAD CUMUITIUM NUL

0.14 ×3.450×0.75		# # # # # # # # # # # # # # # # # # #	FURCE FX FX	ACTENT A T T T T T T T T T T T T T T T T T T	MUNENT 7.2 1%=4.1PS	A PARA E STATE OF THE STATE OF	FUNCE FA	TOTAL DO	AXIAL BTHESS	GENCING WIREGO Y X * Electer Resolu-	SHEAR	STRESS STRESS	COHS. CNITY CHECK:	
-002 0	-	0.0	-05.74	-130.17	-78.70 -52.82	. 26	\$ 17 \$ 17 \$	-,21	-2.25	98.	# 0 0 \$ 0	9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	.186	
		8.42	-85.75	92.98	-	!~	\~	Ž	2.5	N			•	1
		# to .7	-05.76	50.70	•	∹	• 15	٧.	2,5	m (10.		
		9,00		70.0	44,42	⊃ .	7	4	Z. Z	Ň		. 603	\$	
05 100	~ •	0.0	2.37	40.4	•	S.	•	90.	~		60	60.	70	
1		5.7	2.37	50.6	_	٧,	್ಟಿ	9	v		- 050	Ç	•	
		11.0	2.37	1,57	Š	Э,	0	0	~	ä	.01	• 01	20	
	'	~ ^	2.37	17°	2.79		20.	9 3	2	• 6	\$0.		.013	
1			(43)	77.	3	Λ.	•	00	v		010	- 10	3	!
800 146	0	0.0	-14.50	-0.74		3.	.17	~	3		113	.13	•	
		5.7	-14.51	3,05	1.96	٥	-11	2	90.	٩.	10	- 110 -	2	
		•	-14.53	13.84	C	٧.	.15	۲,		۹.	.01	.07	c	
	-	17.1	• = :	55.09	· '	NO.	=;	5,42		.63	50.	50	.075	
İ		•	95.71	20,02	62.75	•	90.	٧.	00	·.	70*	_ 101 _	-	
800 146		0.0	- 32	-15.00		56.0		3.1	24.	.57	90	90	4	
	1	>,7	0	66.5.	_	-, 35	12	3.1	3		90	90	20	
		11.4	8.95	11.51	12,40	2,15		-3.12	246	~	•0•	90.	0.00	
	-	17.1	0	30.58	S	\$6.35	.	3.1	. 42	•	.07	10.	3	
		66.8	8.95	51.01	£	-, 35			3		70 •	20.	€.	1
901 200	~	0.0	20.07	141.65	۰	2	80	•	~	1.31	9.	71.	_	
		14.9	20.05	17.04	-78.40	•	ŝ		•	7	0	0	·m	
		8.63	50.00	-42.55		95.		9.55	1,32	10.	30	30	660	! !
	-	1.04	20.06	-34.60	-67.31	٠.		ŝ	٠.	. 4.5	90	90.	07	
ļ		54.5	\$0.05	27.01	10.5	~	S	Š	٦.	0	-	-12	C ₁	1
906 JLB	1 - 0	0.0	37.0	133,55	٠.	ζ.	2.3	5.0	~	-		-	•	
	İ		37.	676.00	159,98	11.11		153.03	200	04.	13	115	101	
		15.6		258.29	<u> </u>	•	51.6	2.0	•			_	2	
	-	٠. د د د د	150.47	70°77	1/8,30	9 4	7.5	o :	•	529		2:	0	
1					-1			•	•	***		SI	2	1
016	2- 1	0.0	5,36	02.84-	c	-2.45	•	7.7	20.	.37	03	.03	5	
		1.0	5,36	-110.35		-	•	7.	3		£ 0.	0.	5	
		10.2	5,30	-172.50	S	3	79.	-24.93	9	.16	.03	.03	600	i I
	•	24,3	5,36	-234.65	1.6	3	٠	7.7			.03	.03	S	
		32.4	5.36	-596,60	77.**	* 4.5	•	3	•		60	.03	Ö	
= =	۷- ۱	0.0	209,94	66.076-	~	•	4.2	4.3	•		50.	5 0.	£	
			209.94	-551.54	105.00	•	5.4	2 0 1	2	\sim	. 05	905	5	
		10.2	30000	-122.10	-04.16	1,42	4,61	64.53	1.07	90.	.05	\$00	950.	
	•	٠,٠	30.00	287.35	7	•	2 .		?		\$0°	\$0.	S	
	•	75.4	750,04	20,000	4		_	•	•			•	,	

&

THE PERSON OF A STATE AND STATE

PAGE U.S. NAVY - ACAR PLATFURMS - FATTOUE ANALYSIS - HLM 105,0 FEET LUAD CUNDITION NO.

MENREN - GRUUP		FURCE	RUMENT	MUKENT /	SHEAK F	UNCE/	TUKSIUN		2	18 SE	SIS L	¥	1 B L
NUMBER AND	C V I					74	Ħ	THESS	~	81	38 ST#	ESS UN	UNITY
34614	• • •	AIVS	241 X=21	INORIPB	201 X	RAIN	INSKIPS		X	3II8		•	F.C.
12- 912 -2- 1	0.0	-279.33	977.45	520.51	.15	-3.69	5.4	1.1	94.	50.		•	0
ı		-270,35	914.00			-3.54	85.46	-1.11	.33	80	40	•	040
	10.6	6/2-	80.065	_	51.	19.5.	5.4	1.1	.,23	\$0.	•	•	ç
	Z4.3		-96.65	77.	51.	-3.69	š	1:1	••20	\$0.	•	•	9
	34.4	-5/0.3	-457.79	463.70	-	49.50	5.4	1.1	•	50	•	-,	9
1 -405 104 - 10	0	.0.10	55.04	62.21	77.	~	3	. 58	€.	50.		•	•
	2	0 - 0	20.53	94.50	-	2	•	. 58	. `		•	•	•
	15.7	• • • •	9.44	40.59				95.			•	•	047
	40.0	91.6	-7.32	4	Ð	٦.	•	58	٠.	90	•	•	•
	47.4	•0.16	-10.03	-11.20	∵	11.	3	- 38		•			S.
901 194 I	0.0	-65.11	913,54	85.48	9	9	-	5	•		,	•	9
i	•	25.1	-12.14	,	7	20.	-	5	•	56	• •	• •	0
	115.7	-65.14	-10.05		· 3	.0	-/.10	50.	• . 30	0		•	087
	20.6	-43.15	24.3	•		₹0.	-	54.	•	-	•	•	0
	47.5	-43.17	-0.54	-74.13	643	÷0.5		34.	•	_	115	•	0
01-1001 JLW- 1	5	3	-81.57	10.02	2.54	60.	-74.52	10.	51.	_		•	ò
	8	•	-60.35		1.16	.17	79.5	5	~	100	•	•	6
	16.2	•	01.10		. 10	.24	-74.52	3	. 25				011
	¿4.3	7.	-21.05		-1.51	92.	79.5	10.	•10	•	•	•	001
	36.4	7.	6.57	62,37	-2.46	62.	79.5	.01	90.	51.		-	0
11-1002 180- 1	0 • 0	37,54	45.27	-19,15	٥	•	э. 9	1.57	₹45	60	•	•	0.91
	10.6	57.60	~	40.45	~	21	3.	1.57	1	90	•	•	073
	•	19,75	16.01=	48,48	.12	70.	00.0	1.37	. 43	3°	90		0.41
	31.7	37.62	٥	12,21	3	•15	8.0	1,37	.11	.00	•	•	0,48
	42.2	٠.	27.59	-63,72	-	.34	۵. ت	1,37	₽.	8		,	990
901-1004 180- 1	0.0	20.00	464.85	-34.36		-	5.0	7.	7	00			0
	10.6	7.07-	4.57	3	4	~	5.6	1.4	٣.	20	! !	,	c
	41.1	6 0 7	11.15	1	Э.	ا ن	د د	3.	3	50°	•	•	2
	42.2	10.011	14.0	C2* C2	207	12.1	15.40 15.40	1. 6	- 0 4 · ·		000	• •	114
				M.	η	. ()	•				
1 -407 104 - 7		20.70	71.01.	7 7 7 E	•	> <	•		•	70.	•	•	.
		7.0	•	•		> C	? '		•	60		•	9 5
		7.70	• •	• 1	• •	•			•		•	•	א סכ
	67.4	-7.53		12,37	. 29	.21	5.39	. 31	-, 15	0	05	· 	029
905- 904 109- 1		•	87.2	3	, 3	• 00	3	0		# C		•	•
		•	05.50	٠.		0		20.		10		•	•
	13.7		24.24	11.17	20.	30.	1.87	70.	60.	0	0.0	•	CO
	40.0	•	2.35	Ĵ	•	10.	2	~ 0 •	90.	•	•	•	9
											•		

STRAN TERBER UFTAIL PEPURI

	1910										>	٠		
MEMBER GROOM	!	FUHCE	HUBERT	MUMENT	FAKF	UNCE/	TURBION	XIX	OING	STHESS	BHEAR	E.	- 2	
UA	1. NO	*	¥		>	74	X	x	>	~	814ESS		UNITY	
2 2 3 3 6	- -	E	94 X X Y Y	SALVENI	DOTX .	SAIR	SATY-NI			X 0 X		/	CHEC	,
1 -601 506 -20	0.0	~	s	•	•	0	•	-	•		00	60.	ູ	
	0.0	15.50	14.60	1001	27.	20	93	.19.	14		- 05	50	• 010	!
	13.7	~	-2.20	~	•		٠.	-	•		* 0 *	20.	20	
	2 0.6	-	• . 56	2.5	٤.		٠.	٦.	•		50.	• 05	5	
	47.4	-	1.15	-25.05	77.		~	-	•		60	00	0	
U3- 915 109- 1	0 0	3	-10.50	-59.62	7	-	20	•				0.0	0	
,	2	₹		.27.51		9	. 2	•				0	0.7 %	
	15.7	03.05	-45.52	70.71	.15	10.	-1.63	1.45	00		20	20	071	
	40.0	3	-41.47	-2.hB	~	0	₹.	•				0.0	0	
	" 47 . u _		-15.58	9.64	₹.	-	•	•				03	0	1
05-1002 180-1	0,0	25.43	00.44	44.24	×	-	1	-	4			4	-	
	10.0	- 5H . 31	54.5	1207	3	12	4.21	95.19	4					
	-	.54.27	27:1	51.53	50.	0	~	1.3	, 3		20	- 20	0	:
	51.7	#54.24	C#*C=	-CH.30	7	-	N	2.5	٠,		50	0.0	0	
	~	-54.20	-27.19	45,57	~	2	~	1.5	3		90	900	10	1
	5	7	31	•	Ī	•	đ	•	٠			•		
) + • T	0 0 × 1	07			70 .	9 4	200	0 0		- 6	2.0		
	15.2	25.60	57.7	95.6	•	91.		-	. 0			50	:0	1
	•	** . A .	21.75	1.40		Š		7	c			0	. •	
***************************************	٧.	~	101.47	-21.17		1.08	30	7	•			90	0	1
	c	1	24 . 6 -	100	•	U	٥	J			•	4		
	9 9	2 C C C C C C C C C C C C C C C C C C C				5 10	7		10.			0 4	o d	
	41.1	-00.05	15.54	1.23		0	. ~		: -:		1	70	?	i
		-04.61	6.51	5.75	•	~	~	. S	٠.		50	50	2	
	•	-64.40	-40,55	13,39		S.	~	2,5	.		700	10	163	
1 1001 200 100	0.0	9	7 0 1	46.010	•	0		-	4		•	5	, F	
		95.1	5,45	4.29		20	70	11	9		90	9	015	
	15,7	٠.	1.53	11.52		0		-	•		20	20	٠ م	,
	40.4	9	70.	1.84		0	10.		C		90	• 05	5	
	3.12	•	1.76	-54,76		•	-	~	æ,		7 90 1	- 00	3	!
1 -401 000 -00	0	20.02-	-7.54	-59.17	•		80	3	•		60	60	102	
	3	7.7	1.01	-7.00		-	3	3	•		0.	70	0	!
	15.7	50.07-	11.60	24.27	• • 66	11.	5.41	-1.00	•• 30		90	•	.087	
	0 0 V	7. T.	٠.	56.47	•	-	9	3	7.		70.	80	700.	
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	,	97.77	30.10	67.70			Ð.	.	3		500	501	•	
05- 406 164- 1	0.0	27.01	-13.51	-54.17		.13	7.		9 2		90		0	
		47.61	45.	-13.97		5	3	-	-		- 04 -		3	
	15.7	27.61	10.47	10.23	67.	52.	77.	1.13	25.		9	90	.062	
	0 :	14.77	3.0	24.24	•	92.	7	-	r		C		ò	
	•			: 1			;	•	١,) ; > (- 1	

;

TAN ARESER OFTAIL REPORT

20	HUMENT AV AV							,	•	
CONTRICT O CONTRICTO O CONTRICT O CONTRICTO O CONTRICTO O CONTRICT					٠				, :	2
00-1006 180-1 000 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		- a	X	2 4 2 4 3 1 4		STRESS	7 2 X X X X X X X X X X X X X X X X X X	7 50 1	STUESS	
00-1005 100-1 100-5 4 100-1 100-5 10	0) *					_	-	3
00-1005 100-1 000 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			3		60	Š	23	9		5
00-1005 160-1 000 011 1000 011 010 011 010 011 011	.\$.	べ・クコ	3.	0	Э.	ţ	3	00.		00
00-1005 18C-1 1 00.0 01.1 1 00.0 01.1 1 00.0 01.1 1 00.0 1 00.1 1 00.0 1 00.1 1 00.0 1	23.60 23.60	22.43	. 75	. 29	000	20.00	47	90	90	078
20=1000 JL9= 1 C O O V X X C C C C C C C C C C C C C C C C C	75	15	61.0	5	100	35	¥.	. e	9	-
21.7 68.4 68.4 68.4 68.4 68.4 68.4 68.4 68.4	•	707		Š	•	'n	3			• ~
51.7 68.4 44.2 68.4 10.0 7.8 10.2 7.7 24.3 7.7 54.4 7.7	-	2.0	•	0	7	S	100	0	•	2
05=1000 JL9= 1 0 0 0 7 K	9	14.1	50.	56	36.46	2,50	90		70	
00=1000 JL9= 1 0.0 7.8 10.2 7.7 24.3 7.7 56.4 7.7	71.40	•	•	•	ż	Ţ.	œ.	- 00		
10.2 7.7 24.3 7.7 56.4 7.7		7.5	~:	Š	7.5	-	.22	=)
10.2 7.7 24.3 7.7 36.4 7.7	65.0	100.44	54	15.21	47,58	=	.27	.07	0.	10
24.5 7.7 36.4 7.7	7	207	7	0	5.	-	S	70		3
	95	٠ •	- r	•	٠, د د	→ •	.17	•		
		2.0	•	J V	, e	-	-	111		>
.0 5.3	242	131,	٥	1,4	24.9				50.	5
4.1 5.3	124	574.7	٩	1 0 4	54.5	>	•		50.	20
5.3		3 .	٠	7 ·	5	9	7 (\$0°	5
55.35 56.4 5.35	967-	1 3 2 1 2	50.0	11.00	00.50	200	13		0.0	000
			•			,			· ;	. 1
	0 7 7 7		• 4	•		•	, 4	9 0		5 5
2	U.040-	-350.95	41.0	7,00	64.56	1.07	. 52	00	90	.063
\$ 209.	Đ	3.5		٥.	4.5	٦.	0	80		O
2.4 209.	697.6	c C	4	0		٥.	. 35	80.		
70.5	1855.14	7	•	5.9	5.4	-	€.	10.	.07	6
.1 -2/9.5	1245.1	0 . 1	٦,	•	3,4	7 . 7	Š	0	100	_
5.6 -219.3	104.1	404.0	٦.	5,0	2.4	1.1	^	0	.07	07
\$6.9/5= 6.25 \$6.9/5= 2.54	123.20	1400.70	0 0 0 0 1 1	5.97	85.46 85.46		0.50	0.07	• 0 • 0 • 0 • 0 • 0 • 0 • 0 • 0 • 0 • 0	400.
	4	9	•		7		, 7		•	:
	7 03			``	. 3		9	, c	, c	::
6.0 -51.1		51.69			67.7	-1.54	30	10		0
.0 -51.1	-12.7	7.	3	~	7	1.5	-	, C	C	2
, n ~ >	-59.45	5.4	. 70	~	3	1.5	۲.	0	O	-
A. A.	-68,5	1.7	٤.	36.	٠	٧.			0	5
8.0 48.5	-45.0	1,5	>	V.	~	٧.	3	0	0	.077
₹ :	-54.	55.54	۶۶.	37.	12.50	1.67	57.	S c.	\$0.	01
	• ;		n 1	***	?"	•		0 0	0 4	•

Beered Booodsood Selection of the Selection Conference Construction

			- A - B - C	1 KL14 •	TAT D DERUTIA.	IGUE AMALY		103.0 PE	-				
1	LIST			1		;	į				•	7	
SPECIAL CROOM	F E C 1	TORUE TORUE	HOMENT	MUMENT	AK	UKCE/	TUKSION		HENDING 8	TRE 88	SHEAR	3 (60 (
S		A I V	BOLKEN	SdIW-NI	SOLX	8214	INSKIPS	- ;	-	, , , , ,	4	7	CMECA
1 -002 5001-200		14,	1 5.00	£	55.	•	4,41	3	-		80	C	_
	9	•	10		•	7	61	0.5		1	0.0	20	00
-	16.0	10.	-14.57		2	•	14.5	, ,	. ~		9	90	3
	C # 7	70.	•25.76	53,34	.17	• 14	-19.56	. 62	.24		.01	.07	.011
!	- 25.0	-14.	.30.44	~	3	-	14.5	>	2		90.	60.	 :
202-1004 140- 1	0 • 0	.12	-40.75	S	2	.24	20	. 0.			0	60	-
	0.0	51.	-14.74	3	20	121		Э			60	60	5
	C	.12	1.47	•.20	o • •	150	99.0	.01	.02		00	60	100
	÷,		55.69	-	00.	, 25	₽.				•0•	0	5
	76.0	. 12	45.69	0	•		20	.01	AL		- 60 -	60	2
002-1005 140- 1	0.0	-3.47	-34.08	-21.74		•	5.5		70		10.	.07	7
	20	-3.40	-<0.40	3.4	-		5	- 42	. "		60	50	
	16.0	-3.45	-1.72	11.02	5.	.13	-2.53		26		00	0.0)
	0.77	.3.44	•	~	-		2.5		-		50.	0.	5
1	26,0	-3.45	17.65	-20,17	~	-	2. 5	•	.5		- 10	10.	03
1 -002 5001-1001	0.0	52.55	-46.54	4	~	3	•	1.39	£		50.	.03	6
	0.0	\$4,56	\$0.05	0	7	100	3	1.50	7		0.03	0.3	
	10.0	55.55	.10.74	-42.57	27*-	17.	1.08	1.58	07.		.03	50.	.071
	0.42	52.55	25.15	ີ	٧.	77.	•	1.53	-		0	. n 3	9
	_ 5<.0 _	\$\$, 5\$	63.05	3	7	19.	•	1.38	m		.03	0	4
004-1005 140- 1	0.0	3.46	24.45	-14.24	•	0	4	~	•			90	ر س
	8.0	3,40	15.70	3.50	41.	٥,	•	27.	30			96	~
	10.0	3.40	16.0	10,46	. 61	• 0 •	•	27.	• ≥ 4		50	• 05	050
	9	•	φ.	•	.13	2 (•	42	50.			0.	~
!	0.56	•	16.03	#66.33	133	.	•	V	93.			90	m
1004-1006 200- 1	0.0	-7.59	*34.77	-27.27	•	.23	3	~	~		96.	90	~
	2	7.61	-14./1	_	~	,25	Š	v	7		50.	٠٥,	9
	0.0	54.7.	. 95°4	•	3	, 25	v.	٧.	2		• 0	• 0 •	9
	2	-7.64	31.42	28.75	77.	٠ د د د د د د	64.55	• 50	• • •		40.	70.	• 024
	36.0	7.40	53.49	•	\$5,	.25	'n.	٧	~	,	90.	90	
005-1006 400- 1	0.0	-41.53	-57.5B	N	•	• 30	۶.	1.0	•		.03		T.
1	2 E	÷	-2.76	٥.		. 3b	•) ·			C		7
	70.0	ę.	36.05	3 0 ·	1>	• 30	1.95	-1.09	21		.03	.03	.086
	7	•	Đ.	3	•	• 36	•	7:0	•		£ 0.		60
	24.0		101.07	٠.	•	9	0	2	44		-		



孤

RAN TRIBER URTAIL BEFORT

450000 00000 00000 00000 20000 30300 22000 86388 00000 N N N O N NW NO V 55555 55555 20000 Numer verse cocc cocc numer verse numer verse serve 24342 22244 22222 2222 24342 2244 22222 2222 20000 00000 20000 00000 coupo conou canac coupo coupo 0 4 6 0 4 6 0 SECTA

PACAMA JEANNO SESTINA SANCO

			U.S. NAV	4 - ACHH PL	ATFUMMO - FA	TIGUE ANAL	1818 - MLH	105.0 FE	E1				
ADDRO NUMBER	## # # # # # # # # # # # # # # # # # #	FURCE	HUMENT	HUMENT		URCE	TUKSION	AXIAL	BENDING	STRESS		SHEAR	70
) 1 1 1 1 1	8214	Selveri	Sdly-NI -	Balk	Salv	861 X=7.1	# F	>	Z K81	81 RF 88	# E	Car Car
1044 105 HOBE 1	•	•	70.	0	.	0	9	• ·	0	Э.	00	00.	0
	7.5		000	00	2 2	• •	00	2,7	9 0	000	90	00	00
	2 10 10 10 10 10 10 10 10 10 10 10 10 10	0	9 5	3 4	000			9 9					0
* 1 * 1 * 1 * 1 * 1 * 1 * 1 * 1 * 1 * 1	•	•	•	Š-	•	•	>	?	•	>	9	>	>
104- 106 #16- 1	0.4	20.	၁ :	\$2	9:	0	3 :	0 :	0	9 (0		00
	7.3		50	3 .	000	000	? ?	>		• •		000	0 0
	•	0	၁ :	~ ∶	0	00	00.	00	0	• 03	0	0	.001
	6.9		404	3	0.0	70.	•	•	C	٠.		- 000	9
105- 106 m18- 1	•	30.	.01	0	0	•	00.	00.	•	0	8.	00	0
		0 0	<u>ء</u> -	٠.	3 :	ç) (> :	6	3	000	0	0 0
	10.01			- ^			>	9 0	o c	• •	9 6	-	9 6
	•	30	~	.37	000	20	00	, ,	30	0.0		20	700
106- 200 DAL- 1	•		22.	N	2	•	-	-	0		00	0	0
· .	8• E	0	~	-				8	0		00	0	3
	ᅷ.	0	ⅎ.	-	•	9	3	Э:	0		00.	0	00
	15.0	000	70.	9 0	9 9		1.50				000	000	000
	•	•					•	. '		i . I			. '
1 - 01 × 02 - 102			20.0	10.1			000		0 0		٠ و د	000	500
		-	ζη.	٠	3	0	. •	2		•	0	30	•
	10.9	Ξ.	60.	C	•		0		0	0	00	0	.001
	•	\$1.	\$ 0.	~ i	•		0	<u>ء</u>		- 05	0	0	0
201- 204 m16- 1		0	.17	Ð	•	•	•	٠,	00.	3		00.	Ö
	2.	਼	910	23.	20.	000		•	0	- 0 d	0		0
	10.9		20	~ 0	•	• •	• 0	•	> C	•	> c	> c	9 0
	,	•	¬	42,	•	00	00	-	8	3	00	00	001
201- 501 DKL- 1	0.0	70.	-1.70	~			5.3	•	c		0	0	٥
	•	0	•	3.7	-	3	5.5	2	. •			0	3
	ᅷ.	ç	Λ.	0	⊸ .	0	٠. د	? :	0		0	0	0
	15.0	1 1	1.00	-14.63	7	100	\$5.C.				ē.	0	000
; 	•	•	•	•	•	, ,		•	; =		•	•	•
201- 308 140- 1	0 £	0 0	\$ 2	•1.52	3 7			99	7 000		0.0	0.0	.001
					2 3	200	72.	00	. c		2 6		9 0
	, 3	, c	• •	_	• •	•	• ^	000	: c			> 4) (
	•	•				Þ)	•	•		2	2	:



TRAN MERRER DETAIL REPORT

V 10000 THEME STREET STR 100000 NO-NA 24.00 22240 2222 ##### ##### COCCC COCCC COCCC 0000 0 0 0 0 0 0.0 SKOUY A 10 SKOTS

Ü

TRAN RESORR DETAIL REPORT



TACAR AMERIKA ORTANI AMERIKA

C 1 1 4 000 2000 910 .010 0000 020 2.70 25222 00000 00000 00000 20000 20000 22222 22222 56000 50000 5555 20000 00000 BENDING BIRESS 20000 2000 10000 20000 W 0 0 0 C 00000 00000 - FATIGUE ANALYSIS - MLW 105,0 FEE 1 1 1 1 1 20222 00000 22222 135.24 17.17.19.00 17.17.19.00 17.19.00 10.00 10. Jan S 0000 22.22 77.1 0000 0000 2 2 2 2 2 00000 2000 0 0 0 0 0 0 0 V 2 2 2 2 2 2000 0 7 7 7 7 3 3 3 3 3 1.0. NAVY - ACHN PLATFORMS 13.05 13.05 13.05 13.05 44.45 44.55 44.56 87.16 121.03 - WE . 97 - 61 . 65 - 62 . 72 - 63 . 74 - 64 . 74 16.00 155.00 167.93 63.74 73.73 65.77 93.70 1000 1 1 E E 1 7 7 7 7 7 2000 6 E M = 0 Prot GRUUK AND BROTA 400 DKL-= 2 201 510 511 403T

=										3	•	
5 🚡	INTERIOR WITH	MOMENT	MIMEN	AV	611KL 6	TOPRION	AXTAL	S JULUN SH		- i -	7	THE STATE OF
. Ā	, K			X	74) • ×	STRESS	} } }	2	STRESS	STRESS	C≥1 T ₹
₹,	7. A1F9	SALXENI	INSKIPS	Pa I x	K1 P.9	IN-KIPS			·-K SI		•	CHEC
_	.0 2.	~		٧.	•	•	87.				0	~
,	8.5 8.	-	~!	•	•	•	83.				- 20.	
÷	•		٠. د	•	•	•	Э:	0 (20.	0 0
	5.1		14.72	97.	10	1.09	83	13		000	- 02 -	000
	5	*	1	_	7	9	=	•		٠ ؤ	4	•
		7.10	.		. 4	5	, =	> C				: c
		35	· C	• ~			50	1		90	90	300
•	7	7.9		4.1	7	65.6	0	0		40	90	0
	1 7	110.7		3	7	Š)	0		90	90	· C
_	7.5. 0.	15.7	2	-	0	~	•	-		60	60	_
_,	5.1 -2.71	12,05	4.5	100	0.0	. 7	0	0.0		20	20	, c
_	.2 -2.7	10.5	S	-	0		•	•		20	05	. 0
-	.3 -2.7		7		0	7	•	•		000	60	· C
ũ	-2.7	9.0	T	.18	.03	3,25		9		- 85	- 05	010
_	0 -2.7	7-7	·S.		10	-	9	01.0			C	0
•	. N2.7	3.5	7	-		7	2	•			0	0
	٠.	•	-1.70	.14	.01	•.15		•		5	.01	.007
- -	7.7		£ (3 :		~	<u>،</u>	9 ·				0
	• 7	*			10.	•	•	•			100	~
	0	4	•	20°	0		•	•			90.	0
	0	7.	/ H 6	50.	•		2	0			. 00.	0
	•		21.	~ ?		3 ·	9:	00.		8	o •	100.
-			c =	V (•		•	•			3 (0 (
•	,		2	20.	•		•	•			000	_
_	7. 0.		.17	.	00.	~	40.	2 0 °			00	0
	• · · · · · · · · · · · · · · · · · · ·		- 2n	•	0	∹	906	0			0	0
	0:		e t	• :	٠ •	7.	9	0			0	0
-	5.2	121	22.1			51.	3 3	30		00		000
_	4	5		=		J		-	٠.		<	
		2.00	7.95	50	0.5	95.		200				000
	T	1.1		2	0	``	-	°.		0.	10	. 0
	-	•		Э	70°-	S.	9	٥.		0	0	0
-	.1.	7	151	Э.	•	÷	-	.		100	10	0
_	P. B. O.	48.3	۰,	•	70.	0.1	.62	3 C		50.	50.	1
1	.S 64.9	D	٥.	•	20	4.0	ø	0		90	90	03
	0	A 9 7	-52.04	1.05	₹0.	70.13	.62	70.		50.	\$0.	080
	0.00	3	<u>ء</u> •	٥	₹ 0.		. 62	50.		50.	50.	m
-	0.00	50.55	10 \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	4	•	•	•			,	•	

AN KRESEK OFFAIL KRPOR

T.

STREETS CETAIL REPORT

## 71 1.65 24 24 24 24 24 24 24 2														
712 YI 1 0.0 04.71 1.255.44 100.01 750.02 10.0 10.0 10.0 10.0 10.0 10.0 10.0	!	0151				:		- 1	!		i	>	7	;
25 July 1 0.0 0 04.71 1.05.34 0.00.35 0.00.3	 	F ()	FUNCE	MOMENT	7	ATENTER	UKCE	10	XIAL	N N N	STRESS	SHEAR	SHEAK	5
1	SECT		8 A I Y	INNETERS	A I Y N	7	11	X M X = X	- 700		IS X		1 L	CHEC
25 Jules 1 0.0	712 71-		3	54.54	8.540	~	٠	40.	07	40		10	-	=
1	·		· *.	-125,54	9.04	7	a :	19.0	0.7	0.0		0.0	0	• >
1		14.7	H . 7	-166.50	-16.3	7	Ð	14.0	. 40	6 0 •		0	0	•
1		0°57	۲. ۲.	-514,47	3.9	i, i	£ 5	19.6	3 3	51. 51.				~ ~
						•				! 		•	•	, :
	1 061 360) ·	? *	V :	12.4	` .	7.	100.		0		0 (e :	
\$\begin{array}{c} \text{3.} & \text{2.6} & \text{3.} & \text{2.6} & \text{3.} & \text{3.} & \text{3.6} & \tex			٠.	70.02	777	` '	-	7 001	20	-		0 0		
5 = 623 JL6 = 1 0.0 08.29 J9.81 = 606.17 1.36 .20 .20 .85.26 .60 .60 .20 .20 .20 .20 .20 .20 .20 .20 .20 .2			٠,	-97.73	0.5.4	1.7		106.3		1 2 4 5		0	90	
2- 023 JL6- 1 0.0 0 08.29		1.0	~	-108.50	36,4	-	1-1	106,5	50	10		96	O	3
	5- 623 JL6-	•	ζ.	¥.	-	-	~	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	•	•		C	C	70
0		•	1 1	2.5	0				٥			1		
Column C			2.4	7.6	3		ľ	5.2	•	. 0		, 0	• 0	0
6			Z . H	3	7.0		~	5.6	•			2	·c	50
		•	¥.		5.0	~	N	5.6	Ð	-			- 60	0.3
1	6- 626 JL6-		9.00		41.	19	1.7	,	4	c		0	C	2
** ** ** ** ** ** ** ** ** ** ** ** **			44.4			•	1.7	7	٥	. :		0	0	9
# 051 JLo* 1 0.0 7.31 = 107.44			99			~	1:7	-	٠,	===		500	. 03	0.3
- 051 JLo* 1 0.0 7.31 -107.44 24.04 -1.70 -1.12 -100.54 .0 0 1.15 7.32 -107.44 24.07 -1.10 -1.12 -100.54 .0 0 1.27.44 25.02 -1.10 -1.10 -1.10 -1.10 -1.00.54 .0 0 1.00 1.00 1.00 1.00 1.00 1.00 1.0		•	94.4		•	V	1.6	~	•	٣.		0	• 03	.03
- 051 JLos 1 0.0 7.31 -107.44 255.02 -1.10 -108.54 .0 4			84.5		•	-		_	E	~		0	0	°
1.5 7.31 = 127.88	- 051 Jlo-	•	~	107.	æ	1.7	1.1	106.5	3	~		9 0 •	0	•
2- 70 5 200-1 0 0 1 -2 71		•	~	127.	3	₹ ₹	1.	100.5	3	•			90	70.
2= 703 200= 1 0.0 =2.71		•	~.	0 . F	٠,	۲.	~ .	100,5	၁ :	_		. O.	50.	.0
2= 703 200= 1 0.0 =2.71		•	•	10/01	٠,	•	•		> 0				,	
2- 703 200- 1 0.0 -2.71		•	•		-	J:	•		60			- en -	>	
5.4	-002 501 -2	•	2.7	9	28.3	-	0	5	-	~		₹0.	20.	.0.
10.9 = 2.70 = 5.44		•	2.7	~	C . 9 .	3.	0	J.	.	2		01	0	Э
5		.		7	0. 0.	Y	٠.	٠.	• :	٦,		5 0	50	3
S= 653 JL6* 1 0.0 UM,29 55.44 *165.25 1.49 *33 85.54 *0 1.5 UM,29 61.54 *10.12 *24 85.54 *0 2.0 UM,20 *24 85.54 *0 4.7 UM,20 *0 85.54 *0 4.7 UM,20 *0 85.54 *0 4.7 UM,20 *0 85.54 *0 4.7 UM,20 *0 *0 *0 4.5 UM,20 *0 *0 *0 4.5 UM,50 *0 *0 *0		• -	. v	7.0		֡֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֡֓֓֓֓֡֓֓֡֓֡		ָי יַ	? ?			# 4 C O	9 0	90
1.5 0.7 20.0 1 0.0 0 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0			1			. 7	. *	<u>ن</u> ا	, 1	:			, ,	
4.5 0 00.25		•		•	7	•	, .		D 4	-		^ 4	> 0	• ·
4.5 08.15 64.45 -233.04 1.0208 85.54 .6 64.85 64.85 64.85 85.54 .6 64.85 64.85 64.85 85.84 85.85 8.11 -5.40 8.1		• •	. E	. יי	- ~	13	1 ~		9	71		100		> 0
4- 701 200- 1 0.0 -4.51 -17.84 39.48 -32 -11 -5.40 -1			9.1	3	0	ે.	0	3	٥	-		30	70	0.3
4- 701.200- 1 0.0 -4.51 -17.84 39.483211 -5.401		•	, K	Ð	£	~	7	5.5	70			0.0	0	0
5.5 -4.50 -16.68 50.3300 .07 -5.401	4- 701 -200-	0	3	-17,84	7 0	~	7	5.	-	~		0.0	.03	.01
		5.5	7	*16.68	6.3	?	0	5.4	~			0.0	C	0
*4.50 *9.40 *5. \$6. \$9.40 *1.		11.0		. V. KB	± .	٦.	~ ∙	. t	٦.	23		90.	• 04	• 01
1 - 07 - 5 - 79 - 5 - 5 - 5 - 5 - 5 - 5 - 5 - 5 - 5 -		20.5		\$ 3 ° 6 ° 1	2	٥	~	2.4	٦.	ç		6	9	9
		`	•			1	77		•	•) (



, . \·

) 1 1 1 1	1	1810		4 7 Maria							>	7		
	0 P. ◀		5 🖢		7 7 7 1		74	N N N N N N N N N N N N N N N N N N N	STATE OF	2	016 P. 1	STRES		
:	SEC To		ATPS	SdI N=NI	INEKIPS	*IPS	KIPS	IN-KIPS						
625- 706	200 - 1	•	6.43	-43.11	£	•	1	~	-	~	£0.	0	3	
		5,5	٤.	3	-3.6U	90	90	3,30	=	30	0	10	021	
		-	6.01	*35,15	~	. ၁	S	•	-	-	0	0	3	
			18.4	15.04	11.0	>	٠.	٠.	-		•	00	-0	
1	i	-	1	90.18	۷.	3	•	~	-	€.	0	0	03	
127- 650	J.6. 1	•	-64.57	-217.50	-	~	2	7.1	0		0	0	•	
į	:	•	7.9	-430.07	9.79	7	3	7.7		-		0	3	
!		•	5.40	-648.45	000	3	3	7.7	•	~	10	•	~	
		9	2	25	-51,29	20.	700	17,75	09	•.10	.01	.0.	0.035	
		•	ς.	-244.74	37.h	Ð	~	7 • 7	٠	-		0	M	- 1
651- 701	J.6. 1	•	~	55 5x1=	16.7	~	*	141.1	50.	~	80	0	-	
		7.	7.31	-148.65	221,75	Z 0 2	3	-141.14	50	6	90		010	
		•	·~	-4000-47	54.7	. 3	7	141.1	.05	-	60	0	9	
		•	٣.	-216.05	٥.	3.	7	141,1	Э	-	010	•	00	
		•	~	-225,46	2	A.	. 45	141.	3	-	=	1.	C	
653- 703	11.60 1	0 0	~	10.30	5,6	•		3	•	_		C	-	
	,	•		77,10	0 1 1				•	• -			֓֞֜֜֜֜֜֓֓֓֓֓֜֜֜֜֓֓֓֓֓֓֓֜֜֜֜֓֓֓֓֡֓֜֜֜֓֓֡֓֜֡֓֡֓֡֡֡֓֡֓֡֡֡֡֓֡֡֡֡	
			2 . 7	44.57	2002		: :		5			0	, 14	1
		5.3	42.72	1.92	-145,34	-1.52	* 2 • 2 Z	00.00	30	1.2	0.4		•	
	† †	•	7.2	· •	104.5		~	9	•		101	.07	.035	
652- 706	J.b. 1		50.49	07.00/6	•		3	7 - 7	•	_	6	•	-	
	,		9	07.557	3	-		7	•	•	, r	, c	7 6	
			-00.05	-210.70	12.00	Ç	1.03	17.73	00	13	100	1	350	1
			65	-174.48		7	Э-	7.7	•	7	0	30	0	
:	:	•	•	-124.75	7.	V	3	1.7	•	-	30	50	0.35	
701 - 107	1570		00.4	5	4	2	-07	•	3	7	-	-	4	
		•	000				•	• •	7 3	. 4			· •	
			00.4	-		_	. •	2	. 3	-			030	
		1 4 . 1	30°¥-	37	3.61	87. •	9.46	40.6	27.	99.	. 12	. 12		
!		•	00.5	96.86	~	3	•	9	4	~	-		5	ı
701- 704	13/- 1	0.0	60.	34	£	10.	_	5.	9	-	_	-	-	
		4.7	64.	30.08	3	•	6	5.2	9	~	14	-	9	
		3.5	20.0	-7.35	45.90	14	-,72	.5.24	70.	.21	. 12	. 12	010	
		3	74.	1.70	 		Š	5,6	3		. 11	~	~	
!	1	9.0	74.	40.64	Š	•	~	ۍ د	Э	~		•••	9.5	•
701- 801	JL 7- 1	0.0	-5.16	20.44	0		0	62.3	2	0	27	•	0	
		7.1	-5.17	10,18	259,85	-1.58	12	-62,30	400	53	90	90	910	
		14,2	-5.16		~	•	~	64.3	?	۳,	0	0	\sim	
		۲۱°3	2.50		4 :	 1	٧.	62,3	•	٧.	-	-	-	
		7.	12.5	77.17.	4	•	•						•	

G.

PACETA TATE OF SHEET AND THE

2	######################################
---	--

Ť

STORYS PRESENT DESCRIPTION

a l'assessatification de la compacta

ŧ

i



GTEAN TEARER OFTAIL REPORT

©

STRAN MEMBER OFTAIL MEPORT

10	* *		2 K 2 K 2 K 2 K 2 K 2 K 3 K 3 K 3 K 3 K 3 K 3 K 3 K 3 K 3 K 3		.5 3	A NI N	URCE F.2 F.2 F.1 P.3	TUKBIO BX BX BX BX	X I A L THE SE	ENDING STRES Y Z THE STRES	SHEAR	SHEAK STRES	& ► O
10	12- 412	1 0	7	. 0	287.0		8	7.51.0	•	30			2
10		£	6.7	. 3	208.9	: 7		19.7	M	, -			3
10		•	_	7	2005	7	•	10.7	•	-			20
901		,	۲.	Ţ	252.7	~	•	14.7	~	-		0	0
10		v	4.7	3.00	211.4	~	æ.	14.7	~	-		0	3
10 10 10 10 10 10 10 10	01- 902 169	-		57.0	63.0)	0	3	0	1	705		2
10		•	S	00.4	52.3	, ⊃,	0	3	0	M	95		5
00. 10. 10. 10. 10. 10. 10. 10. 10. 10.		15.7	~	-3.55	20.5	7	0	Ò	0	~	0.0		
1		407	٠.	7	6.5	3.	0	2	9	0	30		00
10		7.7	٠.	٩		.	0	Ď.	2		- 50.		ر د د د
13.7 10.7 10.8	941 904 -10	0	_ C	20	23.5		0	1	3	1	70		٥
10.1	,	٥	_	•	7	2	C	^	3	m	20		20
1,		~	0		6.	, 7	•	^	3	N	.03		0.3
001 10.0 11.0 11.0 2.2 2.2 11.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.		0	C	•	Ŧ.	~	°	۲.	3	C	96.		20
001-1004 10-1 - 24	!		10.48	·.	3,3	Ž,	0	~	3	4	- 60.	c	C O
1	01-1001 JE9	0	^	4	45.0	2	20°	:F	0	-	-		0
905 100 1 100 100 100 100 100 100 100 100		£	N		17.4	7	9	2	3	-	• 0		0
00. 64.5 - 25 - 25.7 196.98 11.9 196.54 10.0 11.5 196.54 10.0 17.5 196.54 10.0 17.5 196.54 10.0 17.5 196.54 10.0 17.5 196.54 19		91	•• 25	7	97.5	7	C	5.0		2	0	0	3
00. 10. 01. 02. 20. 20. 20. 20. 20. 20. 20. 20. 20	÷	•	., 25		46.9	~	•	5.5	•	-	0	0	Š
10	1	~	•• 65	٠.	3 2 o A	v.	•	3.	.	٥.		-	S
901 1004 160- 1 0 0 1 1 2 2 2 2 1 2 2 1 2 2 2 2 2 2 2	01-1002 18U	:	17.5	30.4	¥.	~	~	70	٠	~	C	0	3
00. 50. 17.39		10.5	7.5	Đ	21,5	-	-	2	٥	~	0	c	3
901-1004 18U-1 0.0 11.24 -25.01 33.44 -3.5		41.1		3.4	ک . ۲. ک	3	•	\$	•	~	0	C	70
901=1004 18U= 1 0.0 1 1 2 2 2 2 4 4 5 5 5 5 6 6 5 5 5 6 6 5 5 5 6 6 5 5 5 6 6 6 5 5 5 6 6 6 5 5 5 6 6 6 5 5 6 6 6 5 5 6 6 6 5 5 6 6 6 5 5 6 6 6 5 5 6 6 6 5 5 6 6 6 5 5 6 6 6 5 5 6 6 6 5 5 6 6 6 5 5 6 6 6 5 5 6 6 6 5 6		41.7	M.	7	10.1	٧.	7	30	٠	•	0	0	2
901=1004 180= 1 0.0 1 14.22		. 42	×.	45.8		.	~	ž.	e.	~	\$0.		0.5
902= 903 109= 1 0.001 1.650403050505050303030303030303	U1-1004 1PU	,0	,	۵.	7	∙v.	~	•	٥	100	36.	50.	2
42.2 14.14 = 1.45 = .01		10.6	7.	-5.70	21.1	V	٠.	•	£		C	3	5
51,7 15,16		41.1	÷.	=	37.6	?	0	٠.	0	m	0	C	7
902 902 10.0 . H1	• .	51.7			17.9	4,1	→ ₩	9.1	0 (- 5	0	C (6
902- 903 164- 1 0.0 .41 .42 .55.17 .03 .17 .03 .72 .03 .03 .03 .03 .03 .03 .03 .03 .03 .03		,	•	•	. ·	•	١.	•	•	•	:	2	,
15.7 .01 .05 .03 .17 .03 .15 .03 .02 .03 .03 .02 .02 .02 .03 .03 .15 .03 .02 .02 .02 .02 .03 .15 .03 .15 .03 .15 .03 .15 .03 .15 .03 .15 .03 .15 .03 .15 .03 .15 .03 .15 .03 .15 .03 .15 .03 .03 .03 .03 .03 .03 .03 .03 .03 .03	U2- 905 164	-	3	•	5.1	~	C	1.7	9	~	0	¢	0
15.7 .51 4.04 .05 .10 .05 .17 .03 .15 .05 .05 .05 .05 .05 .05 .05 .05 .05 .0		2.0	ar.	Ď.	٠,	v	9	1.7	∍	•	ٺ	Ç	6
40.5 40.4 10.4 10.5 1.54 .0.5 1.54 .0.5 1.54 .0.5 1.5 .0.5 .0.5 .0.5 .0.5 .0.5 .0.5		15.7		٠	1301	٠,	0	7:1	9		0	c (ဂ် ဝ
905 904 104 1 0.0 - 01 1.54 .01 - 01 1.54 .02 .03 .13 .04 104 104 104 .03 .13 .03 .03 .03 .03 .03 .03 .03 .03 .03 .0		\$ 0 P		•	15.4	•	•		•	-	c o	·	3
90.2 904 109e 1 0.0 = 01 1.54 .01 = 01 = 01 = 01 = 01 0.0 = 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0		67.4		•	£	-	⊋		>	~	•	၁	3
00. 50. 50. 10. 00. 10. 10. 10. 10. 10. 10. 10. 1	605 +06 -206	.0		Ð	\$	>	0	Ð	→	ے	20.	2 u •	0
15,7 = 01 = 0.0		2.0	$\overline{}$	3	3.	>	0	Ð	•	C.	0	2 0	C
		15.7	0.	.	2	> :	0	9	•	្ទ	c (C	9 6
		• •	•		•	> :	•	• 1	•	•	•		5

STARK MEMBER OFFIAME KREDORM

0.0000 00000 00000 00000 00000 00000 0000 0000 0000 0000 017 012 012 019 0000 100 90000 0 2 6 6 0 0 5 6 6 0 20000 00000 20000 20000 50000 20000 0000 C 3005 V . 29 . 12 . 05 00000 24 00 10 01 29 35 07 18 07 16 0 - 0 N 0 0 0 0 0 00000 2002 27.15 77.44 7777 100 00000 0000 00000 30000 000N 71232 2000 2000 H 9599 46.50 2 2 2 2 2 2 U.S. NAVY - ACHR PLATFORMS 13.63 32.52 17.24 102.55 54.15 12.25 12.25 32.41 4.89 111.26 117.27 20.0 20.0 20.0 20.0 20.0 20.0 20.0 21.31 14.77 8.22 1.57 152.72 10. E 38.03 R. E.S. 11.36 11.35 11.36 11.37 17.56 17.04 17.94 17.54 11111 53.10 55.11 53.12 55.12 53.14 1.11 1.13 1.16 1.16 15.7 2000 # K C A F F T • 0.0 10.0 6.1 51.7 5 C C C C K AD CUNDITION -601 Sun -20e

0.00

2022

22222

01 01 02 22 32 33

4 4 4 4 4 4 W

20000

-10.57 -10.37 -10.37 -10.37 THOUSE THEFT SERVED SERVEN

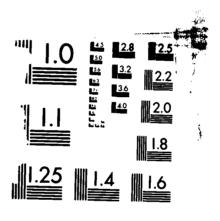
CONTRACTOR

PAGE 101	11160104
PAGE 101	
	-
	5.0
,	9
)	1
•	TALVAT
	THE C. ROLL BIN B. BLANCE ANALYSIS B. M. B. LOS. O. YOUR
	FA11
,	
	0.4760
	2 2 2 2
•	A 7
	,=
	:
4	•
· •	•
, word finance	

i

A MARKA GA	1070	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	∪ × :	DARNI	UMENT MA	PY FU	D T	3 X	AXIAL BTHE 68	ENDING	STRES.	SHEAR	SHEAK	200
3		• 1	84 T ¥	DATE T	INOAIPS	Φ.	7	Q X ¥ ₹ ₹			:			
05-1004 18	1 -0	•	1	-11.60	Ŧ.	ζ.	0	4.	٥	7		\$0.	• 05	•
1		0.01	~ ·	67.0	12.0	P 10	0	7	٠	٦,	:	• 03	0	1
				30.	7 • 6	• ·	•		•	•			0	•
	!	46.2	14.27	-7-65	**************************************	, r,	10	1.46	90	30			7 S C .	• •
***		c	,	14 000	٥	:	-	ÿ	7				•	
• • • • • • • • • • • • • • • • • • • •	,	•	, ,	50.43	•	> :	٠,	•		•		7 (> •	•
,	:	•		07:7	3 6		~ `	7	7	•		7	0 0	•
		•	- ^ ^ ~		• 3	> =		ָ ק	v ^	•		- r	- C	•
		44.2	-51,22	-57.09	7. 46	2 2	.37	1.50	17.1			0.0		Ī
4001-40	-			7 " "	r	1	7	1	•	•			•	
	;	> -	, ,		• 5		•		•				> C	•
1	•	. ~	•	109.64	-121.18	50	! -	-16.78	97	12.		 20 !	20	
		3		72.7	· ·	٥	٠.	18,7	3	~		90	C	•
		•	•	67.51	•	~		18.7	?	c.		90	0	•
010-010	72.	0.0	Ð.	-116.41	C . 92	۶.۷	37	۲.,	2	15				•
		- K	4.9.	• 54.11	0 7	2.2	57	5.	٦.	~		0	C	•
	ı	~		-<1.61	-540.14	07.5-	67.	17,52	E0.	12.		20.	70.	•
		3	Ç.	52.49	36.2	2.5	. t.	7.5	?	••		• 05	C	•
1	,	36,4		74.50	12,2	2,2	67.	5 • 2	7	Ç.		70	0	•
110 011	1 -5.1	0.0	0	27.4	31,4	٥	5,5	10,3	٠.	7		50		•
:		ĸ	c.		5,0	٥	3,2	10,5	٠,			103		1
		•	.	340.13		1.04	12.5.	10,36	.39			50	.03	•
		64.3	10 x 1		T . K	•	3.6	16,5	٠.	0		£0.		•
		V	٠ •		•	0	2.5	18.5	~	~		50		1
4 216 -210	7.5- 1	0.0	, .	06.656.	77.0	v	•	1.65	\$5.	3		0		•
		 D	r.	.674.50	۲.	17.	2,05	-14,75	. 55	. 30		03	0.3	-
		Ð	~	-344.70	56.5		•	19.7	.35	_		C		•
		۲°۰۶		01.70	55,5		•	19.7	57.			5 0.		•
		\sim	•	77.07	7 t.		•	٠ <u>٠</u>	. 35	-	-	C		1
~ ~	 •,	?• c	₹3.4€	00.45-	. 3			۲.۶	.62			£0.	03	•
		? L	63.72	-25.48	7 •	2		-2.76	79.			- 102	70	Ī
		r	63.6¢	-7.16	, 55 t	→ :		7:7		~		7 0.		•
		ू २ ४	20.62	~ :	•	•	-	, ,		0		50.		•
		· >	63.76	(2.48	•	•	~	7 • 7		~		70		•
		•	80°23	36.45	24.	v		20	•	•		40		•
		,•	60.55-	24.15	37.0)	٦,		č	۲		£0.4		•
		•	01.7.	11.35	-51.29	-, 14		٦.	.58	2		6 0.	€°.	•
			11.//-	-1.43	٠ د	٠.	7	0	ŗ	Ç		7 C		
												,		

5/6 FATIGUE ANALYSIS EAST COAST AIR COMBAT MANEUVERING RANGE OFFSHORE KITTY H. (U) CREST ENGINEERING INC TULSA OK SEP 76 27-771-100 CHES/NAVFAC-FPO-7616 N62477-76-C-0179 F/G 13/13 AD-A165 651 UNCLASSIFIED NĿ



MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS 1963 A

Ť

STRAN MERSER DETAIL MEPORT

026 016 024 024 0 0 0 0 0 0 0 0 0 0 020 011 011 020 00000 031 010000 102 10/05/76 90000 2000 00000 22200 40000 65000 0 0 0 0 0 0 0 W 90000 20000 9 0 0 0 0 9 4 4 8 00000 55555 STRESS 8 2 2 5 M 20 - 0 0 N 25.00 4 N - N 5 . 15 - ACHN PLATFURMS - FATTIONE ANALYSIS - MLH 105.0 FE 55555 22222 22222 ~~~~ ~~~~ ~~~~~ 7.00 M 1.5.6.1 2.6.1 2.6.1 2.6.1 00000 44444 20000 * 2000 24224 00000 72517 4 4 2 4 4 F Y E S 13.01 17.02 11.03 57.95 25.15 12.30 13.35 9.56 5.09 11.06 HUMENT HZ IN=KIPS U.S. NAVY 35.67 35.67 11.70 11.00 20.00 20.00 20.00 20.00 20.00 20.02 20.05 20.05 24.54 11.68 11.68 115.48 MUMERT FUSCE FX AIVS 00000 V C 0 2 C 00000 V E 1 2 3 00000 V F 0 C C N + 3 & 0 GRCCV AND SECTA LUAD CUNUITIUN -007



 $f_{i,j'}$

TRAN MEMBER DETAIL REPORT

U.S. NAVY . ACHH PLATFORMS . FATIGUE ANALYSIS . MLW 105,0 FEET LOAD CONDITION NO.

	1 2 4	FORCE FORCE	MOMERT	せして 下 と 一	EAR	CHCE	TUKSION	XIAL	BENDING	5	HEAR	HEAF	ar.
SUMBER AND SECTA	F T	× ± ×	84 X 1 X 1	SdIYeVI	> u ×	R I PS	SAT X=VI	STRESS	>	Z ******	STHESS	SIRESS	CHECK
01- 102 418- 1	ó	6	55.	20	000	0	•	9	•	•			50
	-9	90	70	3	90		ē			4			٠-
	7.3	90	32	1.97	90	10.	00	00	0	10		0	000
		0	25.	3	90	•	ē			٥.			S
		0	49.	٥.	90.	•	Õ	9	•	N	10		0
1 -414 404 -10	s	•	10.0	٥	4		=	•	-	4	. 2	ć	-
	•	•	•	•	2 -			•) =	•	•	7 -
!!!!	•	•	30				> =	•	•	•	>		5
	•	. 0	0.7			•		•		•		•) C
; ;	3	50	55	3.03	93	00	00	00	2	28	10	00	013
			, '	,	•		•	,		•	•		,
1- 201 DRL- 1	> 		•	0	 -		3 0 1	٠:	c. c			5	0
	•	•		•	-	→ -	9 4	•	3 (3 3
	•	•	•	•	:-	• •	2	•	•				3 6
! ! !	5.0	000	•	17.37	C		15.63	8	0			10	200
1	5		1	4	•	•		•	•	•		•	
	> *		<u>-</u>		? :	2 9			•	v			- 0
	7.0	-	• 3	C. 2	2 3			> <	2 5	2			> c
	10.9	2	1.75	3	30				. 0				015
	14.5	-	2	4,15	2	0	3			39	00	00	
2- 104 nob- 1	0.0	00	00	7	9		0		0	0		00	0
	3.6	0	9	22.			9	9		0		0	00
	7.2	30	9	70		00.	00.	02.	00	00.	8	9	000
	10.9	00.	20°	02.	2		9	3	0	0		0 °	C
!	3	00	50.	2 7 0	•		•		0	9		00.	C
2- 105 n08- 1	•		20.	% 0.	•		00.	2	C			00	C
	•	٦.	Э	7)		00	٥.	0			00	C
	•	-	3	~	00.		000	3	0			00.	0
	10.0	==	3 0	95.	• •		000	~ ~	000	20.	000	000	500
- 406		•	**	•	•	•	:		•			! . ;	
	, •		77.	٠.	•		2	> <	•	•			⊸.
	7	5	74	91.10	20	0		9					~ c
	0	0	27.	3	•		9			•			0
;	14.5	90.	15	54.			00.	Э	Ç.	70		00	200
03- 203 UML- 1		10.	1.08	94.5	~	0	7.2	9	0			C	0
	•	10.	79.	7.7	~	•	7.2		100			10	C.
	5° /		9	-12.40	-11	10.	-7.25	00	7 0		10.	10.	100
	•	10.		9									•



TEAN SELBER OFTARL REPORT



\$

EE E



{}}

11/1

THAN MERSES DETAIL REPORT

00000 00000 0 2 0 0 2 0 0 2 0 0 3 0 0 3 0 2000 00.5 00.5 01.5 02.1 02.1 030 0.20 0.50 0.50 0.50 0.50 22600 00000 22222 V W W W W 00000 2 4 4 4 4 20000 55555 -KSI-99.2.2.4 00000 3122 2000 22222 55555 22.40 22.40 22.40 22.40 88888 -1.06 -1.96 -1.35 D D D D D 90000 200000 00000 FZ M M M M M 20222 77777 20333 99998 88998 88998 88998 18.97 24.61 08.56 BY I H-NI 544.80 404.50 263.05 -139.01 311.24 324.55 387.60 182.71 2.75 1.95 1.77 7.02 2222 7,7,7 FUPOR FX FX FX FX FX LUAD CUNDITION NU STOCK SECTA



	:					į				- 1	> i	N	
NERBER GROUP			- Z - Z - Z - Z - Z - Z - Z - Z - Z - Z	7 7 7 X X X X X X X X X X X X X X X X X	SHEAK F	/24	NOTES AND L	AXIAL	ME 401NG 4	518653 2	STEAK STAFE SO	BIREBE	C 1 1 2
StCTN	TN FT.	Se I x	Sel X-v1	INSKIPS	\$dfx	KIPS	Selvent	•		K81		!	
- 400 UKL	• 1 0•	•	410.04	3	2.1	7.	79.3	٠,	÷.		11.		03
	1.		368.00	ň.	~	₹:		3	ď.		7	⊶.	9
	7.7		260.46	V6. V7.			7.00	20	6 4		===	~ •	3 5
1	247 T		-549.57	219.00	1.67	7.51	79.31	3	- 543 -		52	. 23	020
- 501 JL4	• 0	-16.1	55.42	2	25.1	3.1	20.5		0		. 55	N	400.
į		-16.1	-46.74	45.7	20.4	1.5	20.2		~		.23		S
	N P	-14.	-141.21	٦,	27.6	9.0	20.2	•	2		*2		.014
	. a	15.11	-143.33	151,38	-26.40 -30.09	-3.06 -3.03	126.24	90.	6.55		25.	25 50 50 50 50 50 50 50 50 50 50 50 50 50	200
74 015		15.1	•71.64	ص	. 4	. 4	9		•				
		12.5	2	-	•	÷	50.05	9					• 0
	6.3	12	51.05	40.27	14.02	3.63	-56.98	3	30		2	15	
	5.4	12,3	77.0	N	٥	•	56.9	•0•	0			-	9
!	6.5	12.3	v	< .	٩	9	56,9		•••				0
- 503 JL4	. 1 0.	-405.41	-	\sim	15.5	7.3	51,0	2.6	2		.19	91.	13
İ	-	- (146,00	0	15,4	r.	51,0	2.0	2		. 20	72.	13
	M 4	04	454.25	42.546	70.7	S	3.	S 1	~		-2°	2.5	M :
		1	1024.62	-1400,94	17,09	41.64	-51.00	-2,62	\$ t		. 23		149
511 71	- 1 0.	612.9	2.645	£	7.4.	٠.	34	0	9		90	0	9
	1	472.9	25.	Ē	4.6.	•	94.0	0	45		90	96	150
	2,3	2/4	51.7	-676.92	-5.45	16.1	184.02	3.04	33.		80	80.	•
	त । भ	0.570	976.02	0 0	***	•	30	٠	M :		80	æ :	.159
		• > / 6		2		_		2	- Cp.		90	80	2
- 500 JL4	~ .		7.4.7	223,93		-11.34	209	2.73	0		910	.14	13
!		0 4 4	-154.34		0.20	ċ	0 4 0 0	· ·	- 001		510	٠.	⊸.
	2.5	645.0	-523.24	. 7			209.0	: ~	•			-] [
:	9.4	675.0	-768.70	0	7		209,6	. 7	92			117	136
- 512 "	• 1 0•	4	-25/,55	30	•	~	85.7	3.1	Ξ.	•		-	5
		7 0	64.861.	T			93,7	7	-			••	5
	7 7		CC - CT - CT - CT - CT - CT - CT - CT -	-	ָ הַ	٠,	700		7				\$
,		5.4	-23.16	315.74			183.78	3.16	12.		20	20	154
- 502 105	-	2	٠,	īŲ	•	•	٠. د	17.	•			0	4 C
į	H. M.	21	14.02	0 1		• 10	-20.35	4	1,43		15	. 15	. 579
	0.7	70.71	8.10		:	∹.	20.3	3	Ð		224		S
				•	,	¥ .	3	4	•			•	

THE REPORT OF A STATE OF STATES

T

raese rannona vandida hossasaan sasnasaa kandonna araabaa habbaasa disessa disessa disessa disessa disessa dise

i di ja

LUAD CUNUITIUN N	٠ د د		•)					23	AGE 108	02/10	
	•		U.S. NAVY	Y - ACHH PLATFO		ATIGUE ANALY	818 - ML*	105.0 FE	E 7	!			
	1810											2	
TOTAL CAUCA		ROYOF PARTIE	BOMENT	*OMEAT V	SHEAM FL	URCE/	T. TOYEL	AXIAL	BENUING &	814688	SHEAR	SHEAK	
ø	-	S A I A	Nak les		X I P S	X I P S	1N-K 1P8	 -		K 8 J		Y .	C.E.C.X.
501 - 504 165- 1	0	-64,31	-126.71	٠.	.17	0	-	2.1	•		.01	C	
	¥ ° K	-64.32	7	-	~			4.1	•	i	0.	0.	7
	•	٠,	9	77.0	~:	~ ,	~:	2.1	٠		51.	(\$.
	15.1	-04,35	14.02	80.505	4 .0	70.	27.	.2.13	90°-		12.	12.	1 34
•	,	٠.			•			, '	•	i : !		,	
501- 601 JLS- 1	3 .	10.83	v.	07°50	•	∹.	25.4	~ ~	# : ·		25.	55.	0
	C • •	05.44	55.0		2 6	27.7	6/2°41	67			00	0.5	
	3	-53.50	70.481			. ~	25.4	١ 1	3		. .	9	
j-1	*	.53,49	641.74	74.1		~	25.4	~			7	9	
501- 642 200- 1	0	97.70	246.26	×.	-5.41	5	9	-	•		3	4	5
1	, °		. 3	50.7	4	3	20.0		•		35		717
f	0	04,73	-54.35	2	~	10.1	20	1.75			- 12	.27	
	•		55.5	~	•	*	9.0	1	7		.20	~	5
1	70.0	•	-217.82	4 H . 7	•	~	0	~	5		115	- 18	_
505 - 503 105- 1	0.0	•	-5.75	~	4.7	\$	æ		1.00			\$2.	_
	5.3	٠.	-21.06	-	~	•	3.	٥	~			-	0
	~	5.0	95.60.	7		3	9	٥	£		-	-	9
	- 1	>	3 2 2	63.76		77.	14.07	9 4			010	2:	0.05
	•	•	70.80.	Č.	~	?	Ð.		, , , , , , , , , , , , , , , , , , ,			-	S.
502- 504 105- 1	0.0	1.10	-10.04	-	~:	.11	~		£				•
	4.5 L	٦.	00.7.	•	~	.11.	٠,	_	10.		-		~
	► •	0.7	1.50	-2.H	01.	12.	5.56	010	77.			.13	600°
	- 2	•	20.0	•	7	32.	٠,		02.			.13	
	13.6	9.	60.37	•	01.	920	~	-	_				~
502- 505 105- 1	0		-14.66	K . 7	-1.54	.24		.65	•1.76		18.	1	-
.,	3.8		•10	2.1	•	.18	2.7	•	•			97	
1	~	94.6	-5.45	£	>	.13		2	•	!	100	٠,	0
i	15.4		. 4.0	07.55.	. 6 ¢ ¢ 1	90.	2 2				91.	0 F	20.0
. The same of the	· c		, ,	•		4	3	•					. :
	3 4	•	77.77	7	9 4	C P	71.7					-	2:
. 43	9.		70.65	7	04	38			•			21	- o
• ,	11.4	44.01	-35.32	19.2		•	12.1	. ~			•	• -	, (
	•		10.65		•	1.05	12.1	1,59	1.		=	113	0.50
	:	0	•	٥					•				•
1010 600	· ·	10.050	613.03		60.25	-15.51	22.104.		27.		25		N . V .
	3.0	2	24,7	15.7	21.5	15.1	301.4	2.0	4		67	. 3	0
• • •	•	550.9	54.5	33.0	20.0	15.9	341.4	3.0	-		7	3	. ×
	9.1	2	16.46	15.4	· ·	٠.٥	391.4	3.0	•		. 45	4	ĸ

142 .036 .055 .055 .118 .034 .115 258 1158 1158 057 0 3 3 0 0 0 0 M 4 T 125 156 186 210 SHEAH 109 27 15 07 30 30 SHEAR 2002 ---K81--STHESS BENDING 1.19 50 71 71 71 8.05 24 C U 7.58 2.45 1.65 1.85 P O D O M ANALYSIS - MLW 105,0 FEET AXIAL 9 9 9 9 9 22222 50.76 50.76 50.76 50.76 110.97 110.97 110.97 87.000 133.40 135.40 185.40 175.40 24444 TUKBION NX INEKIPS 10. ES 7. 11.2 5. 56 5. 56 61 67 67 67 2000 200 N 20000 100.17 2.64 2.94 1.61 FATIGUE 12.50 1.50 1.50 1.70 25.13.1 11.01 10.50 PLATFORMS 25.00 10.20 21.11 22.52 -201,48 -141,59 -36,89 -37,02 101.03 69.69 120.52 210,45 210,45 252 64 202 06 202 06 205 300 224 60 225 50 255 52 -510.03 -625.57 -1545.57 -2159.99 -587.34 195.67 978.69 1761.71 2544.72 841 x = 21 57,54 212,25 343,09 452,56 -174.57 -13.69 106.07 10.57 40.69 84.63 164.49 210.85 125,49 43.25 *22.17 10.14 4.57 8.78 8.16 41,03 57,47 64,40 63,05 700.03 -72.04 -845.01 -1617.42 142.57 142.58 142.58 69.20 69.21 69.21 69.22 672,91 612,91 612,91 672,91 FURCE FX AIVS 2000 2002 Proj 10.0 14.0 25.3 ETCCF AND SEC 12 SUND1110N <u>:</u> 165-

LUAD CUNDITION NO.	, o		U.S. NAV	Y . ACMK	PLATFONMS . FA	FATTGUE ANALY	MJM - 818.	105.0 FE	E T	DATE 10	105/74	ı
,		,		ı							2	
	T	•	1.27 P. 24	MUNENT NA	/===GMEAK F	UKCE	TURBION	AXIAL	HENDING STRESS	STEAM	SHEAL	GE-30
			SALX-VI	INexIPS	SQ X	KIPS	INEK I PS			2	2	C 1 ()
512- 712 -1-	~	*****	-25.10	£	1.04	٠.	A 5.9	3.1	~	-	~	5
	•	-640 ×	431,19	7	1.04	•	83.4	3.1	~	-	-	<u> </u>
	16.7	F :	10 t		69.1	6	85.9	3.1	3	2	-	2
•	25.3	18.054	1794.24	197.35	200	5.46	185.94	-3.16	. 63 	000	010	.177
FEUTENBUL NO. PERSON PE	0 I 0 0 I 0 0 I 0 0 I 0 0 I 0 0 I 0 0 I 0 0 I 0 0 I 0 0 I 0 0 I 0 0 I	-8.4137536	306-03534	46003	2.4461409E=0	1.607486	6E = 04 = 8 • 0	9.50	70	ı		1
31- 621 360-	**	-52,48		-1083.48		•	58.1	3.		100	P	4
!	2.0	55.55	22.463	1587.76	15.01	•:	5 1	75.	ï.	•	!	9
	9		474.33	-1802.46	. -	``	1.85	. 1	? -	٠	7 "	5 6
:	0.1	İ	545.69	3 3 5 5 T	•	6.87			200			.072
PELITARION OU POSS FELITIBATION CHECK MELLEN BOS BAS	210 010 4 4 50 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	-,1317193	•	2504635	. 4261271	4,511093	76-10 -1.	0753#7	.5750219		:	!
-97F 625 JLB-	° 0	!	53.84	232,00	-12.4	12.8	63.9		7	. 3	3	<u> </u>
	1,5	1	-170.49	453,39	-11.0	1.7	63.9	3.8	۳,	*	-	. 2
	o 4		-575.54	563.34	-11.6	10.7	63.4	\$.	7	-	~	2
		549,75	-724.89	1050,90		# 4.25	463.94	3,65		35	. 132	275 515
E SULL SULL SULL SULL SULL SULL SULL SUL	0140 0140 0403	.1217265	V	961156	** 4027021	-2.176875	6E-09 1.	334546	.9128823	† 	ı	1
35 ece Jee	0 .	9 4 9	452,56	æ.	٥.	7	2.00		48.		-	^
:	517	645	578.80	278.71			44.2	•	3	•	•	·
	1	0 4	0000	A 14	7	~•	7.7	•	4 1	0	0	\sim
		9 6	645.91	241.79	7 7 7	2,97	02.33	4 4	. 51 . 55	200	. 0	231
21- 651 JL0-	1 0.0	55-	510,57	æ		۲.	6.04	•	۲,	20	94	
1	1.5	25-	545.54	/	ε.	÷	60.5		. 3	5		. ~
	2 4	24.54	615.57	<u>,</u> ,	ວຸາ	•	50.09	•	3 1	~		Ş
	0.1	• > 5	700.05	-2158.71	2.55	2.49	540.52		1.60	52°	52. 52.	0.00
22- 705 200-	•		-218.05	~	Ð	•	30.5	7	90	<u>.</u>	-	-
	\$	0.4.7	`.	~ 1	1.56	1.05	-30.45	1.75	500		2 -	159
) 	69.7	-41.33	ě	7	•	3	7	9	۹.	·À	1

1.15 3.28 02, 02, 0517	I	4	1	1	1	ı	,	ı	1	ı	ı	1	ı	!	1				!
				ı				•		1		ı		•					
2	12 22 32 32 32 32 32	F09	2.0		*	1	1	ļ 1		1	•	1	1	1	i	I	ı] 	i
14	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	1.00	→ ~	i	ţ	1			İ	1					ļ		ļ	1	
باج	(1-1-p-1)	~ 10 0		t	1				1	1		! !	:		<u> </u>	i	1		
٠.	WWW.00		w 3	Į.	i	•						! !		; ;	! [!	:		
_			i		1	1	i				!			•			ļ	! !	
- 05	22.25	15	. 47	, , 1			•								 - 				
						•								<u> </u>	! .				
•		1											. 						i
10	: a < 100	M & W	3 F			t i								 	! 				1
3.2	111111111111111111111111111111111111111	NN =	~~			!													
. <u>.</u> ,	a a a a w		بر ب <u>ن</u>					}											i
	2000x	2.4.2	• •	i														İ	;
S																			
. 30.45	00000	3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	7.7																
•	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4																	 	
	rrece		- 7																
	2000	F		i															!
ļ	D		į	į									 						
9.01	2 4 6 6 6 7 5 7 6 6 6 6 6 6 6 6 6 6 6 6 6 6	· · · · · · · · · · · · · · · · · · ·	,											:				!	
	D 2 0 0 0	4 - 4	5																:
		,																	
7	*******	3 3 V	- - ^																
	11.03 17.03 17.05	-5/3.24 -3/9.14 -243.95		i															
के या के	100 100 100 100 100 100 100 100 100 100	2.25	3																
∿	6 0000	>	Λ×	1												! !			
U. & Y	3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	160.05	. ε . ε . ε . ε . ε . ε . ε . ε . ε . ε	i											 			 	
3	-735.58 -894.98 -1055.07 -1148.50	171	•		İ														
د .		٠ ٠ ٠	.	•									i	ļ				!	
7.	5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0 7 7 6 	 	!	İ						!							:	
	****			1							ļ		ļ ì		! 	l i	I		
•	0.000	2 N C C	 			•	! !			!				 			:	•	
N		_	→ ∀	:		i		İ	1	İ	į		;	 				i	
21.44 A1.50 37.5.02 4.12	tegan ese	2 2		 	!	!			!								!		
	5			:	!	!					İ		,	!	İ		1		
	•	101			1	ł	i		1		: I		!	; 	÷	i	!		
	A23•	• • • • • • • • • • • • • • • • • • • •	,	•		-	!	. !	· !	•	;		1	1	•				
,	į į			· • •				•	•				:	7 : :					_

10 10 10 10 10 10 10 10	7000	+ SIO +	e Della	I N M X C X	TA ARIT	¥ 14	/*************************************	NO I WOULD	~ ×	2.00 P. C. C. C. C. C. C. C. C. C. C. C. C. C.	¥ 4 ×	7 JH	COMB
310 10 10 10 10 10 10 10 10 10 10 10 10 1	NUMBER AND	, J) X	¥	H. 2.		7.4) E	TREG	Z	. S.	(E)	UN1 1
10	SEC 12	# -	۸ ۲	d X = 7	12-21	<u>a</u>	d d	¥ Z		- I Ø X			CHECK
1,	-002 90	0.0	2.5	10	7.	0	30	16.8	3.7	1.0		_	22
11.0 1.0		5,5	.5	ď	5,8	3.		10.8	5.7	1.1		0	5
1,		11.0	5	ď.	2,5	3	7.	10.8	3.7	Œ.		~	22
10 10 10 10 10 10 10 10		7.01	42.5	7.7	6.	'n	2.6	16.8	3.7	Š		-	2
10. 10.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	1	617	42.5	/*Q∪ ?	7.0	∍	3.7	15.0	۶. ر	2		2	2
1.5	56 JL0-	•	45.4	244.57	•	٥	~	43.9	٠,	S		0	23
1		1.5	5.4	875.58	~	S.	30	43.9	٠.	5		0	23
	*	9.0	0.7	876.50	•	₹.	Š	7.57	·^	3		90	23
0. 1 0.0		9	4.5	655,55	. آ	٧.	1.9	43.4	v.	S		90.	23
01 JLC = 1 0.0	-	•	0.		~	٠ •	5.3	45.9	v.	•		910	5
1.	01 JL6-	•	5 × 5	٠,	N	1 %	3.6	79.1	3	S			90
5.5 -5.4.35 524.50 -14411.05 -224.08 -3.40 979:10 -41 = .45 .40 .40 .40 .40 .40 .40 .40 .40 .40 .40		#.	•	600.47	~	21,0	3.5	79.1	7	٨		•	07
5.1		5.5	M. X	524,50	0	26.4	3.5	7.1.1	₹.	•			05
7.1 0.0		5.3	۳. ت	450.03	=	24,0	3.4	79.1	4	£.		• 66	2
03 JLe-1 0,0 -564,35 -1274,35 1695,47 8,04 4,525 -565,10 -4,09 -1,33	,	7.1	54,3	377.00	301.4	26.0	3.4	14.1	7	3		24.	03
1	03 JL6-	•	584.3	1274.5	3.6	2	Ĭ,	565.1	9	,		9	2
5.3 5504, M5 = 1070, L20 1314, 117 4.84 6.53 = 555; 10 = 4,09 = 106 334 314 37 37 37 37 37 37 37 3		£.	504.8	-1194.44	3		0	565.1	2	2		200	2 2
5.3 -564.86 -444.85 100.70 8.00 -565.10 -4.09 -990 .37 .37 .37 .28 .39 .39 .39 .39 .39 .39 .30 .30 .30 .30 .30 .30 .30 .30 .30 .30	 !	3,5	504.A	-1070.40	314.1	20.5	2	565.1	3	0		75.	5
00 JL0= 1 0.0 6444 05 605.30		5,3	564.8	4014.00	0.45.4	0.7	0	555.1		٠.		.37	25
00 JLc- 1 0.0 0 0444.05 710.55 710.55 7.0 5.08 -3.61 -443.90 4.51 .51 .45 .15 .15 .15 .15 .15 .15 .15 .15 .15 .1	1	7.1	χα: π	126.5	X.			565.1	⊃ 3	`.		30	2
1.6 http://doi.org/10.554	-01F 90	•	0 7 7	805.50	-7.70	Š	3.6	43.4	Ş	'n		10	2.5
0.5 0.4,05 0.4,05 0.4,05 0.4,05 0.1,03		1.8	0.77	710.55	-140.57	٥	5.5	43.4	S	3		7	2
5.3 644,00 416,39 -645,40 4.51		3.5	0.77	\$60.51	-266, 55	7.	6.9	45.4	š	3		5	2
7.1 644.06 419.55 = 640.26		5.5	0.71	416.39	60.450-	7.	¥.4	45.4	ŗ	m		-	2
04 137 = 1 0.0 45.30		7.1	C	219.35	-606.28	20	0.01	45.9	.5	,41	~	~	2
4.3 4.3 56.45 1.02 -6.66 2.25 1.07 10 17 10 10 11 14.1 43.50 -11.02 -2.49 -6.66 2.25 1.07 11 11 11 11 11 11 11 11 11 11 11 11 11 11 12 <	02 137-	2		5.7	63.47	5	7	9	N	٠,	71.	-	~
9.4 49.50 74.19 59.75 1.02 40 -0.68 2.25 1.07 1.7 1.1 14.1 43.50 -11.00 -25.29 2.00 -0.68 2.25 449 27 1.2 15.4 43.50 -25.29 2.00 -0.68 2.25 2.49 2.25 2.49 2.25 2.49 2.25 2.49 2.25 2.49 2.25 2.49 2.25 2.49 2.25 2.49 2.25 2.49 2.25 2.49 2.25 2.49 2.25 2.49 2.25 2.49 2.25 2.49 2.25 2.49 2.25 2.49 2.25		7	5,5	54.45	84,31	>	7	9	2	Ś			17
14.1 43.50 =11.00 =25.29 2.00 =34 =6.68 2.25 249 27 28		3	5.5	61.4	54.75	3	7.	9.	7	٠,	_	•	7
15.4 43.30 -26.50 -105.74 2.49 -10.66 -0.66 2.25 2.97 21 21 0.06 04.15/*** 1 0.0 -4.5 -25.55 -35.53 -99 -10.66 -11.65 -4.3 -1.21 -21 -0.6 4.1 -4.5 -9.5 -9.5 -11.65 -4.3 -1.64 -1.2 -2.0		, ;	3,5	-11.00	-25.29	3	٣.	6. 0	'n	7.	121	.27	2
04 157 1 0.0 = 4.35 = 25.45		ċ	3,3	۶ ۵ °	-165,74	>	Δ.	9	٠.	•	.37		25
4.7 -4.33 -10.64 41.44 -15 -11.65 -43 -16.4 -12 09 4.4 -6.32 -9.50 -9.50 -5.03 -11.65 -11.65 -43 -16.0 -20 -20 -07 14.1 -6.29 -1.92 -0.5 -11.85 43 -1.29 -30 </td <td>04 157-</td> <td></td> <td>. H. S</td> <td>-25,55</td> <td>63,53</td> <td>•</td> <td>-</td> <td>11.0</td> <td>7</td> <td>1,21</td> <td>~</td> <td>~</td> <td>8</td>	04 157-		. H. S	-25,55	63,53	•	-	11.0	7	1,21	~	~	8
9.4	:	4.1	. K.	-10.6h	41.4	3	•	11,6	7	1.0		_	60
14.1 = R.30 = 4.56 = 15.69		.	. H.	05.6-	и,	·.	~	11.8	3	-		~	0
16.8 = 8.29 = 3.82 = 150.72		10,1		14.3E	u١	٦.	0	11.8	4	Ň		~	20
01 JL7= 1 0.00 54.17 297.20 -4444.29 10.56 -1.87 340.917768 .34 .34 .09 7.1 54.14 149.12 -1051.00 3.91 -1.61 340.9177 1.35 .28 .28 .09 14.2 54.13 23.47 -1155.53 -1.63 540.91 .774428 .28 .28 .09		-	~	-3.82	150	20	•	11,8	3	2.5	•	•	7
1 540.14 149.12 =1051.00 3.41 =1.61 344.04 .77 1.35 .28 .29 .09 .29 .29 .29 .29 .29 .29 .29 .29 .29 .2	01 317-	0		97.2	~	2.5	1.8	6.04	•	۵		į,	9
2 544.13 25.47 =11.55.55 =1.03 =1.35 340.41 ,77 1.44 =28 .26 .09 .09 .42 .07 .07 .97 .42 .42 .07		7.1	. 1	1.67	ć.	2.5	1.6	7.07		~	•		60
5 54.15 FR.C. 05 FR.C. 44 -6.48 FR.C. 15 540.41 77 .07		7	÷.	3.4	~	•	1.3	40.4		7.	•	~	60
			7	=	=			•					

Column C	Column C														
10 10 10 10 10 10 10 10	1,		N134 4	37.0			1E. A 6 <	URCE	3	X I A L	ENDING	PES	HEAR	2 V Z	20 ► 1 ►
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	Colored Colo	,	, <u>-</u>	8 1 4 1 4	4 H H P	N=N	<u> </u>	A. T.	ż		- 1	* X S I			- U
	1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	-C12 010	5	1.5.1	455.0	•	8	•	28.4	2.7	3.3			- 3	8
	1,		√.		3.	•	کا ک	1.3	20.4	2.7	1.22			N .	7
1	1		<u>,</u> ,	7 • • • • • • • • • • • • • • • • • • •	•	• .	, ,	~ `	200		, o		- 6	- 1	0 C
10	1	,	•		139.5	• •	1 3	2.0	26.4	2.7	3.2	•	7 2	U J) (T
25	24- 74- 10-11	- 705 157-			٥	0.0	\$ 5.5	3	٠,	٠,	٥.		•	100	0
1,		•			.45.3	3	2.1-	C			62		~	1	7
1		•	,		•17.0	~	S .	-	S	•	. 15		$\overline{}$	-	5
			•	a .	ο.	~	•	™ :	3,	•	-		0	0	5
1	1	1	τ.	- 4	3	Œ.	1.S	3	Š	γ.	•	:	6	~	2
10	1	124 167-	•	75.	t.	٥	3	•	٥	.	₩.		0	O	6
10	14 -52		•	- >54	300	-)	0	٥	3	ń		50	0	3
1	10		.	52	<u>٠</u>	e,	3	 (•	3.	2		0	0	5
1			, 1	5.5	, ,	٠ ٠	5 3	v	0 6	3 5	9		•	•	ر د د
10	25			•	•			ĺ	•	•	•		<u>.</u>	•	•
	1	- 705 1e7-	ດ • ວ	4.0	¥.	0.09	5.1	0	1.5	3	2.1		~	*	~
14. 1			1 3	ຕຼາ	· ·		.	o	S	ů	`.		(⊸ <	50
15.0			. 3	• 7	•	0 X	2 7	-		, ,	7 1		> -	-	, ,
1	13	1 1 1	τ.	τ.		71,5		-			2,9		. 1	• 📂	.
	\$	- 705 157-	•	21.1	3	125.4	•	3	5.7	1.1	<u>ر</u> - ۲		-		4
1,	1		7.5		· <u>:</u>	101		~	3.	7 . 7	1.2		-		٠.,
	1,		•	-	7	14.3	•	-	5.7	7 . 1	\$		-	-	
	\$		J X	•		~ ~	•	-		•	•				C 3
\$\text{5} \text{0} \text{1} \text{0} \text{0} \\ \text{1} \text{0} \text{0} \\ \text{1} \text{0} \\ \text{1} \text{0} \\ \text{1} \text{0} \\ \text{1}	\$\text{5.6} = 1 \text{1.0} = 1 \text{0.0} = 1 \text{0.0} \\ \$\text{1.0} = 1 \text{0.0} = 1 \text{0.0} \\ \$\text{1.0} = 1 \text{0.0} = 1 \text{0.0} \\ \$\text{1.0} = 1 \text{0.0} = 1 \text{0.0} \\ \$\text{1.0} = 1 \text{0.0} \\ \$\text{0.0} = 1 \text			•		•		•	•	•	•		•	•	•
	5	- 8:1 Rus-	•	- t	1 * C . L	7.0	7.	F	7.	4.7	3.8			9	3.5
37.7 = 10.7 0.7 d = 224.90 = 3.17 = 22 d = 2.7 d = 1.30	37.5 = 10.5 (0)	: :	:,	2000		. 0	5	U ~		~ ~	- n			۸ -	2 7
\$ 603 JL7	\$* 603 JL7* 1			5	``		-3.2	. ~	7	. ~				~ N	. ~
\$	\$		•	45.	۲.۷	4.7	2.0	*.	7.	2.7				3	5
7.1	7.1	- 605 017-))	105.7	7	16.2	2.3	3	7.9	3.	M		~	1	4
14.2 -6.54.73 -1120.04 720.41 107.45 -6.41 -1.55 107.45 -6.41 -1.55 107.45 -6.41 -1.55 107.45 -6.41 -1.55 107.45 -6.41 -1.55 107.45 -6.41 -1.55 107.45 -6.41 -1.55 107.45 -6.41 -1.55 107.45 -6.41 -1.45 107.45 -6.41 -1.45 107.45 -6.41 -1.45 107.45 -6.41 -1.45 10.	14.2 -655.75 -1120.09 720.41 3.29 2.10 197.49 -6.41 -1.69 3.20 2.10 197.49 -6.41 -1.69 3.20 2.20 2.30 197.99 -6.41 -1.65 3.50 2.27 3.50 2.27 3.50 2.27 3.50 2.27 3.50 2.27 3.50 2.27 3.50 2.20 3.50 3.50 3.50 2.20 3.20 3.20 3.20 3.20 3.20 3.20 3.2	1	~	10-05		05.3	0	2.0	7.4		۹.		~	~	0
25. 25. 25. 25. 25. 25. 25. 25. 25. 25.			, ,	L. 11.00 .	٠	3 'C	٧.	- '	7.	> :	•		N 1	N 1	5
25 107 1 C. 7.21 5.52 -74.50 -1.95 .00 .00 .02 5.54 .15 .15 .15 .15 .15 .15 .15 .15 .15 .15	10. 7.21 5.56 -74.50 -1.95 .00 .00 .00 .02 5.50 .33 .01 .05 .00 .00 .00 .00 .00 .00 .00 .00 .00		••	, a c ,	;	345.0	. t	•	6.	•	١		-	~	~
155 107 1 0.0 2.55 -74 -1.95 .00 .00 .00 .02 2.59 .35 .35 .35 .35 .35 .35 .35 .35 .35 .35	25 107 1 0. 7.41 5.35 -74.50 -1.95 .00 .00 .04 .05 2.50 .1 4.7 7.41 0.35 6.40 -1.0002 .04 .05 .05 .05 .05 .00 .00 .05 .05 .00 .00		11:		4.12	Z07.5	'n	7	*	*	~		1	3	÷.
7.21	2. 7.41 3.45 44.010506 .04 .05 .05 .06 .06 .06 .06 .06 .06 .06 .06 .06 .06	- 755 107-	•	•	5.36	14.5	P. 1 -	C	•	Ð	5		₩.	1	1.5
0.0	2. 7.41 -2.54 13.45 .42 -112 .04 .05 .05 .05 .15 .15 .15 .15 .15 .15 .15 .15 .15 .1	1	•	•	9,52	3 (3:1	•	သ :	•	٠,		~ (~ (٠.
10	7-41 -94-10 -95-94 1-40 -913 -99-94-10 -95-94		• 1	•	7	د ر •	•	•	> :	0 (ų:		.	٠.	, o
	7.00		; ,	•	v :	700	• 1	-	٥ د	D 4	• ^		•	~ •	3.

 $\mathbf{r}_{i} = \mathbf{r}_{i} + \mathbf{r}_{i} = \mathbf{r}_{i} + \mathbf{r}_{i} + \mathbf{r}_{i} = \mathbf{r}_{i} + \mathbf{r}_{i} + \mathbf{r}_{i} + \mathbf{r}_{i} = \mathbf{r}_{i}$



COOLER TEATER SERVICE SERVICE

##E4 GRUUP FRUUT SECTA FIG 137 1 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4												
0 P 20 C 1 S 2	2.00		1 . 1 . 2		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		•			> 1	7	•
SECTA 0 13/= 1) X (4)	1	7 7 W	د د ن	7.4 1.5	TO XE	STRESS	9	2	STHESS	STRESS	CNITA
100 137- 1	I. KIPS	INOKIDO	INSKIPS	201 x	AIPS	Set yev!			*** 8 I ***			
3 2 3 2	H-13.H	30.	3	٥.	\sim	0.7	۲.	P)		.31	.31	.176
3 5	-13.4	٠ ۲	12,30	-	-	7.0	~	. 31		121	121	1900
		3 .	~	٦,	•	\ • :	`•	•		=:	-	X (
	**************************************	2.03	25.03 24.52-	1 00	.21	10.72	2/.	. 65			27	
- 705 157- 1 0.		-14.26	27.44.75	3	_	8.4	9	ŧ		.07	C	3
7	-51.		٠	. 7	~	P .	1	~		0		2
6		16.80	7		1	1.6	•	~		. 60		~
3 2 2	-51	EC. 03	56.52	2 2 3 3 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	79.	11.87	1.00	96.			60	.150
		•		†		•	•					•
01	187	571.05	, r	~ 1	- 0		•	N :		<u>.</u>	ù.	3
	1 107.7	24.60%	11.20	05		4.2.3	40.4	11.14		2	9 6	277
	167	-164.57	3	3			•	• c			20	. ~
\$0\$	107.8	47.57	3,1	· •	3		· ·			14	114	· C
- 606 JL7- 1 0.	0 454.5	450.43	-459,12	8.1	30	276.2	3	Œ		.52	55.	M
,	11 454.5	963.2	٥.	3.	5.3	270.2	3	۶,		34	934	7
37	5 454.5	34.0	٦.	•	ž.	278.2	₹.	4		.25	\$2	3.
. 17	202 27	709,54	46.54	71.	v 0	-276,26	6.4	20°		.35	. 25	545
)		•	•	•	•		•	٦.		1	:	•
- 610 FZ- 1 U.	12,5	674.05	ø	1.0	6.0	55.6	50.	~		.03	\$0.	10
7	12,3	07.067	•	1.0	0 ~	55.0	9	11.11		50.	03	3
3 -	2.00		7077) c	5. 2. 1	•	• ·			5	3 :
- 82	12.34	141.04	62147.30		00.7		ייייייייייייייייייייייייייייייייייייי	0 3 > 7		9 6	9 0	7 7 7 7
! ! ! ! ! !				•	•	•	•	•			:	,
- 611 PZ- 1 0.	0,0	29.862-	2541,26	5.07	10.	181.08		4 1		80	000	
7	07.274	0/*0400	20,4741	2 3		0 1	<u>و</u> و	16.55		900	0 0	140
21.	675.9	-2570.87	-	?	0	2	•			9		
ξρ ξρ.	4 6/2.9	-2570.45	^	.	Ο,	1.0	•	C		90	90	•
- 812 PZ- 1 0.		1794,24	~	4.1	9	3 •	2.7	7.		.07	.07	7
7.	!	1936.04	_	4.3	•	34.0	2.1	8		0	0	~
10.6	٠ ي	2074.41	7.50	∹.	•) :	2.7	æ 1		0	.04	~!
	75. 55. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5.	24.044	40.00 TO TO TO	0 1 0 7 8 1 7 7 1	7001		9/ 9	•		0	60	.179
D	ţ	ac - ac >		•	•	•	•	-		,		0
- 804 148- 1 0.		74.52	166.19	51	č.	5.7		(11.	-	160.
•		14.5	רַ י	4	•	, ,	٠,	•		, .		
	2.66	-14.57		100	32.	67.5	7 .	30			22.) O O O
77	2.5	•			~	7.	•	9		2		112

2	GRUUP AND SECTA	F 20 F 7.	3000 3000 3000 3000 3000 3000 3000 300	TOPENT	MUMEN! AZ	SATE AT THE STATE OF THE STATE	FUNCE PER PLANTE	TORBLUN	AXIAL STRESS	BENDING Y	STRESS Z Z SASION	WOUTH THE SECOND	SHEAR SHEAR SHEES	COMB. CALTY CHECK
503- 906 2	260- 1	0 3	•	-315.52		0 1	- 0			0 1			0	2 t
		;;	201.e	110.72	E 3	, i	, r		, v.	n 4			70	C CC
i	i	59.6	-201.47	122.50	133.54	50	** 36 *1 . 30	.72	5.30			200	20.	595
204 - 405 1	1000	2	, .1.¢	91.6		. 3	ာ		Š	0		, •	~	2112
į	:	•	~	3	4	•	0	-	55.	3		-	12	3
		11.4	2 0 C	75.4	35,73		9 60	~ ~	ئ د د	2°5		- C		\$70°
1	:	. ~	6 1 6	4.12		1.51		• 🕶	52	2,34		- ~	4 Ň	122
804-906	1 -07	o •	-53,31	-11.00		7	.31	7.	1.5	9 H. 1 .		\sim		0
		ċ	-53.51	10.18	~	1.4	0.30	3	1.5	-		- 125	~	-
		•	15.55-	30.54	5	•	• 28		1.5	T • T		┛.	-	5
			55.56	2 C C C C C C C C C C C C C C C C C C C	9 1 9 1 9 1	51.	200	10.48	1.57	27.		0.4	c 4	.174
1	1	j	30.000	•	•		A 3) >;	•	1		4		•
5.5- 800 1	- A - A - A - A - A - A - A - A - A - A	0.	3 :	-27.45	5		92.	•	26	1.38		-		0
!	!	7.0	0 4 5	C 7 4 C	- 0	0 1	9 J	-00,/3	200	3 4			→ -	V 4
		17.1	. 7	3 6 6	•	. 5		•						
		45.8	7	108.79		D !	Ð	6.7	24.	2,67	!	-		15
805- 901 2	200- 1	0.0	115.46	500,21	510.11	5.34	-1.83	4	٥.	P C:		.37	.37	OX.
:	į	14.9		45,57	¥.	٠.		5.4	∍.	c.		~	55.	Ţ.
		X	115,45	-H0.27	٦.) :	₹,	ν. Σ:	•	£.		0	50.	7
		7.00	116.00	40.70	455.60	14.05	100	25.42	4.00 0.00 0.05	2,57		200	200	249
_ 400 a004	7.88	5	6.1.5	428.55		2	5.26	5	7	3		4	7	~
)	•	351.94	34.0			: =	3.00	`			٠.		、 、
	•	14.2	352,01	556,16	5.5	7	•	55.8	~	0		m	~	•
	j !	26.5	352,04	155.18	191,11	3.52	90.6	355.68	4.70	5.9 8.0		50 50	. 50	282
016-010	.2.	0.0	12.34	-54.19	-<147.30	-6.53	1.7	7.4	50.	0	•	•0	00	7
	,	9.1	12,54	46.091-		٠.	1.7	57.4	•	•	;	0	c	Λ.
		10.2	30°00	365	915.5	5	7.	57.4		3,6		0	90.	$\frac{2}{3}$
		36.4	12,34	25.750-	316.66	66,53	1.70	-57.45	 	. 35	:			9.0
611- 911	1 -24	0.0	672.	-2370,01	7.2	7.	6.0	96.4	٥	1.04			~	Š
ļ	1	T.	6/5.	-1504.63		~	7	82.9	٠	Š	1	-	_	7
		7.07	6/2.43	40.45.A.	1123.14	2 2	30.0	20°000	E 0.0	2 5		7	51.	D 4
						•	•	•	•			•	•	•

Ť

ACTION CONTRACTOR DISTRIBUTION CONTRACTOR CO

SEESES. RECOUNT. EXCESSES

STRAN MEMBER OFTAIL REPORT

U.S. NAVY - ACMH PLATFORMS - FAITHUE ANALYSIS - MLW 105.0 FEET LUAD_CUNDITIUN NU.

20 ← CI	3.	 - -	<u> </u>	10	2	·	~	~	 	•	7	6	- 4 5		~	ស	.			0	74	<u>.</u>	∵ a	D.	Š	<u>ح</u>	.	0 ec	4		? ~	0	٥	~	3	•	20	~
C C C C C C C C C C C C C C C C C C C	8.			-	71.		0.7.	•	-614	v	V	v		•	0	0	•	•	•	~	. 1	~		•	~		~ (č		0	0	0	5	3	•	3	0
2 SHEAK STRESS	=:				-	-	• 15	~	~			-	N 0	,	. 30	12.			7	Ñ			9		5 5 4	7.0	٥:	. 23			90	0		00	90	60	31.	11.
Y SHEAK STRESS	=:		•	-	-	0.1	15	N	N	910	~		N	J	30	7		2	7	2	-	-	9.7	v	~	~	ο.	23	-	• •	90	0	-	0		0	01.	
STRESS Z Z SWITTE																																						
WENDING Y		- "	. 3		2	ε.	_	-	-	1.7	-	0.	7 7 7) •	~	so.	•			ň	o	Ň	97.	•	~	£ .	7	1.62				£	٠,	~		~	.15	
AXIAL STRESS	87.2		2.7	2.7	`	`	74	7	~	2.2	2.2	2.5			.01	ə 1	5	5 5		~	~	٠.	3,55	•	3.6	3.0	5.0	30.00	•		.57	ż.	Υ.		3		~ o •	
TUKSION	184,53	 E •		4.5	7	4.7	94.76	7.		14.7	~	14.7	<u> </u>	•	211.8	2119	10.11.04 10.11.04	711.6	0 4 4 7 3	16.5	18,5		110,50		13.7	13,7	15.7	-13.74		•	56.0	•	•	۰	•	•		•
UNCE/ F.2 N.I.P.S	55.6-		5	9,5	ŝ	3	37	٣.	~	0	500	0	9 9		57.	S	0 4	5		٤.	~	9	• • • • • • • • • • • • • • • • • • •	٠.	-	ا	ė 4	-1.14	-	. 0	50.	-	Ň		0		41.	
A STEAM	97.	3 3		3	3	4	1.07	~	•	v	3	٦.	^- ^- 20 ^- 20 ^-	•	~	4.1	004	. 7	•	Э	Ð,	'n.	0000	•	~	.	₹-)) ·	1	1:1		7.	26.	٥.	Э.	•		20.
HUMENT / HAZ	208	1117.86	072.7	÷	N	m	105.47	13,3	٠,	~	£	3 :	20000	•	ě.	21.5	10.000			12.0	01.6	2.7	40°24		4	•	> =	147.38	. ^	2.3	1	7	J.	~	•	S	_	
MOMENT BY IN-KIPS	2504.58	7 0 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-415.75	Ð	42.10	56.44	3	0 7 0	- 30.70	-<1.07	ď.	-27.19	44.00°		-212.41	-164.59	100.45	45.45	`	134.54	1,84	77.77	74.10	•	-91.76	11.99	05.45	01.00	200	55.45	.34.14	-65.69	71.7-	-5.45	-8.3B	-5.18	40.5	18.14
2 4 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	58.659	Č X	A 40 B	T.	-17,40	-17.90	-17.90	-17.90	-17.90	-55.73	-55,71	•	10.00	•	•	9	70.	400	•	91.99	42,02	\$0.24 6.04	00.00	•	95.05.	76 65		56.64	***	13.85	-15.85	-13.83	-13.85	92.	. 45€	92.	19 °	97
# 1 2 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	0.1	1001	۲	52,4	0 0	3.0	`.	0.0	•	0.0	5.0	15.7	2 × ×	•	0.0	-	7.01	56.4		•	001)	!	0.0	0.0	1.13	E 0.	! = = :		13.7	9.07	•	0.0	•	15.7	9 0 7	A / .
6 K C C C K				1	1 ->01				:	104-1	!			i	1.4. 1	1			1	140-1				:	180-1								1	104-1	; 1			
AEMBER C	815- 918				901- 902 1	,	 - -			901- 904 1					901-1001					901-106					901-1004	1			. 500 -206	•	-		:	902-404				



THE PARTY SHEET SEELS

PAGE 117 DATE 10/ U.S. NAVY - ACHR PLATFURMS - FATIGUE ANALYSIS - MLM 105.0 FEET LUAD CUNDITION NU.

	G. 1.1.1	70	Buare	MOMENT.	ALIME ST	7	/ 53611	TOMOTON	Z X	HE NOTE OF	-	- ia	V LI W	
NORMER A	0.4	2 2) X				7.4 1.5	ž			2 2 2	STRESS	S14ES8	~ L1 ~ ⊃
	St C 1 2	<u>:</u>	KINS	INSKIPS	IN-KIPS	KIPS	A1P9	INSTINS			I B H	i		4.4
405- 405	104-1	•	-5.88	4.45	æ	•		2.0	3	7			~	N
		•	-5.Ad	-10,74	4.5	74.	10.	-2.07	3	-, 39		13	.15	051
	!	13.7	-5.80	-1.11	٣.	•		ر د د	4	ે.			0	5
		40.5	¥.5	00.5-	* •	30.	Õ	2.0	₹.	~			-	4
		27.4	-5.87	5.18	•	1.09	0	2	3	•			. 122	Ñ
403- 405	104-1	0.0	0.0	4	2.1		0	2.3	•	14				5
		•	0	•	75.4	. 3	C		. 20	0			25.0	
	!	15.7		49.14	7.7	. 7			2		ì		0	: =
		9.07	•	-37.57	2	. 3	•	2.3	2	3			0	15
	!	~	0.0	-20.30	34.70		45.	2.3	2.68	3		90	0	152
001=100	- 60%	3		1	u	4	4	7	7	4			٥	40
	1		20.20	27.71				. 1	•	- :				
		-	10.50	27.0	¥ .		١ ٥	. 4		• -			• 0	7
		51.7	71.57-	-11.20	/5	3	~	4					•	22
ļ	;	45.2	-43.18	-67.31	121.33	-2.06	09.	8.49	3.5	01.10	!	5	5.	Š
. 2001-206	JL 90 1	0.0	65.02	495.49	404	-	2	5.2	~	-			•	70
			200	50.50	2		,	85.2	. `	-				•
	!	~		-55.48	20.30		- 510	185.20	92.			114	,	110
		3	S	- >	٠.	3	•	A5.2	~	. •		71	-	5
!	:	32.4	Ş	261.61		1.27	2	85.2	7	7	!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!	. 22	22.	~
903-1005	180-1	0.0	-170.44	1124.03	7.6	Š	N.	2.5	5.9	æ		.21	~	3
		•	4	2	59.0	3	¥	1.5	5.0	Š		91		0
! ! !	: 	-	0.5	36	E. 3	7	-	1.5	6.2	3		21.	15	3
		21.7	-170.31	=	15.04	£7.	9.5	21.51	-6.40	• 10		1.4	, 14	.374
1	:	·	٥.	-100.50	7.0	•	~		N	•		9.1	9.	0
506 - 506	1 -401	0.0	•	77.0	,	~.	•	1.7	3	0			N	0
		5	£	64.9	11.05	n	٥.	1.7	3	3				30
	i	15.7	5.6	3.05	2	Э	₹.	1.1	.47	~			0	9
		0 ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° °	5.04	9,	6.22 20.04	79.	* O	-1.79	. 64	12.		.	~ ·	160.
			•	,	•	ŀ	•		•	•			د	•
006 -006	1 0401	•	~	٧.	3	~	62.	٠,	2.4				3 C.	3
		•	m	7.	4.7	9	42.	٠.	2.4	٦.			-	3
		13.7	-50.31	27.18	11.00	9	62.	12.56	-2.46	1.1		.13	. 13	112
		• •	Ä	•	•	2	2	•	, c	7			60.	N
	!	•	92.05	·	2.5	_	62.	~	∠				~	25
405- 406	100- 1	0.0	62.27	-20.04	95,0		05.	5.1	\$	0		00	0	•
		ò	٧.	7.53		`.		5.1	ŗ	7		01.	0.	2
!		~	~	25.02	45,10	5/0-	3 .	-5.18	2.56	2 5.		• 10	2.	.140
		.	2.5	3D '		`•			ŗ.	\sim		010	01.	~
			70 04	27 70	•			•	•					

7												
	181							;		>	7	
	ָז בַּ זְ) k k k k		- 7 - 7 - 7 - 7 - 7	7	ביי היי	n x		FUDING BIRES	n w n	SARES	200
,	F.T.	A I PS	Set year!	SALK-NI-	201X	BAIV	Selveni		IOX			
180-1	0.0	100.70	104.18	166,58	4.6	70.	1.2	٠	~	02°	N	7
	9. 0	20.001	14.56	•65.51	7.1	•	7	•	Ŋ,	-	70	0
u ~	•		60.01	10.00		70	, .	• 1	V	100	0 (v
	46.6		53.47	145.60	-2.13	.59	-1.45	9	1.30		117	. 224
180- 1	0.0	¥.0	131,54	64.3	Μ.	S	•	~	1	.15	.15	3
	0.0	9.8	-6.35	51.1	*		7.	¥	7	60	0.0	33
~ `	-:	3	-45.53	٠,	٦.	- :	6	~	3	500	50.	30
1	42.2	170,84 170,85	17.41	20.18	0	1.55	7.42	6.21	1.48	15	010	389.
	•	=	1		•	•			, •		: 1	
•		19.47	20.56	30,700	1 to 1 to 1	7000	115.77	9 7	7 9 4	7 7	77.	
	:	•	242.97	M		! 7	15.	ıv	···		:	0.42
v	;	•	110,51	3	•	3.0	15	~	. 1	6	51	200
٠	~	•	-501.48	3	2	2		~	.39		92	200
7 -5 - 1	٥•٥	7.3	_	6460.14	~	5.3	57.4		7	_	-	V.
		2,3	v	4415,82	-	3,3	7.4	Э	0	1010		5
~ '	2.0	12.33	977	3171,45	17,92	-5.33	-57,43	50.	1,32	.16	•	.058
· ·		٠, د د	9	1427.00	٠,		57.4		e,	9 :		N.
	v	•	>	-31/16	-	2.5	3 / s		~			~
r 3- 1	0.0	672.48	6359.5		11.0	1.1	3.5	٥	•		.23	.250
		200	27.27	25.0077	20110	61,14	•	404	0 0			∿•
• ~	, 3	•	156.0					•			2	201
٠ :	~	0	_	11111.67	11.6	1.1	183.51	2,08	10			152
r -5 4	6	68.644-	5972,05	1450	-4.1	18.7); (7.5	2.6	_	_	7
	0.1		•	1744.	1-2-1	18.7	2.	2.7	Σ.	-		7
·	2.0	ς :	ā.	1 4 4 4 6 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6	-2.1	16.7		2.7		. 19		£
u •	7 7	DE . D > C	*************************	-1027.60	14.11	10.70	184.55	\$/.Y			-	7 £
	•	-	7			•	, ,	•	٠.	 		
>		4 7	100.00	63	E7 .	02.	13.67	3.26	10.10) e	120
	, 0.0	44,1	3	S		_	5.0	7.5		•	: c	250
~	0.7	12".1	35	50.4	1,51	~		3.6	•	1.	-	. 243
~	\sim		-102.59	٠	•		3	3,2	•	5	-	~
200- 1	0.0	117.79	-170.57	117.77		9	7.7	~	~	.15		-
		117.70	-112.51	164.72		00.	34.43	3,10	1,12	113	13	100
~ ¹	Ð	117.75	54°55	139.06	30,	39.	7	3	4	•	•	•
	₹			34 34) () : • :	•				` ;

\\...

RAN MEMBER, DETAIL MEPORT

PAGE 119 DATE 10/05/70

HENNEN GROUP	FROM	FURCE	MUMENT	MUMENT	¥	FURCE/	TURSION	YIY	BENDING ST	SHEAR	Z HE A	31
NUMBER AND SECTN	F 70	X X X X X X X X X X X X X X X X X X X	INSKIPS	8dI WeNI	» A X	6dI¥	Ž	STRESS	Y 2 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	STRESS	STRESS	CHLCA
1.02-1003 200- 1	0.0	3.01	40.40	-74.06	٥.	7	2.1	0	30		~	~ 3
	0.0	3.01	59.8	₹	. 41	7.	54.7	20.	920		024	-
:	ø	3,01	-24,18	3	V	4	4.7	3	3		_	50
	2 4 6 2 4 6 3 6 6 3 6 6 3 6 6 3 6 6 4 6 6 4 6 6 5 6 6 6 7 6 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6	3.01 10.01	-105.45	15.08	1.10	07.	-52,71	80 80 0 3	4	910	91.	0000
	İ				•		•			t	1	
1005-1004 140- 1	0	01.	-109.67	67.5-	•		7.5	.01	0			Œ
	20.	01.	-53.75	•	•		5:	10.	•			3
	•		75.5	20.	•		. ·	၁ :	٠,			0 0
	25.0	2 2	114.01	52	55	26	17.57	55	2,15	,	24	160
1002-1005 140- 1	0	04.4	-H4.27	-01.67	•		7.3	٥		62.	20	=
	0	07.0	-56.44	27 6	7.	~3:	7.3	•		414	-	~
	₽	04.0	-20.00	32,06		.35	-7.30	. 60	72	11.	.11	• 066
	3	94.6	11.24	7.42	ζ.		7.3	•	~	21.	.14	3
	•	54.6	45.04	-67.12	7		7.5	٥	3	020	N	0
1003-1005 200- 1	•	129,75	-245,72	-176.08	•	0	٠,	4	٠.			~
		129,75	145	-116.64	9.	0	~	7.	0		90	2
	٥	129.75	-04.77	.57.2U	•	1.05	4,55	3.41	. 41	90.	0	.175
	•	129.75	55./1	2.54	•	0	~	.	•		90.	~
	•	169.75	156.19	61.58	•	9	3	ŧ	9		C	0
1004-1005 140- 1	1 0,0	3.	55.48		•	~	٠.	0	₹.	.22	.22	0
	0.0	٠,	41.54	11.04	7	۵.	7.0	٥	30	•	•	3
	15.0	45.6	17.81	_		., 25	-10.78	00.	99.	.13	.13	0.00
	0 7 7	ŝ	л.	6.17	.	4	0.7	Φ	-	.17	-	3
-	36.0	Š	10.62	۲۲.50-	•	V	•	Ð	~	83	~	حد ح
1004-1006 200- 1	1 0.0	7	12.40.	-	-1.5	\$5.	28.7	•	9			9
	3.0	19.4	43.44	_	£.	95.	28.7	š	٠.		~	S
	16.0	-19.45	21.29	45,76		95	-28.74	51	.,55	11.	11.	.050
	3	3.	76.57	_	•	.58	20.7	S	·.		.13	•
	36.0	09.61	131.65	-55,74	1.5	128	26,7	Š	-		. 010	•
1005-1006-200-	2	-105,26	7.70.	-59.40	\$ •	06.	~	2.1	£	.01	0	~
	0.0	-105,26	9	_	\$ ·	06	7	2.7	c.	20		•
	0	-105.26		44.35	4.04	06.	4.18	-2.17	- 50	.07	.07	.215
	64.0	-105.26	164	3 :	.	06.	~	2.7	٥.	.07	0	M
	9	-105.2b	751	S	•	50	•	•	4	•		4



GE 120

U.S. NAVY . ACMA PLATFORMS . FAITCUE ANALYSIS . MLM 105.0 FEL

LUAN CUNUITIUN NU.

FAGE 140

MERSEN GROUP NUMBER AND	F F C	FURCE	7	-	HEAR F	URCE	LSHO	AXIAL	HENDING Y	STRESS	SHEAR	SHEAM	CC48.
SECTA	• 1	F 1 P 9	14-KIPS	INSTING	na! ×	KIPS .	SATHAL		i	K & X			CHEC
U1- 102 #18- 1	•		11		٥.	00.	0		c	•	0	0	00
	•	0	10.	3	•	-00	9		0	0	0	3	9
	• ;	0	3 :	~	? :	300	9		•	਼	0	0	9
	> v	3	9	0 1	5 : • (0 3	9	9	•	-	00	e e	000
•	•	•		•	•	200	>		>	>	>	>	3
01- 104 -18- 1	o. o	00.	10.	1.	•	0	0	9	Ç.	•	0	0	3
	4.5	000	Co.	3	~		Э	00.	°.		0		C
	•) •	2	N:	•	0	9	00	0	•	0		0
) · ·	9 6	V = = = = = = = = = = = = = = = = = = =	\ 0 •		•	9 9	•	0	- ;	000	0 0	000
	•			'n	•		>	00.	3	>		>	⊑.
01- 201 DKL- 1	•	90.	90.	-	2	0	Š	9			0	00.	C
;	5.8	00	05.	1	.	0	S	00	0	,	0	00	0
	~))	60.	9.0	70.	10.	-1.52	0	000		00.	00.	000.
		0	29.1.	• 1	:	9	'n,	9			•	0.	Š.
	•		v	C	100	•	ĵ	00	0	!	C	00.	0
02- 105 m18- 1	ů°ů	.01	5 n •	Ñ	00.	00.	2	00.	00.	0	00.	0	00
!	9.5		•	-	22	900	3	000	0	0	0	0	C
	5° ,	0 ') 	0 0	20.	000	0 :	00	0.0	00	00	000
	0.0		→ •	•	9	00.	?	00.	000	9	0	C	0
	3			•	000	000	2	000	00	੍ਹ	C	C	9
32- 104 #08- 1	0.0	•	•	9	00.	c.	3	٠,	C		Ç		3
1	5.0	200	つ :	c, e	000	0	>	3	0	0	0	0	(·
	• :	ູ	• :	•	3.	e,	0	•	•	•	0 (0	0
	10.5				•							0 0	
i : :		•	•	•		•	•			•	:		•
05- 105 H05- 1	0.0	.01	000			0	3	00.	00.		C		3
	•	0 0	> =		> :		o :	Э:	000	0	0		C (
	• 0	, c	> =	ò	• 7	> c	•	> =	•	> <	> c	> <	
!	•	5	00	Э.)	30	9	9	00	5	00	00	100
03- 105 #18- 1	0.0	0	02.	M	_	•	0	2	0	505	00	00.	0
	5.6				22.	0	0	2	00	50	00	00	C
		.01	3	•	00	90.	00.	00.	00.	~0•	00.	00.	0
	6 0 0	0	•	•	0	0	0	•	0	.01	00.	٥ •	
	₹	•	20.		000	0	9	•	00	00	000	C	Ç
03- 203 DAL- 1		٠.	17	2		90.	99.	•	c		00	O	C
		٥.	.15	×	00.	0	Ð	•	•		C	C	0
	~	200	_	70.0	3	20.	99.	00.	00		00	00	000
	•	•	50.	Š	3 ·	90	98.	•	٩		٥.	0	C
	•		٠										

U

TRAN PERSER, DETAIL REPORT

PAGE 122 DATE 10205/76

U.S. NAVY - ACRR PLATFOX48 - FAITGUE ANALYSIS - MEE 105.0 FIER LUAD CUNDITION NU.

36336 2336 30336 3	1 0 E	 	TURCE TX SX	ACHENT BY	HUMENT	2	14CE/	CKSTO	A F	ENDI	TRES	STEAL	SHEAR	C S I T
	2 2	•	SATA	Catvent	04 14 14	0	_	•				ĺ		ر
205-203	1 -014	0.0	-	\$ 0 0	M	000		•	2		0	ō	0	00
		9.		71.		つ :		•	•	.	9	ā (0	0
		•		٠.	- ×	> :		•	•	9	•	ō	> •	3
		14.5		•	, T.	•	•					•	9 0	700
		•			•			•	•	:	•	>		
707 -20		0.0	00.	10.	C	00.	0	2	٠,	c.	3	0	9	S
	;	3.0	700	00.	=	3		2	2	٥.	Э	0		c
		٧.	.00	20.	0)	0	2	•	°.	0	C	0	>
		6.01	00.	00.	02	05.	00.	00.	00.	00.	00.	00		9
!	:	14.5	00**	00.	=	-	0	2	2	Ç.	<u>-</u>	C	0	ခ
205 -50	1 -60+	•		10.	0	2	0	9	9	0	0	0		0,0
	!	5.5		00	9	7	9	3		0	3	0	00	•
	!		O	22.	1 03	00.	30	00	00	90	3	00	00	9
		10.9		200	50°	٦.	٠.	•		0		0	00	3
1		24.5	101	000	-	<u>ء</u>	2	3	>	C	Э	C	00	60
cs- 205	118- 1	0.0	90.	2	3	9	0	0	9	Ċ	á	C	c	9
		5.5	0.	17.	~)	2	9		C	5	C	20	0
		7.5	00.	.15	.17	9	90.	00.	00.	00.	-02	00	00.	00
		* O T	•0•	9	0	2	•	0	0	0	Õ	0	00.	3
		` 14.5 -	90.	-0.04	0	⊃`	•	9	9	¢	0	0	000	9
15- 503	505 UNL- 1	0.0	70.	05.		•	~	~	٦.	c.		C		000
1		•	70.	5.	4,3	٦.	٦.	٠.	2	c.		0	0	9
		7.5	# D .	•	£ .	7.14	-, 12	05.4	00.	. 0.2		10.		00
			70.	•	m:	7.	7	٠,	.	•		0		-
:	i i	12.0	70.	-51.71	δ. Σ	-	-	٠,	?	Ċ	-	C	0	Э
3- 306	120-1	0.0		₹0.	I	5	90.	-		c		00		٥
,	1	5,6	10.	5		9	O	-)	0		C	30	
		10.5		20.	7	3	30.	-		0		0	00.	0
•		64.5	20.	21.	-1.62	V :	30°	. 10	00	.03		00•	90	00.
		, 100 i	- 100	A1.	7.	Š.	000	-		Ō		0	200	Э-
34- 205	100.	0.0	.01	00.	0	?			•	0	0	0		0
!		200	0	0.0	c	٦.	٩	9	~	0	0	0		C.
		7.5	\sim	27.	70°	00	9	000	00.	00		00.	00•	00.
		0.00	10.	•	:	•	9	0	•	0	0	C		8
			10.	000		•	0	•	•	್ಥ	0	C	000	100
34- 200	110-1	0.0	70.	30.	•	10.	0	?	•	C		0	00	0
1	i	•	70.	17.	_	Э.	٥,	3	•	°.	0	C	00	
		~ .	~ .	•	21°		3 · ·	00.	00.	0.	•	00.	00.	00
		•	~ .	3	ñ.		•	3	2	•	•	0	00.	0
			30	-	-			•	:					

STRAN LEFFER OFTAIL PRODET

205- 206 125- 1 0.0 205- 206 120- 1 0.0 205- 206 120- 1 0.0 205- 306 125- 1 0.0 301- 306 125- 1 0.0 301- 401 04C- 1 0.0 301- 401 04C- 1 0.0 301- 401 04C- 1 0.0 301- 401 04C- 1 0.0 301- 401 04C- 1 0.0 301- 506 125- 1 0.0		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	A L L L L L L L L L L L L L L L L L L L	1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			XIAL -	HENDING	814538	V BHEAR Stress	74	
05- 600 m10- 1 05- 600 m10- 1 06- 501 160- 1 01- 500 165- 1 01- 401 046- 1	M C C C C C C C C C	7 ; 5 X	S SCHMA NEED		7			>	•	7158		
05- 206 m13- 1 06- 301 120- 1 01- 303 125- 1 01- 401 044- 1 03- 306 125- 1		11111	DC-M3 NESO	၁၁ :	8474	20 X X 20 X	x •	-	2 ************************************		701410	Creck
01- 301 160- 1 01- 303 165- 1 01- 401 046- 1		1111 111 1 14W 	CHW3 NESO	Э:	0	•••			•	00	00.	C
01- 301 160- 1 01- 303 165- 1 01- 401 046- 1			-Ma NEGO		٥.	0		٥.	0	0	<u>ء</u> د	
01- 301 160- 1 01- 303 165- 1 01- 401 046- 1			Ja Nitao		0	3		0	9	0	0	Ų,
01- 301 120- 1 01- 303 123- 1 01- 401 044- 1 03- 306 123- 1		111 1 Mare 	N K 3 C				9 9		999		0 0 0 0	N N
01- 501 163- 1 01- 506 165- 1 01- 401 046- 1			N # 3 0	•	•				•			
01- 303 125- 1 01- 303 125- 1 01- 401 046- 1		111 1 14W	. 4 0	.	٠	3 :	Э:	e :		0	0	Ċ,
01- 303 125- 1 01- 303 125- 1 01- 401 046- 1	သွော်တာ လူလူလူလူ • • • • • • • • • • • • • • • • • • •	11 1 14W		> =	: :	* 1	> =	9 0		> 0	3 5	. () c
01- 308 125- 1 01- 308 125- 1 01- 401 046- 1		4 5 7 4 7 5 4 7 5 4 7 5 7 5 7 5 7 5 7 5	•	• •	00.	2 3 4	9 9					. C.
01- 303 165- 1 01- 303 165- 1 01- 401 046- 1	¢ c 3 c c	, , , 4 k 2 9 t s 2 k 2 9 t t 2 k		3	0	7		500		0	ن ن •	0
01- 303 125- 1 01- 508 125- 1 01- 401 UAL- 1		5 4 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	55.	60		-	09	00		6	00	C
1- 303 125- 1 1- 500 125- 1 1- 401 0xL- 1 5- 300 125- 1	200	6.53 8.43 8.43	-			7)	00	!	00	C	5
1- 303 125- 1 1- 500 125- 1 1- 401 0xL- 1 5- 300 125- 1		5.45	•	Э		-	00	10.	!	C	C	
1- 303 125- 1 1- 500 125- 1 1- 401 0xL- 1 5- 300 125- 1		J.	1.0.1	•	70.		000	.01		0	00.	106
1- 503 125- 1 1- 500 125- 1 1- 401 0xL- 1 5- 300 125- 1	•		·.	¢5.		~	00	76	!	6	C	۲,
1- 500 125- 1 1- 401 UAL- 1 3- 500 125- 1	•	64.	3.2	10.0	90.					0	000	C
1- 500 125- 1 1- 401 UXL- 1 3- 500 125- 1	.	17.		10.0	00	٦.			; ;	0	000	ာ ၁
1- 500 125- 1 1- 401 UAL- 1 3- 500 125- 1	•	45.	1.7	•) 0	=					3 (•
1- 500 125- 1 1- 401 UAC- 1 5- 500 125- 1	> ° °				9 0		9 9	0 0			9 9	V (0)
1- 500 125- 1 1- 401 UAC- 1 5- 500 125- 1	•		1	•		•			*			
1- 401 UKL- 1 5- 306 125- 1	6.	3.		•) •		9	50.		9	30	200°
1- 401 UAL- 1 5- 300 125- 1	1	27.	7 1	> :		v		9 0	-	2 0	• •	<u> </u>
1- 401 UAL- 1 5- 300 125- 1	• '	•		, ,		5 7	• (, c		•		: c
1- 401 UAC- 1 5- 300 125- 1		11.	¥.			07	000	6		20		103
5- 500 125- 1	•	3.50	7.3	64	.03	17.7				20.		٦
5- 500 125- 1	-	1.05	3.4		C	17.7	>	0	;	0		
5- 30e 125- 1	-	-1.45	700	Y	•	1.1		0		0		0
5- 50e 125- 1	•	27 ° 5	-	•	900	_ :	0 0	20.		25	~ .	500
5- 506 125- 1 0.		•	, ,		-	•			, ;			-
7 .	•	۲۶۰	3,65		c.	~:	3	0			00.	3
,		920	1.80		2 0	 .	2	c,	i) (0
		C.	•	> :	•	-	5 :	9			<i>-</i> •	9 0
C - 7 V		5	70.2	77	00.	61	20	101	1	0		
-			1	•	•	•	=				•	
· · · · · · · · · · · · · · · · · · ·	•	7.7	13.67		-	* 22 ×	• •	6		~	20	000
2001	6.			~	•	~	>	Э	!	2	0	C
21.12	o •	2.5	•		11.	~		. 10			7 0 •	0
₹. .	•	\$0.12	-64.17		11.	Ž		<u>.</u>	•		> 0•	(1)

T)

TEAN SETBER DETAIL SEPOST

124

PAGE UATE U.S. NAVY - ACHK PLATFUNG - PATIGUE ANALYSIS - MLH 105.0 FEET LUAD CONDITION NO.

MERHER GROUP WUNNER AND	. 7 . 2	FURC	HOBENT	1244	E in .	1 2	CKS10	IA	BENDING	81RE	SHEAK	SHEAR	CONK.
SEC. 1	- Lu	8 1 L	- 241X=21	0414171 ·	344X					******			ټ
140 BOT - 400	-	•	7.13	3	-		٥.	0	50°		0.0	0	00
	7.1	,	-5.41	ŗ	-4	~	0.7		- 100		10	2	0
	14.2	c.	77.25	-13.40	.13	•115	10.76	9.	70°		0.0	.01	7000
	41.4	•	-30.58	3	-	~	7.0		90		٥.	c	0
	49.5	•	-45.19	~	-	~.	٥.٧		60.	-	- 10	•	9
01- 501 JE4	. 1	11.54	30.09	0	~	~	30	0	0			C	0
	-	5	-	^	. ~	~	2 97	100	. 0		٠,	•	
	•	5	45.51	9	~	2	48.5	• >			. ~		90
	7.5	11.54	27.20	-17,55	27.	1.27	-46.54	30	10			\ 0	000
:		1.5	100.54	3	7	2	8.5	∍	0		50+	- 0.5	20
14 015 -10		-	55,15	-	•	9	2	=			Ş		5
			17.13	7		0	7	• ?	• 6		100) a
	2.3		00.7	-21.11	10	1.05	20.22	35	.0		20	0	500
	•	~	-11.58	Ð	•	1.0	6.6	· •			9.0		0
:	Q • 7	-11,35	-25.4h	5	•	٠ •	6.2	-	Ċ.		+05		9
03- 503 JL4	. 1 0.	160.21	94.54	T.	٥	~	4.5	•	0			20.	~
	1,1	5.6	101,16	_	٩	~	4.3	v	C			0	3
	2,3	45	•	15.54	.03	1,23	44.57	.50	70.		20.	50°	. 025
	3.4	66.8	3	٥.	٥	~	4.5	v	0			20.	3
-	0 7	126,21	151.04	2.	٥.	2	. J	v	90.			- 05	Λ.
05- 511 P1	. 1	-124,39	-23,50	~	3,	5.	21.6	Ţ	Ç.				20
	1	25.3	EA 050	3		7	21.0	٦.				0	2
	4.3	44.	-55.46	46,73	3.	-1.20	-21.60	15.	. U.S	i	20	50.	920
	•	25.3	76.	J	*.	1.2	21.6	Š.	ç.				3
1	•	-124, 59	27.64	~	7	2	§	J.	0				0
05- 506 JC4-	0	2.60	-38.46	79	~	7	5.7	3	٥		70.		2
!	_	600	-41.7V	٦.	1 . 1	2	2:5	3	Ç		80		20
	•	109,5	9.	5.1	7:	~	2.7	₹.	٠.		. 0.2		20.
	3.4	-109,57	16.56	20.33		52.	25.75	M 7 8	→ 0		2	200	200
	•		•	_	4· •	_		•	2		70.		2
05- 512 F1	. 1 0.	0.0	2	-11,30	7.	_	20.	05.	0		. 02		
1	1.1	2.60	2	~	1,4	1,5	20.4	S	0				V
	£ . 3	? >	`.	٠.	7.7	*1.37	76.02-	05.	5 0		2 0 •	20 •	0
	•		•	5 . 5	7.		٥٠ د د د	s.	0				N
	· ,	109.50	474.14	√	1.6		٠ د د	S					~
21- 502 165	-	•	4.19	າ	٠,		1	~	~			20°	
!	5.8	-5.0	2.54		., 50	10.	6/.	. 10			20	20.	5
	7.0	• \$ •	5	•	٧.	0	~	-:	٦.			C	
	711	0.5	٠.	⊶ (3.	0	•	-	٠.			~ 0 •	0
		•	•		•		۰	•	•			:	٠

LUAD CUPUITIUN NU	8,		IL.S. NAVY	• AC4k	PLATFORMS .	FATIGUE ANALY	YSIS - HE	105.0 FE	19:	0	ATE 10,	41/50/	
ADDITE SERVICE	1 1 2 L 1 2 C L 1 2 C L 1 2 C L	7 2 4 7 2 4 7 3 4 7	STER TO THE TERM T	1234UA 2	SHEAK FY KIPS	FURCE/	ST ST ST ST ST ST ST ST ST ST ST ST ST S	AXIAL STRESS	BENDING	SIRESS Z KSI	SHEAK STRESS	Z SHEAH STRESS	CCC CCC CCC CCC CCC CCC CCC CCC CCC CC
501-504 155- 1	010	2.52	2 7 7 7	125.90	54.	000	111	8 7 3 3	35. 10.	:	M M M	M M M	3 2 2
501- 601 JLS- 1		ง จำจำจำ	3 0 F 3 - 5	THE ORNE	~~ ~~~		ימממ	33 3333	0- 0000		CO COO	CC CC > 0	0 → 0 0 0 0 0
501- 022 200- 1		10 0000 10 0000	v o -				2 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3						0 000
502-505 105-1		/ www.w	0 2277-	5 2 2 2 2 2 2 3 2 4 4 5 4 5 4 5 4 5 4 5 4 5 4 5 4 5 4 5			•	?				0 20050	
502- 504 105- 1	0 x 0 x 0 x 0 x 0 x		7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	SECOND SECOND	3333 333		111	20000 MAM			00000 0000		N N O N M N N N N O N N O N N O N N O N N O N N O
505-505-105-1	0.0 0.0 1.1 1.2 1.3		V 2 V 2 V 2 V 2 V 2 V 2 V 2 V 2 V 2 V 2	at Novovo			· · · · · · · · · · · · · · · · · · ·		20000	<u> </u>		00000	
503- 603 JL>- 1	0 m 4 0	115.07	76.71 72.40 65.61 54.53 54.53	24.45 -5.47 -41.57 -77.40		\$2. \$4. \$4. \$5. \$5. \$5. \$5.	9 5 5 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9		00000				0000 0000 0000 0000 0000

PROPER JEANS ARBINE SAXES

ANDRO RANKSE	1810	W	FURENT	<u>-</u>	¥ 4	UNCE/	TURSIUN	X I A L	HENDING STRESS	≻ ₩	SHE A	30
	3 L	8 2 1 v	2012	4 IPS	× 1 × 2 × 2 × 2 × 2 × 2 × 2 × 2 × 2 × 2	841 X	X T	ESS	Z	8	2	CHECK
503- 625 200- 1	0	٥.	0.1	9.0	~	3	~		1	0		~
	s o	7,00	54.12	£ .	-	3 :	•		2			5
~	15.0	•	77.0	Č 3			~ °		c •	ō (5
; i	20.5	•	2	1.51	10		3.45	12.	.26	0.0	9 9	C10.
504- 505 105- 1		14.	2	• 39	7	C	_	3	9	•		5
		\$	~	-	9		•					90
			۶۵.	۲.	3	0	•	?	٠,	0		
	11.6		77.	20.	.01	30°	.17	50.	5 0 -	00.	96	100
	•	n.		e.	•	0	-	. ⊃.	•			0
504- 506 165- I	•		•	¢	~	•	2,5	2		0	• 03	-
	2.		`		ขา	9	4.5	3	0		• 03	S
	• •	•	04.7	7 7		•	יי ניע	ə :	۰ ۰	0 0	n :	က ၁
	· •	``	-3.62	-25.40	52,	20.	-2.58		25.	2 0	1 M	90
505- 500 105- 1	0			0	_	9	3	٥				
;	•	~	-2,20	2.5		•			•	٠.	u ()	•
	•	7.	٤. د	8.2	-		3	3	•	- 26	20	2
	7.7	1.73	45.54	#15.XG	21.	40.	1.55	• • •	.13	20.	7 0•	500
	•	•	,	٠. ۲.		•	Ç.	.	_	50.	₹6 • ·-	~
500- 600 JLS- 1	0.0	~	66,00	•		1.9	1.8	`:	٠.	0	C	
	1.5	1.0	-	7.0	3	1 , 9	2	~	0	0	, eq	•
	c ;	٠ د د	.	-54.51	. 4.	56.1.	21.45	75	.03	500	603	0.036
			*****		3 3	•	æ :		٠,	5 0	• 0 3	•
:		•	•	•		•	•	•	•	, Sc.	£0.	~
500- 624 200- 1	0	ე • <u></u>	-	4 S	7	~	7.2	~		\$0.	50.	~
!	ۍ.	ر د د	21.17		7		7,2	~	~	0	C	0
a.	.	10 1 C 0	VU. 5	7.7	₹.	2	7.5	~	•	0.5	0	00
	2007	5.06	-28.52	44,41	200	.,22	7.40		1.1	0 2 2		210.
510- 710 PI- 1	0		-45.46	3	-	3	^	9	•		•	•
		~	-57.74	1.33	-	. 7	9		• 6	1 0		200
-	∿ :	-11.35	E	544.24	-1.47	77.	20.40	50.	71.	~	95	600
	٠.	~ .	7.1.	43.7	<u>.</u>	7	٥. د	•	۶.	0.0	0	5
	•	?	-155.50	43.2	<u>:</u>	3	٥.۷	<u>-</u>	~	₹0•	9	0
511- 711 Pl- 1	•	-166.39	57.55	4.7	₹.	6	21.5	٠,	0		c	3
	•	~	u. 7	12.6	*.	•	21.5	•	٠.		0	•
	•	٠. د	`	000	.	2	21.5		• 10	20.	.03	0
	2 (25.07	2000	10 10 10 10 10 10 10 10 10 10 10 10 10 1	77	1.01	-21,52	15.			£0.	.039
	•		•	,		,	`	•				

STRAN MEMBER OFTAIL REPORT

0~00 040*	CU~0111U~ ~	دن. وي	;		19				c		PAGE 127	70/05/74	ı
				0000	ב ב ב	•		M1	103.0 75	-			
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	3 3	F 5 0 X 4		F 0 5) 2 4 4 1 5 2 4 4 1 5	X 4 3 1 8 1 1 1 1 /	FURCE sees	10 kg 10 k	×	OING ST	≥ 1 5 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	7 ×	•
T	A.45 8ECTH	F 7	# # X	Salvin	-	» ± ~ ×	F 2 A I A	X III	STRE 38	Y Z Z & Z	81	STRESS	CHECK
512- 712	1	0	v		107	3	0	5	: : :	_	_		_
	,	•	• >	2	48.52	0 0 1	6	20.48					200
		14.1	¿.	S	1. H	3.	•	200	Λ	. 🕶	O	0	^.
		· • • • • • • • • • • • • • • • • • • •	5.0	7.00	\$	3	٥.	5.0	3	710	0.0		₹3
		65.3	109,58	-573.40	•	•	0	50.9	v	-	0	0	?
631- 621	160- 1	3	1.5	14.42-	42.4	1.7	9	144.7	80.	0	. 80		0
,		•	1.5	0	54,5	1:1	1.6	144.7	Э		-		67
		•	٠ . ا	-45.	500	1.7		-144.7	€ O	-	90.		5
		۰ - ۵ ۵ - ۳	11.55	126.04	77.57	9/11	1 4 4	-144,78	5 5 5 5	9.1	3 0 50	0.0	010
,		•	•	0 • 9 6 •		:	C .	***	5		90.		_
635- 623	Jt 0- 1	3	14.1	•	15.0	₹.	-	14.7	09.	0	0.	90.	~
		 -	114.19	J .	-104.65	1.59	•113	114.72	00		90	90	050
		•	7 :	•	25.0	•	-	14.7	000	¢,	0	• 0 •	
		•		V 1	7	'n	;	14.7	0 (0 10 :	┙,	90	90	3
	•	ċ	7.	•	7.	^	7	7 4 7	0.0		90	90	IJ
60A- 626	JL0- 1	•	7.1	7.	6.67	3	۶,۷	9	`.	c.	70	0	5.0
	!	•	107.1	-154.77	56.7	3	2.5	0.4	`.	7	0.4		~
		→ :	5	01.461-	-54-16	. 4.	.2.21	24.01	\$7.	•.13	70.	70.	070
		•	107.1	-235.25	7.7	ო.	2) 			0		3
1	1	•	V	-673.44	•	-		o. 2	`•	-		0	3
621- 651	J.6- 1	Э		٠,	51.4	7.	1,5	145.0	Э	-	90		2
!	;	S .	\$		0.50	1.4	. 5	145.0	Э	2	0	0	-
		c (~)	5°5°		٠. د ،	145.0		~ ∶ (10	0	ີ່
		•	11.55	-264.30	414.47		16.1	10.041.	C *	د. د د	10	0.0	3 1
			•		•	,	•			4		>	→
h22- 703	200- 1	5	~	t 0 3	31 . A	-	-	٠.	٠	-	50.		5
	! !	•	7.7	∿.	· •	٠ •	9	٠,	•	۲.	20.	C	~ 0
) 4 	0 t		5.7°.70	07.		7.30	\ o •	02.	M (.	, o	015
		• •) <i>S</i>	` -	2 2		•	•	٠,	n •		5 6
:	:		;	1		•)		•	•	•	•	-
665- 655		-	7 S	50,64			Ó	3.5	D:	-	c (0	7
		•		20.10	0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	•	o c	2.0	D :	-	00	90	3 .
		•	• 5	01.07	7.1.76	•	• n	2 4		~ -	0 0	0 6	૩ :
		-	. ~	05.10	292.1	1 2	19.	115.02		- 10			
							1	•		•	•	•	1
101 -729	20D- 1	3	~ :	-26,55	٠,	~ ;	~	٠.	٦.	~;	70.	0	~
•	:	•	• c	1 ~	'n	. •		~ :	~; ·	~ 1	0		2
		•		_ ~		1 ~	2 0		•	٠-	n r		-
	•	61.9		45.66	-45.15	1.05	7.5		. 13	7 - ° 1			
				-			:	•					,

the third of the state of the s

Ť.

1

SIXAN ARABEX ORTAIL ARPORT

COTB. CHECK .021 .020 .020 .015 00000 00000 00000 00000 135 075 024 079 Z SHEAK STRESS 2202 82220 00000 50000 5000 22225 0 - 0 - N SHEAN 9 9 9 9 9 20006 00000 5 0 0 0 0 2225 22225 BENDING STRESS 200 200 300 300 300 20000 2.12 1.19 1.24 2.05 200 22222 2225 PATIGUE ANALYSIS - MLW 105.0 FEET AKIAL 1111 25.05.00 25.05.00 25.05.00 25. 22222 2 2 2 2 2 22222 2 2 2 2 2 187.15 187.15 187.15 135,13 135,13 135,13 135,13 102.56 102.56 102.56 20000 21.67 21.67 21.67 21.67 TUKS IUN 11.52 000 11.24 11.78 1.27 1.27 11.05 1.57 12.10 18.66 7777 - SHEAK FY FIPG 11.00 11.00 11.00 11.00 11.00 10.00 22223 8.17 8.17 8.17 8.17 8.17 8.17 E & C C C 13.50 13.50 54.63 103.27 17.94 18.21 10.51 5.10 1,29 -10,14 -13,58 -74.71 -77.73 -72.42 -02.43 261.74 266.00 145.51 01.55 -240,90 -241,07 -245,18 -245,37 -19. nd -18. So -10. US -2.55 78.51 584.81 685.80 SAI YOU' J.S. NAVY 37.85 1.85 -1.19 -112.55 -260.74 -273.17 -290.19 -313.74 -324.04 -317.75 -292.47 -255.55 156.59 54.45 -12.21 -72.22 -273.00 -500.80 -319.44 -324.05 134.11 53.41 -11.11 -61.02 -105.54 1107.20 -105.59 11,36 11,35 11,35 11,35 119.75 27.7.5 7.007 FURCE FAR FAR 50000 3 - 5 67.00 A 40 BEC 12 -002 710 100 FERSTR



المائد

KAN MEMBER DETAIL REPOR

020 020 030 010 107 076 077 131 2000 20000 11.72 11.72 12.72 12.72 2000 9 N 6 N 8 2.52 1.15 1.15 1.84 55 57 17 17 17 4444 23233 **** 22222 2222 33030 2222 00000 . 37 . 34 . 06 . 55 77.00.11 50 50 51 11.54 20000 00000 24244 2007 A C - A E 707 154.65 35.10 105.25 58.75 20.13 10.77 12.69 12.01 12.74 14.57 181.56 1827.90 1168.35 134.70 SOL XIN 10.00 12.00 12.05 12.05 111113 120.14 -10.14 -50.59 -23.37 203.55 500.70 313.42 112.40 230.57 130.08 -35.82 -81.14 -24.41 10.00 17.00 17.00 10.00 10.00 141.05 h0.85 -7.44 105.65 06.32 06.29 06.29 06.39 13.62 13.66 13.59 13.58 20000 85588 TUPCE FX RIPS 7 X C 3 F 7 C 6 F 7 C 0 2 2 2 2 O CONSTITUTO OF 6400F

FI . DESME OF												
CARTER CALLOY THEORY SECTION OF TO 157 1 00.0 CC 157 1 00.						1				>	7	,
SECTA FT. Cue 706 157- 1 0.0 14.1 13.5 35- 706 157- 1 0.0	7.09CE	HUMENT HV		**************************************	UKCE/	TURBIUN AK	AX TAL	MENUING S	TRESS 7	GIEAT	SIEAK	CCAB.
C4= 706 157= 1 0.0 14-1 155= 1 0.0	KIPS	8214877			KIPS				-KSI-			CHECK
14.1 14.1 13.5 15. 700 137- 1 0.0	1.63	-116.60	10.45	683	.57	~	90	0		.13		. 0.01
14.1 13.5 15. 700 157- 1 0.0		-75.03		~	•	7	00.	~	1	~	-	_
14.1 13.5 700 137 1 0.0	•	J.	4.3	3	~	٠,	\$	۶,		~	~	u
05- 700 137- 1 0.0) to 0	\$ 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	70.1	1.60	7.35	2 3	1.15		23.	2.2	. 122
35- 70e 137- 1 0.	•		•	•	•	•		•		•	•	
•	•	6.0 0	•		5	٥		0		916		0
	٠. •		0			ē.		ď		1	(0 :
	•	77. T	. ·	> =	7	ō 1	↑ ~	•		~	~	N J
	200	148.12	72	25.0	1.70	4.63	.51	2,62		. 72	27	.125
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		:			:	, ;		•			•	
	- C - C - C - C - C - C - C - C - C - C	0 3 7 7	ر ا	u -	7 0	* 5	``	vc		o c		છ ૩
2- 1.652	45.70	12.31	50.60	2	10	2.49	0	30		70.	20	C 17 7
7	-ch.72	25,36	0.3	3	C			~		0	0	
	۶. ۲	٠ ۲	2.	2	-,35	3		-		70		820.
•	43.5	173.55	6.9	2	2	9	1.5	-		22.	~	6.7
7.1	\$.	-154.40	31.4	•	6 P	9		2		-	15	~
~	•	-5111.40	-1111-15	.32	70	89.03	-1.32	-,42		90.	60	Č
~ :		291.48	- ·	Ð.	~	o :	2.5	٠.		-	• 10	.041
,	۲. ۲.	67.40T		.	•	•		-	İ	-	_	0
		-156.44	4	٥.	.77	. 0	3	~		0	.01	_
·	•	20.00	e i	٠ •	~ 1	9	3	25	1	10.	10	_
٧.	•	•	* *	20 :	~ 1	o :	• :	۲,		7	5	
1		104.50	2 C	• •	110		\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	920		0 0	.	510
		•				•	-	•		•	•	-
•	125.39	511.44	.	-	55.	21.	.50			0	.01	~
	70.04	75.35		• °	54	==	n s	r n	İ	0 0	- -	0.57
		574.05	3	•	52	21.1				> c	> c	֓֞֞֜֜֞֜֜֞֜֜֓֓֓֓֓֜֜֜֜֜֓֓֓֓֓֜֜֜֜֓֓֡֓֜֜֜֜֡֓֓֓֡֓֡֡֡֡֓֡֡֡֡֓֡֡֡֡֡֡
•	\$	545.46	77.1	9	.25	1:1		~	•	10	6	0 2 2
0.0	85.601	04.878-	4.6	7	06.4	900	- 3	-		2	3	1
7		20.054	S S	7		2	3	•		. ~	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	, ۱
	109.50	527	-	1.65	06.	60.02-	77	23		70	2	0.20
	•	1004.03		'n		20.4		\sim		0	0	~
7	.n	-611.01	\$0005	V		6.0≥			i		20	•
	~	71.41	4	Э	7	-	0	-7		-	-	
5.7	-1.25	27.44	-34.35	• 10	45.	6.19	50.	84.		~	27	0.51
7.	۲.	-6.74	1.5	v	3	~	3	•		-	_	0
-	~	10/5	\$. \$	3.	~	7	•	• •		~	~	9
E	`.	_	٤.	٥	2	~	٥.	ů,	:		•	3

 $(1, \dots, 1,$

ı





K.F.

Paser Groot	2 1 3 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	J ¥ ;	OMENT	UMENT R.Z.	HEAK F	74	01810 XX	AXIAL	BENDING 8	1 PE 55	HEAK	NAK	COMB.
200	•	2 L → C 	2	2	ZY IX	מ	2						7
904 1400	0	10.22	2.2	-39.93	•	0 ·		87.	1.59		. 1 1	. 1	\$ 0 °
. !	2.4	201	70 77	53		`•	3.5		¥.		10	-	<u>, </u>
	7	0.7	7.7	17.84	7.	•	9	3	~		60		m
	1 / 0 1	_	9.50	j.	3 .	ů.	2		•		Ö	0	3
	66.9	1001	-71.55	34.43	ζ.	~	ص م	₫.	-			0	~
901 JUB- 1	3	15.23	114.50	-85.53	-4.1	31	٥	_			. 77		_
		•	1	08.1	7.1.	3	•		~~		90	•	20
-	16.2	~	57.29	86,3	7.	7	٠.	-	~		0	0	0
	K to 3	13,21	ſ.	155	.	•	90.0	. 19	020		60	0.0	.017
!		~	20.36		3	05.	٥	-	N		-		~
903 200- 1	6	•	7/ 000		1.5	92.	S	γ.	ç		010	10	•
		Έ.	1.43	Ç	•	~		``			90	9	S
	4.4	7	45,65	-116.10	01.	50.	7.54	57	14.		50.	.03	990
	L		10° 40	5.2	2	-	ŗ	·	٧		.01	.07	.047
:	•	2	-32.71	3.7	7.1.	~	ζ.	·.	٠_		01.	. 10	T.
805 148- 1	0	7	-54./1	06"87	•	. 29	10	-	€.		-	_	700
	5.7	~	-31.01	•	•	3	0	7	. 3			2	0 0
	77.	-2.18	77.	77.11.	01.	23.	89.5	07.	21.		.12	. 15	.014
			55.68	?	•	.57	30 1	∹.				M :	-
		•		•		60	•	•	-			3	r
1 -801 709- 1	0.0	9	15.16	2,12	•	30	7	-	7		90	90.	-
	5.7	0	1.5.	٣.	•	16	₹.	\rightarrow	∹		96	#0 #	9
	7 . 1 .		• •	77.	3 :	70	0.00	00.	•.36		2 0 •	2 0.	• 015
			ů.	? ·	•		3 :	o :	٦.		M .	0	_
		10.	75.7	~	9		7	•	~		50.	50.	8
405 108- 1	0.0	1.57	7.14	12.64	~.	n ≥ • 4	す	-	67.			.07	0.00
;	5.7	1.50	42.60	45.		12	す	-	-			0	3
	11.4	1.50	40.0	-5.10	•	01	67.	-	3			0	2
	17.1	1.55	•		-112	01.		. 1 1	.23		*0	70.	• 015
:	6.77	1.34	4.51	11.00	,	72.	07.	-	3	,			N
805 148- 1	0.0	16.00	97.08	7.2	•	0.4.	20	3	Ň		-	.12	1
!	5.7	. 3	75.13	S	•	•	2	7			-	•	
	11.4	•		5. X.	•		7.89	77.	60.		11		.035
	17.1	.6.51	-30.52	∹	₹.	200-	2	7	7		•	-	9
	45.4	~	3	S	-	2	2		ď.			0	Ð
905 JL8- 1	•	7.4	37.04	3	1.1	15	7	7	6		-	•	7
		^	9.0	20			4.2	5.	3.		• 0	• 0	5
!	έ.	7.4	415.4	=		96.	D7.49	54.	150		.07	. 00	057
	3	07.45	∹	3	-1:1	÷	4.4	3	90		-	-	9
											•	•	

Ġ

(Line)

0 3 8 0 5 9 0 5 9 0 7 1 0.00 00000 012 009 003 003 003 073 050 050 070 926 SHEAK STRESS 0000 20000 P C 0 0 7 22220 90000 4 - 6 0 N BENDING STRESS N-00-0 0 0 0 0 0 00000 20.49 101 3.65 2.64 3.15 3.45 24 24 24 25 25 46 76 76 12,120 24444 0 2 2 2 2 00000 1.000 622.33 699.54 577.05 254.41 28.33 1197.30 1119.90 113.60 46.14 21.75 22.59 18.15 5.46 7.80 19.87 1100 04 1100 00 1100 113 4.40 4.90 11.70 145.61 40.14 1111.13 56.54 EUSENT NA IN-KIPS 11.000 10.57 10.12 31.03 .5x.20 .39.47 .12.40 .23.78 115.02 -165.30 -208.27 -38.41 545,74 360,32 130,69 -92,55 Selven -17.50 RIPS 0 7 0 C C 0.0 1.1 1.7 1.4 1.4 11.e 17.1 62.8 GRUUN AND SECTA 103- 90P AR ARRES



TRAN MEMBER DETAIL MEPUR

25.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0000 0000 0000 0000 06 W 050 055 055 070 0000 0000 0000 0000 0000 20200 25000 V 0 0 1 99200 00000 00000 20000 20000 90000 2000 00000 5 0 0 0 0 2 4 4 2 5 00000 00000 00000 20000 5.00 mg 2000 2000 2000 2 C N N S 3220 3 2 5 7 5 11111 2222 2000 21.16 21.16 21.16 21.16 16.51 55.03 Set Yea WHO WHO WAS 0000 00000 20000 0 N S N L 22.09 22222 -360.91 -554.74 -328.50 -302.39 152.10 162.53 301.72 225.27 38.34 27 20.90 25.14 65.07 153.07 153.36 174.37 54.17 SOL KON 26.50 31.14 2.65 14.63 5.45 5.45 27.11 -5.44 -15.64 37.06 31.02 1.75 31 Y = 2 5 5 5 5 5 5 5 5 5 162.62 162.63 162.64 11111 5 0 5 C C 14.07 14.07 14.01 14.00 2000 2000 2000 2000 2000 A C & V C O 0.0 10.0 61.1 51.7 0.0 10.6 61.1 51.7 6 K 0 C P A 7 D S F C 1 N



LUAD CUNDITION NO.

ACCEPT RESIDENT NUMBER AND PAGE	1 1 1 2 2 2 3 2 3 3 3 3 3 3 3 3 3 3 3 3	FURCE		UMENT MA	. x	i N	DRSIO RR	A P	BENDING		SHEAK	₩ ₩	6014.
2 L J 40	-	90 21 4	8417-41	811412I	841×	8214	201X-41			I S X		/	C * E C
04- 405 104- 1	0.0	1.59	1.74	~	~		4	-	.58			0	~
	7	1.56		1.0	∹	•			90	:		9	•
	15.7	٠,	v.		• ·	9			92.				~
	6. C. A. A. A. A. A. A. A. A. A. A. A. A. A.	1.56	-1.54	17.54		10.	9 7	15	20.0	1	500		100°
900			•	,	;	•	;		•				,
1 -601 506 -60	- 7 - 6	37.37.	20.00	~ .	→ -		3 :	•	<u>٠</u>		9 6		
	15.7			200	15		22.2				70		
	8 c . 8		:	. 5	•	-	. 3	•			0		7 3
	2.12	_	7	-	~	•	3	•	7	1	. 03	C.	0.5
05-1002 180- 1	•	5.0	23.05	\$	20.	23	. 7	3 5	£		٠٠.	C	
!	•	٥.	•	Š	7	7		Ð			70	*0	
	21.1	62.92	•	52,03	5 0.■	00	62.	. O.	. 45		.01	E .	\$ 0.5
	•	T 1	0 3		3 1	٠١ ٠	`.	6 9	N :		M 0 0	0 (
	•	•	60.2			u	•	Co		i		/0• -	
05-1003 319- 1	5	5.62	-407.04	5	~	J	2.5	80.			.14	• 1 •	
	•	7 · · · ·	50,00		٠,	T. f	0 € 0 0 € 0 0 € 0	5 :	3 (1	600	0	٠ د
	• •	7° 0	133.00	• 1	•		יי פינ	> :	v •		0	9	: د
	36,4	5.55	•	~	1.50	2 H 6	, 	500	27	:	77		
	3	44.71	4	⋖	-	4	1	4	4		•	•	-
	01		•		9 9				-			· c	• c
	_ <1.1 <1.1	~	-25.15		3	50	58.5	1.03	22		10	10.	
	_:	24.04	05.0-	5.3	>	2	5.0	•	0		.05	0	.07
	٥.	\$4.00	50.43	~	-10	Ð	2	٥	70		. 10.	C	?
1 -602 506 -10	9	-1.53	-1.57	7	75.	0	7	-	7		\$0.		0
1		•	75.00	2.0	\$1.	3		-	~		.03	C,	0
	15.7	\$	-3.58	٠.	?		3	7	2		_	C	Э
! ! !	, KO. C	25.1-	5.45	15,10	2	0.0	9 9	113	57		03	~ e	20
C4- 400 104- 1	0	15.04	47.0%-	34.96	74.	0	٠,	. 62	٠.		50.	\$0°	3,0
	0	15.03	<0.05-	~	25.	0	2.5	•	~		20	C	>
•	15.7	15.04	ဲ	*15.X4	11.	01.		74.	÷		.03	5 6.	.,
	0	5	•	1.4	Э	\sim	٤.5	.02	٠,		٠٥3	c	\$ 0.5
	77.	15.01	. 27.02	-16.30	2	~	٤.3	٥			70.	700	0
05- 400 164- 1	5	\sim	-10.00	٠.	~	•	1.1	3	·. 2		. 62		0
!	0	-17.69		2.4	91.	900	-1,16	52			- 26 ····	70.	
	15.7	~ '	* D • V *	ε.	~ .	9	-	'n.	- '		20.	o (7
	5				-			,					2

0.55 0.15 0.70 0.53 0.53 10000 2000 4 2 0 0 2 3 $G_{i}^{(j)}$ 746E BENDING Y 22.00 .71 2000 20. 24.23 3 - N THE PLANT THAT TOWN I TAILED ANALYBIA - MET NOW O PER AXIAL BIREUS /***** 1222 33333 -21.15 -21.15 -21.15 -21.16 116.15 N N N N N 121.51 TUKSION MX Bal a-NI 15.77 16.03 1.31 2.64 **PK** 200 7-1-1 4444 22.22.2 469.07 469.07 579.16 567.10 -455.64 841 X+V 216.43 -135.51 -177.14 -172.41 100 E 1640.55 1041.41 537.65 136.00 -1451.00 -1066.51 -594.01 -155.50 -655.01 20.24 2.54 BAIYER .5.55 .5.50 .5.57 .5.57 -11.55 -11.55 -11.55 -11.55 000.00 000.00 000.00 51.14 51.14 51.14 51.14 8414 LUAD CONDITION NO. 20040

DATE . 10/05/	
DATE.	
:	
;	
ı	
٠	1119
	105.0
٠	ī.
	S182
	AVA
	A T T G 11E
	4 0 5
	ATFOR
	E A A A A
	TAKE OFFICE BUSINESS OF PARTICIPA AND AND A SUBSTITUTION OF THE CONTRACT OF TH
	Ž
	5
	-
∞ ,	
.DV V.D	
111000	
O CVC	
-1	

										,	•	
MENALM GROUP NUMBER AND SECTO		7 4 4 7 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	TOTENT TY LATEND	ICSENT AL IN + A I F W	/===OHEAK FI FY *IPU	UXCE/	NOTE TO THE TOTAL	DATA CO	HENDING BIRESS	GTERGO	SHEAR	CC13.
002-1003 200- 1	5 1 4 4 A	00000	200.34 200.34 200.44 37.44	111111111111111111111111111111111111111	2002	22222	**************************************	N N N N N	2.5.0 2.0.0 2.0.0 2.0.0 3.0.0	0000	0000 0000 0000	00000 10000 10000
1902-1004 140- 1	2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2222	55.75 17.70 17.70 17.70 18.81 18.81	2.0 2.0 2.0 2.0 3.0 3.0 4.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5	55555	22222		0 2 2 2 2 2	- m - m - m - m - m - m - m - m - m - m	9 6 7 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	3 D 3 D 1	015
1 -005 140- 1	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	3 3 2 W C C C C C C C C C C C C C C C C C C	2,0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1113007 11137 11170 1200 1200 1200 1200 1200 1200 12	10.01		0 0 0 0 5 3 3 3 3 3 3 3 3 3 3	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	32 32 35 50 50 50	~ N 3 N ~	00.00	0000 0000 0000 0000
235-1005 200- 1	6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	37.54 51.45 15.85 16.07	600.95 100.95 100.67 100.67	33333	N M M M M				W W W W W	N N N N N N O O O O C	00000 00000 00000
04-1605 140- 1	6 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	33332	13.04 13.04 15.07 1.40	10 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	3 0 0 0 0	20000	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	9999	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	00000 0000 0000 0000	0.05 0.05 0.05 0.05	00000 00000 00000000000000000000000000
1 -000 Soot- 1000	P.V.	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2000 B	2000 E C C C C C C C C C C C C C C C C C	9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9		00000	21.22	2.2.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0	C C C C C C C C C C C C C C C C C C C	0000	
35=100e 200- 1	A K & G C C C C C C C C C C C C C C C C C C	30°09 30°09 30°09 30°09	2 C C C C C C C C C C C C C C C C C C C	15.65 2.65 12.85 2.66.70 1.15	11111	3 3 3 3 8 8	8 8 8 8 3 4 4 4 4 4 4 3 5 5 6 6 4 4 4 4 4 4 4	97.00	00-my	##### 00000		00000 00000 00000

PAGE UATE

1	I I I I I I I	1. E. E. E. E. E. E. E. E. E. E. E. E. E.	בי בי	20 M F 10 M	7 × C	7	7 K	Z (E E	n			OF SESSEES	4000 v.
	16 1 H F R	- X W X	ŝ	REMARK	MAX.	0	LENABRE	HAR	, 61	TOTAL	UNITY CR	UNITY CK	UNIIY CA
3	٠. رخ	: CA	2	*().*	U. CK	3	NI).	U. CK	3		61 1,35	GT 1,00	LT .50
£0 → 1		3	~	201- 204	10°	~		£0.	_	12	0	c	15
ابرر. ا		. 07	7	301- 401	70.	^		30.	^	•		•	•
201	502 -202	0.	~	507 - 502		~	102- 105	.01	^	•	0	3	٠
16 0		5 0.	7		. c	^	- 1	50°	7	~	0	0	, p -1
165		30.	~	301 at 103	70.	~		30.	1	3			, m
JL		. 15	~	407-409	71.	~		50.	^	•	0	0	m
ī	511- 711	. 41	7	512- 712	. 1.9	1		. 16	1	•	0	0	٠
105		07.	^	500- 500	67.	~		. 15	^	٠	0	0	£
کار		. 22	_	-	. 42	7		. 05	^	~	0	0	M
(n >		. 45	^	704- 605	. 32	1		. 32	^	12	c	0	12
507		.14	~	204	-12	_ 1			-	- 	•	0	, m
JLA		۲۶.	_	-	٠٤٤	`		. 23	^	•	0		3
15/		. 43	~	702- 103	0 7	7	705- 706	6.1.	^	٠	0	0	٥
716		07.	~		. 56	7		.10	1	•	0	•	: :
1 02		. 1.5	-		. 13	7		.03	7	'n	0	0	1
ž		÷ .	7		5 -	7	712- 312	.18	_	ø	0	0	•
177	401- 604	17.	7	300 - 20E	67.	<u>,</u>		. 15	,	•	6	•	;
ر د ۲	802 408	٠, 46	_	405- 405	77.	~		000	^	m	0	0	m
83	405- BCS	. 13	1	COD	.14	^	AU2- 604	.03	^	r.	0	0	•
701	707 -177	.65	-	904 -706	. 24	_	90% -506	. 21	1	•	0	0	•
710	405-1005	70.	^	9001-906	70.	^	901-1001	₹0.	7	m	0	0	m
(101	905-1005	. 45	~	4001-406	. 35	^	901-100	82.	^	٠	0	c	•
3 2 -	405 - 405	.13	7	504 - 10a	.12	_	704 -206	\$0.	^	~	c	0	m
5		\$7.	~	1014- 414	57.	7	1010- 410	• 12	^	M	0	0	1-1
200	1001-1001	42.	_	1005-1006	446	~	1005-1005	. 23	^	•	0	0	•
) 1	1002-1002	٦١٠	~	1004-1005	01.	_	1002-1004	•	~	~	•	0	-

TUTAL MEMBERS

10 - 45

TOR LECTURE SOURCE STREET RAN

4

(i.)

L. W. NAVY & ACAM PLAIFLRAS & FATIGUE ANALYBIG & MLR 105.0 FEET

/-NEXT IND HIGH CASES-/ CONFINED UNITY OR CCMMINES UNITY OX 3,57 491.35 1555,18 BOTHENT DATEST CONTRUCTING TOPSION UNITY CHECK SIXVek TAKINGS CUMBINED UNITY CA 125-0 2460 1000 25.0 2 130-0 7110 7.01. 1000 3-0% 2-021 7711 U-140 11200

TO A PERSONATE SOUTHER SERVICE SERVICE

2 10/05/76 PAGE UATE

	1	z				ı			١			1			ŀ			1			1			1		,	i					ı			l								,			
164 CASES	COMPINED L	NITY CK		4 2	۰	~	_	. e36 3	_	¥ 500°	\$ 450.	۰	* 7	5 7	D.	30	3.	- ·	- :	# ·	- 1	0 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	7 7	~	023	>	_			7 :	. .	7 5 7	0) (T)	000	~	1.5	20	∽ ,	3 3	. .	,		200	920	
, , , , , , , , , , , , , , , , , , ,	CHAMINED LD	Z C Z	60	53	73	6 0	95	70	27	a) T		. 55	5	~	6	5	 :	# (u (> :	D	0 4		212	5 1	75	31	20	, 5- (. .	9 #	7 9		55	ا د م	20	76	7.0	76		~ 3	D 0		6	0	
21			7	40.0	1.0	10.8	40.0	1.4	775.6	44.7	-	9.76	6.050	241.7	38.7	E E O E	7.4	9 .	3 °	7.707	700	7.7.	165.7	50.7	135.5	531.7	109.5	2.2	-71.52	3.5	7.00	4 1 1 1 1 1	2	•	69.3	370.1	777.0	541.2	90	171	1001	0.4	800	2.5	1 D	
HOEN ACTIONS	7	N-1-4-1	-376,14	 	7.0	65,3	52.5	10.9	78.1	40.0	٧.	25.0	24.0	42.4	9.0	323.0	۵.	1.00	000	C :		•	26.5		23.4	3.0	20.02	9.5	⊃ :	, .	•	,		7.89	71.0	34.0	0,470	5 5	564.5		7.0		31.0			,
TORSION		IN-AIPS	-10.97	ż	26.23	6.7	3.4	Š		A3.4	H 3 . 4	58.1	55.4	4.4	20.0	30.5) : 0 :	Y	0 0 0 7	•	7	• •	•	0.7	3.0	28.4	š	4.6	.) · ·		•	•	1	2.5	76.4	55.6	7 ·	3 :	5.79	n 1	u ^			•	
FINCE		31.1×	-146.57	3.	4.6			5.1	2.5	7.	2	52.5	1.67	٠ د	56.0	, 00	•	 0 :		ונים נים	7 4		4.5	V .		7.	Ð	,	0	17.	•	***	٥	51.0	2	24.2	16.5	16.7	\$ ·	ů,	7 6 7		: :	3	٥	
1810	¥	E20(FT)	o 0	15.4) •	15.4		0.0	25.5	25.5	25.5	1.0	7.0	0.1	7.0	21.6		61.6	ו12	n :	2 2) c	16.6	10.0	14.6	o• o	0.0		10.0))	9 -	0.0	0.01	0.0	3.5	14.6		1	20.4	25.8	0 1			22.0) 5	
1040	3200	J	~	^	1	^	^	1	7	7	7	_	1	1	_	~ 1	~ 1	-	- 1		-		~	1	7	~	_	~		~ P			. æ	^	7	1	^		۱ م				. ~		~	1
ALUES ALUES		S X V - 7	~	. 085	ø	9	5	~	•	•	000.	'n	v	200	Ð,	σ,	750	•	> ∶	,	47.0	10	121	-	Ð	Э	_	9	001	, ,	רח	, ,	• •	.052	-	100	3	~ ~	-	. 10.	• ;	7	, ,	, ,	•	-
. > <		Y-AXIS	•	•	2	3	7	.017	2	3	~	2	-	~	2	3	^ı.	3 :	^	u :	2 2) C		0	-	v	3	~	001	3 :	7 0	, ,	2	. 5	÷	Ş	\Rightarrow	V	∽	> :	9 3	> -	. 5	20	3	
単語のまたのと		4 X I A L	.167	~	V	J	2	101	3	2		~	.174	50 0°	. 017	190	.177	2 :	9	? :	- 1 -	- 6	701	~	5	100	Ξ	\$ 0 C •	25.0) .	_ =	֓֞֝֜֝֓֓֓֓֜֝֝֓֓֓֓֓֜֝֜֝֓֓֓֓֡֝֡֓֓֡֓֡֓֜֝֓֡֓֡֓֡֝֡֓֡֡֡֝	300	=	2	1.7°	≥00°	2	.157	0 2	C + O •	; .	٦	• >		
TOUT X EN	£		_	-	ю	3	\sim	• < > 5	•	-	105	-	-		ø	٠.	.251	۰ د	600	665	1 4 7 7	0.50	, ∿	141	0.0	8 + 2 ·	****	0.030	35 T.	90.	100.	·		1	3,5	. 557	₹0.	Ð	9:		672	7	000	2	13	
	20029	2		~	102	165-	417	400m01	7	<u>.</u>	7	115	160-	112	-010	4c.0	٦٢. د	0.00		ן ה ה	3 -		15/-0	157-	-17	→ 0.0 >	13/-	107	0 / 0 7	101		7 - / - 1	7-/51	13/-1	2 · 0 · 5	71/16	,,	2	,	3 3			1 5 0	000	007	
	*****	•	5- 62	۸ • • •	20.0	5- 50	٠	50 -6	- 71		~ ~	; 0 • 1	24 -5	¥ • ¢	, e		•					2 -	1 - 7	1- 7.	ĭ.	1 33	^ •>	70	70/ -20 71/)				5- 70	9	. I	10 •	- G	•	300 - IC		• •	. 7	 •	; 0 1	

CON LEGISTER SOUTHERS SERVICE SERVICES

	,	- 441744	֓֞֞֝֞֜֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	CALLY CARCA	1			/******/	アレシンロ	ENGER ACTIONS	A	/-NEXT T	i D	IGH CASE	/-87
1 1 1 1	\$00×0	CU-10 1.160	•			200	1 E) X X	<u>.</u>	2 Z	CHBINE	10		_
٠ ا	2	04117 CK	PXIAL	Y-AXIS	67x4-7	200	ENU(FT)	A17.S	12-XIPS	INSKITS	SHINANT	UNITY CK	Š	UNITY	2
3 - 6 /	200-01	55p.	,354	510.	.047	_	2 -	-261.59	7.	5.5	92.6		v	30	4 0
434- 805	100001	.122	020	000		~		7		. 77-	1.64.	3	.	\sim	Ł
9 + 90	10-071	. 141	.112	.001	0	1	,	~	3	11.	29	.042	٠	5.0°	S
402- 404	10-07	451.	> 000	050	.073	^		7.	1.0.	1.00	1.60	1	10	4	ъ
.6.	10-002	.691		3	. 105	^		5.	25.4	£	1.0	-	s	^	£
٠ ١ ٢	113-01	.254	.217	₹ 7 0.	.019	~	10.4	'n	355.8	50.1	13.5		\$		4
11	1011	070	200	000	. 0 SH	_		٠,	75.0	54.1	47.3	.010	~		X.
> =	74-51	. 108	.124	650.	\$00.	7	0	076.45	182.9	70.0	817.2	•	×	~	£
r -21	F 6 - 0 3	.165	.158	.057	010	^	•	50.460-	164.5	364	8.1		'n		Đ
7.50 · 1.50		. 145	\$56.	2 00	490.	~!		-17,40	~ · · ·	30.7	149.3	£	'n		£
- 7	124401	۰.	.170	2	.005	1	:	•	-14.	22.0	11.4	C	ъ	v	£
1001-105	7 - 7 -	V	.001	100	• 040	1	10.4		-211.6		504.6	-	9 0	~	Ś
2.01-175	100-001	٠ دع	4155	510 T	450°	~	٠.	٠.	2.81.		79.6		5	0/0.	Œ.
7	12001	0	. 41	•	450.	7	· •	,	-15.7	3.	47.	_	s	240.	£
₽ ≥ 0	٠	960.	>00.	.003	. 054	7	~	Ø	5.0	26.	19.2	4	S	0 7 0 •	~
• • ·	104-61	.027	. 001	970.	000.	_	27.4	47.	3	å	-	£10°	'n	.012	æ
,	101701		. 0.55	≥ 00.	040.	1		ż	0.5.	•	54.00	Ś	•	. 051	٤.
•	10401	-	.135	-	970.	^	o• o	٠. د	6.5-	-55.37	-		'n	160.	Œ
1-27	10-041	\$42.	102.		\$50.	_		•	3.0		75.A		S.	すいつ・	£
408-1005	114-01	270.	.014		10.	7		-20.56	185.2	,	34.0	.01	'n	. 01.	Ð
. 5-10"	190-01	t t t	. 507	***	900.	_		3.0	21.5	3	17.6	178	'n	101.	τ
t t	104-01	.160	~~·	600	170°	-	- 27,4	٥	7:1.	2,1	69.5	600	'n	.053	£
· • • • • • • • • • • • • • • • • • • •	101161	•	.151	.001	₹00	-	•		12.5	20	3	.102	ī	U 5 13 U	£
·	1つイーに1		. 1 1 3	150.	150.	_	7.72	Ä	1.5.	5.6	5.8	1,00	\$	n	ı
-	120-04	•	176	. 525	050	7	•	`.	2.1.	1.40	6.5	\$60.	\$	2/0.	r
7	100-01	دد.	807°	700°	.001	7	7.77		۲.۲	76.4	20.78	77.	S	-	£
9001-con		3	£10°	800.	.021	7	16.4	07.41	115	٠,	465.53	.017	'n	. 017	£
<i>y</i>	÷	.100	200•		.116	_	3 ° 3	?:	127.4	2000	660.1	~	s	6>0.	æ
- -	ζ,	0	.124	\$ 5°	₹7 □•	~	•	76.	143.5	¥.5	3410.7	•	v	.	æ
	10-57		~	0100	010	7		9.46	144.5	475.8	820°0		s	\ : O •	4
-			455.	750	.014	~	•	-154.14	13.8	67.5	15,0	.114	^	\$41.	Ŧ
J1-100	10-012	· .	3	550.	.010	~	•	17.	707	٠.	17.1	.07	S	.071	4 0
	5	5 0.	900	010	.017	_	24.0	Э	-52.1	67.5	39.5	.014	10	.011	ъ
001->6	10-091	150	000	.091	000.	^	~	010	17.5	٥	55,		'n	3.00	£
7.22-1005	10-01	.118	< 60.	•	6 7 0	1	•	;	\$1.5	4.4	61.0	3	•	340	£
C001-500	400-01 7	• > > •	.153	1000	70°	_		124.15	4.5	2.7	2	0	S		τ
F0 1119	10-01	470.	v	4	470 ·	7	•	ť	7.01.	5.6	55.8	m	10		s
0001-000	40000 P	100.	950.	~	•	7		,	-56.7	3	~	.027	^	.017	Œ
					:	•			٠		•			•	

S ON PROTEST SOUTHER SHEET SATES

PAGE

1	TOTIXEN NOT	4 50 LUAD	UIST OFHUM	12	ATRUCKING AE TOASION AX	MOER ACIIONS MUMENT 17	40:4E~1	Zeris Steris	35	Y-AKIS SHEAK	בר גר מא	: YR .	7+/27×	NERT MIGH CV.CK.	33
-			D END(FT)	217	NATATE	0 1 1 4 e c T	INTIFE	_		1 1 Y					
1- 102 m		, 0	5		30°-	~		0	^	C	7	•	5.	0	'n
1 701 -1	\$ · • 1 · • • • • • • • • • • • • • • • •	.	>	•	°	ï	0	0	1	C	3	•	,	0	^
. 201 0	20.	~ ~	•	0	1	-	~	0	~	0	-	•		0	•
<- 175 -1	10.	,	•		÷.	ے د ح	7	0	<u> </u>	C	3	S.	55.	0	Ŋ
3) () () () () () () () () () (* '	3	•) () () () () () () () () () (<u>ء</u> د		3 6	~ •	000	25.	•	3 6 3 6		s,
	•	· ·	٠	~ :	•	~	•	5 :	~ 1	0 :	Λ:	•	60	•	Λ.
			•		o 1	v -	~ "	3 3	- :	•	3 .	•	٠,	Э:	л.
		· ·	•	-	Ÿ	4. ·	٠, ۱	9 5	٠,	Ö		•	•,	၁ :	∧ u
		n -	n /	•		•	ر ا	3 5		> <	Λ =	•	•)	n 1
	10.	1			2		75.7	000		: 0	7 3	•	•)	n s
	· · · · · · · · · · · · · · · · · · ·	. ~		2				, 0	. ~	: 0	, -	• •	, ,)	٠.
1- 202 -1		. ~		•			7.		. ~	0	. 2		. ,	• •	, v
د	\$0.	1		3	•	٠, ٥٧	7	0	1	C	3		۲.	Э	3
1- 301 0	00. 10-	1 6		~	3	Đ	0	0	_	c	-		, ~	•	v
1 505 -	>c. 10-	~ ~	3.0	11.20	1.3	2.7	÷.	C	~	c,	7		~	3	'n
57	>1.	, ,	•	2°57	۲.	٩	7.	0	1	C	3	•	Š	3	'n
1 204 AU		7	•		C	9	₹.	0	7	3	s	•	1	10:	•
7 V: N = 1	rc	/ - -	•		0	0	¢:	3	_	C	<u>٠</u>	•		3	^
1 4 NOV - 0	? • · · · · · · · · · · · · · · · · · ·	0 1	• •	Š		•	٠, د د) ()	٠.	0 1	.	•	<u>۰</u>	3 .	Λ.
)		,	•	00.0	•	75.53	•) :		o c		•	•,	> :	n ,
	• •	, _ ,	14.5			• •	24.	000	مرأ.	200			n 3	•	ח ר
- C.0 Al		7 52	3	~		S	٠.	000	^	C	77	•	ζ.	. 0	ν.,Λ
. 2 . 6	10-	*		~	0		z,	0	1	c	3		· ,*	ာ	'n.
1 1/5		1 0	•	~	7 . 17	- 5.7	54.0	0	^	C	_		`~`	∍	S
5- 300 UT		x .	v	7.	-22.90	7			7	0	-	•	۲.	3	v
- 505 16	• • • • • • • • • • • • • • • • • • • •	~	•	4.5	Œ	5.7	۲.۶	Ö	_	0	Đ	•	3	_	J r≀
- 500 10		7	·	7	ï	•12°0	, E	C	_	C	Ð	•	;	0	11,
Σία . •	٠. • • • • • • • • • • • • • • • • • • •	~ ·	۲۹۰ ۱	•		φ.	۰,	D .	~ 1	(ر ا		•	073	.
2 0 0			•	v	-;	•	\ \ \ \	۰,	-	9 6	•	•	, .	~	<i>3</i> 1 (
		•	•	•	- 0	7 6	* • • • • • • • • • • • • • • • • • • •	B 0	- r	v •	1	•	•	٠ د د	<i>.</i>
		- 4	•	0 -	. X			u n		5 6	1	•	, .	⊸ ≎	ر ۱۱ <u>ن</u>
1 2 2 1 7 1	10		•		56.	71.4	×	, -	_′	• -	ч			> ::	٠.
- 505 JL	21. 121	20		9	51.	ر. ۳۶	460.9	5	~	5			-	^	. ~
	-01 .10-	0 7	•	6	. 79	~	770.8	3	^	S			_	O	(L)
- 500	10.	2	£.0	5.0	\$	68.7	57.0	_	7	-			_	•	~
- 516 -	101	~ (•	7	103.70	23.1	15.7	010	~	0		•	'n	669	^
1-5:5 10		1	•	, 2	, 0,2	17.3	80°2	•^	~	~	Λ.	Š	_	•	∿
71 112	~• 1o-	· ·		70	•	7.47	19.	÷ 10.	~ 1	(v	'n.	ů.	~ •	
)				14,522	· ·		J ~	~ r	9 :	•	v.	<i>.</i>	~ 1	.
	·		•	•		7 · · ·		7	. ^	٠.	u J		•	0 -	V 1
		. ~	200			• •			. ~	- c	n 3		_	۸ -	n .
01 404 ->		. ~	,		7.7		5.5	• ^•	. ~	. ~	. 4	. 15	•	• •	'
			•		-	٠,	101.59	7	_	, C		u	٠,	•	•
								•	•	>	_	•	6	٩	•

TOR PROBLE SOURCES RESERVE SACTOR

PAGE 2 UATE 10/05/76

U.S. HAVY - ACHR PLATFURIS - FATIGUE ANALYSIS - MLH 105.0 PEET

* * * * * * * * * * * * * * * * * * *	1004	CO441.60	L'OAD C'ini)	DIST FRUT END(FI)	7 T X T X T X T X X X X X X X X X X X X	1010101 11 41 11 00 11 11 11 11 11 11 11 11 11 11 11	2	104E21	2-AXIS SHEAK UNITY CR	ŠC	Y-AXIS SHEAR Unity Ch	2 2 5	ALY/RY	KLZ/#2	1161 2.05 .05	ບ້
- 625	2	.274	~	3	S	6.9	5.1	1.4	50.	-		-	æ.			'n
<u>م</u> و	2 6			15.4 2.4	20 3	-2.51	7	5 7			50°	~ r	20.0	40.5		JN U
· À	10-541	7	٠.	15.4		7.0	5.50			-	-	. ~	, ,	•		,
20	,	~	~			3.6		A .00		-		. ~	;		0	ת. ו
7		^	1		~	5.0	16.6	01.4	3	~	•	~	æ	· •	Э	Λ
:		Л	-	45.5	٠,	54,7	18.1	776.6	00.	7	0	~	•		Z	Λ.
7.	<u>.</u>	-	-	š	76.4	83.4	¥.00	244.7	10.	~	_	_	_:	_•	Ð	S
`	<u>.</u>	9	-	•	ま。 ア		~	97.3	5	~ 1	0	~ 1	-	_	116.	Λ.
ر د ا	•	\$ 10°	٠ .	•	5	5# °	25.6 h	9 766	50	~	~ 1	<u>,</u>	•	•	~	Λ.
520	ָרָט.	٠,		•	1.4.7	0.50	E:	9,050	£0.	~ 1	N (_	•	•	0 1	∿
0 20 10		1			•	٠,	7	7 - 1 - 2	9 5	~ r	c :	~ •	•	•	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	ν,
		c -	. ~	•	7.44	֓֓֜֜֜֜֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֓֓֓֡֓֡֓֡֓֡	מי ניא	- 0 0 1 7			> 2		: .	;	70	n J
		• •	. ~	: .	• •	. 4	7	4 7 6 7		٠,	מ מ		•	•	• :	ני ח
	, ,		. ~	• •	83.	2.5	× × ×				0.0	- ~		•	300	יט ר
136	3	~	~	-	\$. £	V	7.5	20	_		. ~			0	0
450 -07	L 3 •	\$ 4 5 5	_	-	7.5	43.9	3.5	~ ~ ~	00	^	0	7	3	=	•	
`.	116-01	Ð	~	•	3 M . 3		17.5	5.2	60	~	2	7			5 C 5 C	Л
`.		7	`	2.0	¥ . 7 D	1.50	74.3	695,4	\$0.	^	20	~			2	•
2	۲ ا	~	~	•		10.4	V5.3		77.	-	-	^	\$	3	•	S
` .	- 15	. 249	~	D. D.	5.5	6	2 × 5	65.7	50°	~	N	^	~	-	~	٥
_	-/5	7	~	•	~	¥ •	¥.	150.7	€0°	_	ヘ	^	\$		V	10
; D	-	•	~ ·		24.	0	7.6	55.3		•	M 1	~	:	-	J	∿
e :		. 273	٠.	٠	3.	₹ :	53.0	551.7	50	~ .	~ ,	~	٠.	Θ.	34.	Λ.
•		, ·	- •		•	ρ,	e '		2.	10 F	~ (,	•		~ ·	20
•		040.	٠.		, :		;	, .	5 8	٠,	200	0 1	ᡱ.	. .	• •	۰ م
. (3			•		ָיַי	.	^ ·	2	~ 7	Ν.	- :	•	. .	η.	Λ.
• 1				•	- 4	\		ָ ֭֭֓֞֞֞֞֞֞֓֓֞֡֓֞֝֓֡֓֞֝֓֡֓֓֡֓֞֝֓֡֓֡֓֡֓֡֡֡֓֡֓֡֡	2	0 r	5 :	D 1		: .	~ :	ο.
C 1			٠,			•	•		2 3	•	•	٠,	٠.	· .	77.	Λ.
		7 -		•	5 6	•	5 4	7 · CO			2 :		∴.		•	Λ.
` ^	•		- 1		•	•	•	ה ה	•	- 1	9 2	٠,	•.	ᡱ.		'n
` `		27.	۰ م		•			, .		٠ :	V =	٠.		∹.	ר כ	~ :
			_	•			1						•	•	9 3	9
10		157	. ~			3	0 7 7 5	\$76.1		~	0.00		• -	• -		٠ ،
			~	•	΄ ͺ	 	0.4/0	777.5	00		•	. ~			•	٠.
_		10	~		3		344.5	541.2	60			~		,	· ~	. v
•	10-74	٥	~	Ð	30	0.40	7	~	3	~		7	•	24.1	3	·
=			^	•	£	5.7	53.2	171.	~ .	^		^	•		•	£
-		. 213	~	۲,	-	5.5	2.5	104.7	S. D.	_	. 020	~	_	,	•	s
	113-07	~	•		٥	۶.	67.5	0.50	70.	~	020.	~	3	,	~	^
<u>}</u>	【ひしつごろ	~	-	÷	₹.	5.	X.S	247.	3	_	. 025	~	3		-	•
•	ů	Ø	~	•		s.	. 3	X	~ 0 •	~	.019	~	_:	\$	Λ	Ü
d= 694	1001	・・・・	~	55.8	, e5	٠.		٤,5			800.	^	3	•	D 1	£
51.0 -/	1:3-01		^		9.0	-3. \$u		I.	~ 0 •		.021	_	•		3	v
•	10-0-1	2110	_	7 • 2		•	V	۲.	5	Đ	o co.	٠	_:	s.	900	£.
						•	•	•	•	•				٠		•

S TOP THE SOUTH SOUTH SOUTH SOUTH

R

:		1	1													
	;			•	.;	THULLING ME	MBEN ACITUNG	/		1	!		!	} ! 	×	5
1411	7000	FAK THUA FUERTNED	1.045	_ m T ∩	FUNCE		2	MUMENT	81 x 4 - 7	33	Y-AXIS SHEAD	3.5 4	L Y / R Y	XLZ/42	1921	
A4.	2	UNITY CA			RIPS	INSTING	15-41	1 6	111	•	-	' :			•	
803- 908	200-01	557	1	9	-201.39	2.74	5.5	92.4	00	7	C		, <u>, ,</u>	E S	£	'n
÷	10001	.142	~		6.1		3	-69.76	.018	-	810		74.5	74.5	800	S
30 mm	10-07	•	^	•	-35,31	7.0	11.0	29.5	>0.	7	~	7	:	Š	Ð	4 0
(P = 5)	140+01	. 155	~	25.0	٦.	eh.75	4.7	10.0	.0	7	_	^	-	5	~	Ð
?	40.00V	₽2.	~		15.B	25.4	2.80	10.1	£0.	~	•	_	3		$\overline{}$	3
	110-010	ςγ•	^	10.6	٥.	55.H	56.1	513.5	\$0.	~	*	7	3	4	0	\$
7	77,	0#0	~	200	4:5	57.4	34.1	47.5	00	^	0	7	7.		-4	v
7 - 1	2	€.	~	•	7	٠ د د	÷	417.2	3.	~	C	^			196.	v
15- 41	12.27	2	^	.	Ð.	94.5	304.5	20%.1	.01	7	0	_	1.	7.	~	•
5 ·	70.70	.145	~	•	7,9	7.00	50.7	169.3	50.	~	•	_	•		700	v
•	コーナル	°52.	^	•	•	14.7	٥•>	211.0	• 02		v	^	•	₫.	3	v
	一つ・ナノつ	£20.	_	16.4	1.0	1.8	T. 10	4.10	• 0 •	1	N.	_	;	÷	910.	Ð
001-1	10001	. 224	~	ζ,	1.9	14.5	¥>	179.A	• 02	_	-		Š	Š	880.	s
50 1- 70	'n	. 400	~	•	•	13.7	8.8	147.3	₹0.	~	~	~	Š	3	. 114	S
≯ • • • • • • • • • • • • • • • • • • •	104-61	£40.	~)	-15.85	٥.	44.4	119.2	.03	^	-	^	•	ė	570	s
) 	120.	~	27.4	921	÷	8.1	-	10.	~	0	_	•	•	.013	s
₽ 2,	3	•	~	5 • 5	5.3	2.0	2.2	64.A	. 61	^	~	~	÷		050	v
Sub -576) -	2 -	~	5	10.05	۲.	S	12.1	00.	^	0	_	•	•	.077	s
) (: I = 5 r	12-01 2-01	•	-	2.0	Š	J.	0 t. 3	75.A	10.	1	-	_	Ġ	•	.108	s
03-10	7	30.	1	7. 5	۲۰٬۶	5.2	5.4	34.4	₹0.	1	-	^	3	·	910.	∿
01-50	2	オフ・	~)	7	1.5	0.40	117.6	≥0.	1	_	_		•	.178	S
* • • • • • • • • • • • • • • • • • • •	,	71.	~ :	27.4	5.64	1.7	2.1	69.5	.01	^ !	_	_	•	•	5000	'n
*	•	3	~)		٠.	\$0.	٥,	. 0≥	~	•	^	•	æ.	.102	S
5) •	`.	~	27.4	8	5.1	43.4	45.4	2.	^	C	^	•	•	0	S
	10-0-1	.2.	-	∍		1.2	-	64,5	10.	-	_	7	Š	Š	いかさ。	S
301+00	コーつと	45.	~	•	3	>	12.4	20.1		~	-	7		š	3	Λ
))	2	ن •	_ '	16.4	3		82.0	463.3	20.	_	_	~	3	ż	-	S
	•	•	- :	•	16.3	57.4	244.7	660.1		-	~	-	:	_	~	S
•	\$. <50	~ '	.	6.0/	68.5	50.0	10.7	~		~	~			160.	S
5	~	ですべ.	_	•	D	84.5	472°H	1650,0	.0.	~	~	~	٠,	۲.	D	s
01-10	⊃ ∴	112.	-	•	7	٠. س	67.5	15.6	. 61	_	_	ر ا	÷	3	. 114	s
501-17	2	241.	~	•	•	7 ·	70.3	17.7	₹0.	~	~	~	•	;	.078	v
001-20	e E	050	_	24.0	3.01	۲.	67.2	5.	20 •	^	-	7		;	710.	Ð
04-160	J	160.	~	•	~	5.	14.6	Ş	20.		-	_	3	ż	\$80.	s
501100	3		~	•	7.		2.79	01.6		^	-	~	3	ŕ	776	v
3 - 9 >	[\sim	_	•		7	45.7	6.0	Č)	7	C	1	•	7	160.	v
001-00	į	ž	_	.	\$		65	-55.45	.023	_	-	~	•	63.3	950	10
))	100.	~ '	34.0	7.	24.7	*	5.7		~	-	~	•		.047	Ş
0001+500	(つ・つご)	102.	_	~		7	۷. اخ	S X Z	on '	٠	¢	•				1

TO THE TO SELECT SERVICE SERVICES SERVI

(*)

THIRD-HIGHEST UNITY LUAD CHECK CUVD LUAU CUVU M M > N > -- N > -- A N > -- A N N M > -- A N > -- A N N M > -- A N > -- A COAD $\begin{array}{c} \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{$ CHECK 202222 F.2 K.1 P.S Ī K.91 200 AXIAL STRESS RSI CC:01

医 " 口之 下出门出国家 的复数形式 医医电影 医医电影

Zi.

TITLE CANE			1810	AKIAL	DENDING	STKESS	/VIEAK	FINCESSON	1		SECONDAN	_	I	I GHE 31
1001	UNIIT CA		END(FT)	00 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	78 K	76¥	SAIK	SdIX	KLY/RY	KL 2/KZ	CHECK	COND	CHECK	10AU 0.00
V	1	~	0	-5.75	-2.39	00.0	-1.03	3.64	28.5	28.4	001	i	400	•
<u>^</u>	11.	~	15.2		20.02	00.0	1.60	82	3	49.5	053	ا می د :		· - >
5 4 4	£:	~ ~	0 1	~:	• 1 • 45 	0	ჟ.	10.	53	26.7	~	5	.020	~
• 7		- ^	7967	0 5) ,	•	21.15	, 、	55.	œ:	670	ių i	- :	ا (م
))) V	1 .25		0	٠,٠		•	. 6	10.10	*		7 2 2	, ,	200	- T
"	20.	~	3	. =			8.11	3 0	21.	41.4	200	n un	٦ -	٦ ٦
ī :	7.	~		•	1.03	=		~	21.4		940	'n		£
	0.0	~ ^	s 4	∹."	70.	°.	0	3	21.		.077		.034	~
	• •	- ~		\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \		Ç (4.26	29 1	.	•	.035	.	010	~ ,
0 71.0	1 1				55.	• •	76.1	2		•	000	- I		n =
1 160	1 000	~		•	1.00	2	2		3	•	~ ~	n .r	7 6	n •
~	1	~	41.4	7	5.48	•		-	30	30.5	١ ٥	·v	950) ~
-10 ف	1521		•	ŗ.	-1.48	÷	7	54.52	3		101	j	. 3	;
1, 4 00	~ .	~ ,	21.9	د. د .	2.57	•	.6.95	~	~		Œ	ijn	.031	~
	52.		: .	~ 1	-1.29	٠:	٠.	٠.	30	•	102	ا ا	1000	~
		. ~	n c	• 1	60.1	• ·	n .	•	3 .		560	.	3 (3)	a 1
ר ל	· `		•	. =	1.35	•		רם	nu		010	~ u		~ -
310	1	_				•	•			•	000	: - - -	999	1
151 5	1 , 22	^		2.25	2.97	•	•	~	Æ	41.5	133	* #0		
15/-	1	~	ė	₹.	-2.66	0	2,88	.03	E.		.121	c		•
) \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	*·	~ •	14.2	۲.	77.	•	-	٠,	72	•	\$40.	` ^	\sim	r
	•	- ^		`. 1	04.4		6	00.7	0 :	70.3	134	iv :	340	-
10	1	-	• ±	` =	3.4		•	200	0 4	•	1810	•	7.0	^
201		- ~	•	• •		•	* *	7 -	0 4	•	? U	6 14	~ *	e e
5 137	1	. ~		•	-2.21		200	• •	- ×	•	* · · ·	r =	100	C U
Ž	54,	7		``	•			1.52	_	70.3	143	! : ur :	300	'n
د	1 ,40	1	•	3.	-1.60	٠,	Ð	\$	21		17.5	· :/\	•	ec
101	1		÷	74.	4.50			٠	10	61,3	090	, N	460	Œ
0 15/	1.	10 (•	•	2°63	٠	Ξ.	3	83		100	1	.070	•
	•		•	Ç	50.1) ()	3 '	۲,	₹	41.5	125	æ:	Ð	•
) -) -	36		•	•	200	•	• •	? .	2:	•	146	ر ا	ō	ا : م
, V	, ,	. ~		•		•		n	u n	, t	3.50	io i	V .	2 0 3
-74 1		. ~		2.00	0	•		•	7 7		# 10 C	ע ח	013	c «
7	1 . 10		æ	•	-11.11	0	•	1.67	7		. ^	ا سن د	9000	• «
7. 7	1 .11	~	2	_	4.53	•	•	- 42	6		\$50.	• 6 C	. 2	
7 40	15,	_	5	~	-2.74	٩.	-		91.	45.8	0		I	2 0
ا ال ا	. ·	~ (16.2	•	-1.03	•	ŝ		24.			,	\sim	Œ
الا الا الا الا الا الا الا الا الا الا	1 .27		•	T '	5.65	Ç.	•	1.40	.85	\$.109	ī.	340.	•
D	90	- ;		•	1.53	C '	26.1.	90.	0	45.8	S	E I	.035	^
	•		E C		20.7	٥	5	8 C	7 .			6 € (-	. ↑
		. ~	• •	•	6.30	2 6	9 7 1	70.	- 0	V. 27	200	. •	990	20.
			•								į			c

o z 0 I z

3	HAKIMUN	LUAD	1810	AXIAL	BENDING	SUTATE	VSHEAK F	URCE			SECOND-H	_	a	9
7 2 3 3 3 3 4	COTEINED CAITY CA	0 . 2 .		01 x E S S	78 ¥	Z K31	841X	KIPS KIPS	KLY/RY	KLZ/RZ	CHECK	C CAD	CATIV	CUND
2-002 0	757.	~	0.0	45.29	-2.07	0	70.	1.73	-	•	1.86	N.	9.0	æ
902 108-C	1 .12	~	22.H	74	2.54	٠,	1611	0	7			· w	٠.	æ
0.0 140-01	1 . 1 41	~	0 0	-1.57	10.	0.00	Ň	.31	91.6	45.8	560.	æ	5 40°	ĸ
~	•	~	22.H	7 ·	4.07	°.	Ð	Ð	-		.073	•	•	'n
901 C00-01	102.	-	•	\$0.5	5.34	٥.				•	.110	5	.07	5 0
4.0 JE0-01		7	10.2	0/07	÷.	٥.		2.6	4	•	101.	S.	.07	20
*10 rd-01	•	^	•	50.	?	٥.	~	1.1			.010	₹.	.013	æ
7	•	~	0.0	2.48	100	٥.	•	٦.	7	•	140.	S.	0.56	œ
916 74-11	•	~	0.0	-2.10	-1.11		07.	S	۲.		.075	ī.	450°	3 0
10-441 70	•	~	27.4	74	-4.10	0		\sim	•	•		ស	920	•0
10-FUL 305	1 ,254	~		45.5	-21.52	0	2,55		•		107	S	950	3 0
100 1 CA-01	•	~	10.2	10.	•	0	5		24.5		0.016	¢	•	J.
U-14 1-01	•	~	46.5	5,35	~	۲.	4.14	1.05	ż	•	おせつ・	5.	070	æ
Cot 120-01	•	7		46.6	-1.62	٥.	40.5	-1.12	Š		.114	, ,	490.	3 D
~		~	•	14	-1.54	0	-1.82	-	•		7	S	0 ≥ 0	~
-	•	~	•	გი•	.0.	٥.	70.	.21	•		.013	r	.012	= 0
-		~	•	₹.	٦.	٩	-1,12	50.	÷	•	050	S.	150.	*
~	•	~	0.0	₽. v	٦.			03	Ð	•	.077	Ś	.067	a
-	•	~ 1	•	. 5. 54	1.01	•		٠. د	•	•		មា		8 0
7	•	_	•		٥	•	-5.15	45.4	3			s	710.	•
-	•	~ '	•	02.0	•	•	55.		Š	•	.178	'n	101	a C
	•	~ '	•	7	٦,	٠.	1.25		÷	•	500	S	\$60.	1 0
⊸ .	•	~ •	•	70.00		0	50.2	67.	;	•	C	io i	242	₹ :
→ .	•	٠,	7.7	05.7		9	•	76.	.	•		.	.054	ac (
-	•	•	•	2.00	0/•	•	•		,	•	· 045	ın .	V	æ
-	\$	•	∿ .	12.0	1.48	30.0	-	•	65.5	•	770	.		•
, ,	•	. ,	7 6 7	0 2	٠,	3			÷,	•	100	n 1	20.	e i
١.	•	_ 1	0.0	C 0•	•	•	•	÷.		•	• 0 5 6	'n	. 620	3 0
17671 117	062.	· ·	6.0°	~ ∨	>	÷	9.			•	160	in I	580	æ
	•	_	0.0	P/ ">-	٥	•	11.5.	•		•		'n	トマコ・	æ
v		~	0.0	`.	-1.14	•		0.40	•	•	.114	s.	450	æ
V	•	-	9	5.10	1,16	٥.		000	•	•	RL0.	sv.	170	€
×		~	3	2 0.	. o 3	0			•	•	.014	£		r
7	•	~	32.0	10.	4.15	0	10.	95.	•	03,8	.035	'n		40
-	•	~	٥.	94.	1.40	°.	76.		•		***	, IV	•039	•
C.2 <		_	>	5.41	70.1	•	. 62	1.05	•		760.	Ţ	180.	æ
		~	c :	-		0.0	•	• 45	63.0	63.8	.038	•		s
0	1 .007	~	36.0	15.	. 75	ē.	1.35	85.		0, 23		ď	017	*
						,							•	,

:

10/05/76. #UNITED CUMPUTING# 67. APEX/SL H. E.D ACAA PLATFURMS & FAILGUE ANA 184 MENHERS 620738 (25654) 521008 (21568) 2389 LUAD CAMUS \$ \$ 888888 SSSSSSS 8888888 5858588 8888888 2808086 555555 **337711111111111111111111111111** STATES STATES STATES STATES STATES SSUSSES ITTITITITITITITITITITITITI 7 656555 STRENCHE TECHNICIONS INC.).ce.eest 5592 0.001 ..oe.eest.tareeorgfile(Liumany) CHERRITORNAL CHERRICAL CONTRACTORNAL CONTRAC \$55555555555858558 111111 3308088888888 11111 55555555555555555 55555555555555555 L MENUTARO TO EXECUTE 0.573 . 21251 MAY, CM100, TSUU, LS. 155.0 (T) J. ジス・モン・SET. TAYE 580771183。 BULL OF CONTRACT OF STATE ロスペピーの しょうしの コカル・ナン・ベン・ 55050505050505055 01443 PUVUVCU. かんののののの

2014 LD 2 21 LD 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	, trick c		
SUPPRESENTATIONS			;
15.14.UNI	. CYCLE 1	Ĭ.	····
.13.24.8ACA.AAU .13.55. u	.0015		
.13.45.CNIT Y, 18 Jf RLL1, 9 Jf FWD .13.51.38CK**** SUBSTITETION	, CYCLE		ı
~ ~	, ovio		1
7100 * 10 TO	,0225		
1/10/24 1 F F F F F F F F F F F F F F F F F F	100.		
17. ESTATE STATE OF THE STATE O	, CrcLE		!
17.51. U 0 00.01.	, 0235		
	,0002 , CYCLE 1	•	
.14.57.18[Arbac Codestitution .14.53.	3246		
701101110000 0x414141 97.02.	**************************************		
	CYCLE 1		
20.57. U .	, 5316 , CYCLE 2		
.21.54. c c constitution	.0131		
. <1.54.0211 5. 15 Jr Jr Jr	CYCLE		
.21.54. 3 .22.21.U.11 3,	. CYCLE 2		,
- 2469 . 49(A:AAC 0:000111011000000000000000000000000000	127		
.22.55. U U 10.10.	0450.		
	ָרְיַלְּרְרְּבְּּ בְּיִלְרָרְבָּ		
	, GYCLE 2		!
	J.500.		
C. CU. C. PA121176 C. CU. C. CU. PUI 126 C. CU. C. C. PA121176			
7 6 7 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3			
7.70.30.00.00.00.00 7.70.30.00.30.00 9.66.30.81	5455,		1
0.40.34.F			,
	967	1 :	
ZU-SU-UYAPL SUYA BALBAA	A		

ette egpu sec. adisc prusa disc acc. Prusatet acc. alore prusa lape acc 50.00 SERVICE CATURE JUST CUSTES SE

APPENDIX C
WAVE FORCES

ANTERIA ESCRESSIONAL PROPERTIES PROPERTIES PROPERTIES PROPERTIES PROPERTIES

:

BARRES DESCRIPTION

UNITED COMPUTING 67, APEX/SL 8.6.0

11.25.29. 07/20/76.

nndaddadadada	nn_	70	A	A	00000000	000	22		MN	B	00	TANAKANKA
dadddaaaddaa	3	5	**	*	00	0	2	_	Z	3	3	444444444
99	23	3	**	* *	3	00	2 2	z	Z	3	3	4
dd dd		20	AA	A A	00	00	Ż	7.2	2	35	חח	A AA .
30	3:	3	**	*	00	00	Z	z	Z	3	3	4
dd	21	3	**	**	00	0	Z	Z	2	70	3	7 7 7
ddddddddddd	DEL	3		YYY	00	00	2	MA	N.	20	20	T TY-
daadaadaaa	3	3		* * *	00	0	Z	2	Z	20	20	77
3.0	n:	3	* * *	***	00	8	z	7	ZZZ	20	2	444444444
20	200	20	2	<u>,</u>	00	00	Z	; !	2	20	_ 00	- AAAAAAAAA
<u>a</u>	3	3	**		00	0	z		z	2	20	4
2	3	3	**		00	00	2 ?		Z	2	2	7
da	1	nn -	AA		00	00	7		Z	20	00	A AA
2	7 0	3	*		3 0	00	Z		Z	3	30,	44
<u>a</u>	ນນານນານນາ	ນທູດ	*		0	0	2 7		Z	000000	000000	4
	111111111111111111111111111111111111111		^^	!	2000	000	22		NN	1111111111111	. Dimmer	* * * -

2 FT WAVE HEIGHT

5.9 SEC WAVE PERIOD

1.3 FPS SURFACE CURRENT

(0.8 knot)

SEALUAD-2 LIMPED BY SYNEKCHM TECHNOLOGY, INC. HOUNSTIN, TEXAS PELLASE 2 HOD 12 JULY 1976 1.34 1.34 1.34 1.34 1.34 1.34 1.34 1.34 1.34 1.34 1.35 0.0 0.1 0.0 0.0 0.0 0.0 0.0 0.	PAGE	6 6 7 7 8 0000550000055000					
	SEALUADAZ DEVELNPEU BY SYNEKCOM TECHNOLOGY, INC. MOUSTON, TEKAS PELEASE 2 MOD 12 JULY 1976		i	1. W. L. C. C. C. C. C. C. C. C. C. C. C. C. C.	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.7 0.7 0.7 02 FT MAVE MEIGHT	l I

BECOME BECOME BECOME (SOUTH SOUTH) SOUTH BECOME BECOME BECOME BECOMES

133

MASS COEF 1. Me00 1. Me00 1. Me00 1. Me00 TABLE REPURT ... TANG DRAG COEF **** COEFFICIENT NUPHAL DRAG COEF 74600 74600 74600 74600 Olane Tex In

OZ FT WAVE HEIGHT JULY, 1976 27-771-01 C. CHERN COTPUT UVITSENGLISH INPUT UNITS

R F P O R T *** 8 - X V 6 2 0 U

MAVE PERIOU # 5,000 SEC MAVE CELEMITY # 174,256 FT/ D/L # 594545 LATIOA # 63523	## 09525 ## 05524005 10 10 10 10 10 10 10	TO 05 .49517256E=01
9EC 77 77/9EC		.18276903E=06"
		-,43273022E=10
		16170619Ee53
		*,36187653E=17

WAVE PROFILE TABLE

TETAN 0.0 A(FT)N 0.0 DEPTH(FT)N 107.7

P R A H I I O NCILISO

		, , ,		, , , , , , , , , , , , , , , , , , ,		, !		! !	1			
00*09	VERTICAL FORCE KIPS	80	e in	กัง	5,1	8 00	1.1	P- 60	2.5	4	6.0	, 💊
MAVE ANGLE	RSL NT	145.	252.	566. 681.	710.	559.	104.	176.	.007 .004	342.	12u. 62.	280.
	FISH Y X X	-71.	91.	243.	319.	272.	100.	- 84. - 139.	-185.	-161.	12.	109.
	×	126.	•235. •383.	-511.	.634. .585.	-489.	-167. 8	155.	364. 355.	302. 221.	99.	-257,
	Σ	1+	4 4°0	4 +	+ 8.2	+ + 0.4	+ 2.2	12.0	24) 3 2 6	11.3	+ 3.2
	I >	1.4	2.7	5.9	7.3	99.0	3 · · ·	-1.8 -3.3	44	-3.4 -2.5	11.1	3.0
! !		• •	2.1	2.8	M W . 0	N 0 8		0.11	-2.1	9.1.	Ð	1.3
NOITION 1	PHASE ANG. TAVE TOTSTRUC.	201.45	101.50	121.17	30.78 00.58	20.19	-0.00	#5.00-	-50.78	-121.17	•161.55 •141.75	-201.95
LOAD CONDITION	TMIAL DIST. TO TO CHEST	0.00	70.0	00000	0.031	10.0	00.	30.0	0.02	70.0	000000000000000000000000000000000000000	100.0
	* *	-~	~ 7	v o	r 0	0 0	11	13	150	10	200	21

MAVE NUMBER .

N.

WAVE DIRECTION # 60,000

3,6218 KIPS 7,3478 KIPS	8.1920 KIPS	*634.2373 FTekIPS	709.7087 FT-KIPS
X SHEAR FORCE B	RESULTANT SHEAR FORCE B	X MUDLINE MOMENT B	RESULTANT MUDLINE MUMENT &

.. 0661 KIPS

Z VERTICAL FONCE &

UNITED COMPUTING 67, APEX/SL 8,6,0

07/20/76. 11,10,13.

										•					
AAAAAAAA	AAAAAAAAAA	44	VV VV	44 44	44	VV VV	44	*****	AAAAAAAAAAA	44	77 77	VV VV	44	44	
٥	8	ş	5	ĝ	9	; 3	5	2	9	20	20	90	Õ	_	!
0 00000	00000000	O) 	0	၁	þ	_	_					3	COUCE	שטניייטע
Š	2000	3		0	2	10	20	-	7	٥	.	ָ ט מ	S	COOL	Č
z	z	ŏ	Z	5	ō	Ē	_		1		č	Ō	č		=
Ž	Z	ž	Ž	Z	Ž	Ž	22 22	ZZZ	Z Z Z	2	ž	Ž	ž	z	Ē
		2	72	Z	z	Ž			İ						
Z	ZZ	ZZZ	z	Z	z	Z	z	z	Z	ž	z	Z	z	z	2
0	000	00	00	0	00	00	0	00	00	0	0	00	00	00	
00000000	00	3 0	00	00	00	00	20	90	00	90	00	20	00	00	A A A A A A
*	* *	ÀÀ	. **	* *	* *	444	* * *	**	ÀÀ	>	<u>.</u>	*	>	<u>*</u>	A
**	**	*	**	* *	* *	**	* * *	A A A A	>						
3	3	3	3	5	3	3	3	3		3	3	3	5.	ひこうりつ	111111111111111111111111111111111111111
3	20	3	3	3	3	:	33	20	Ofi	5	3	25	3	SUCION	111111111111
deaddddadd	danadadddan	<u>a</u>	3	a a	a	*********	00000000000								1 !

7 FT WAVE HEIGHT

1.3 FPS SURFACE CURRENT

(0.8 Knot)

DEVELOPED BY SYNEY #0.03 TO 0.72 0.72 0.72 0.74 0.74 1.34 0.74 1.34 0.74 1.34 0.74 1.34 0.74 1.34 0.74 1.34 0.74 1.34 0.74 1.34 0.74 1.34 0.74 1.34 0.74 1.34 0.75 0.77 1.05 0.77 0.85 0.77 0.77 0.85 0.77	- 10 m		05,0														
	SEALUAD-2	UPEU BY SYNERCOM TECHNOLOGY, INC. ** HOUSTON, TEXAS RELEASE 2 MIU 12	0	1.3	2 M = 4	P	1,34	0 1			7.0		0.0		D.B.F.	C. CHERN	
	• •	# # # #	5	0.74	0.74	7.0		1.0	21.3	32,0	N 5 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	6.4.0	2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	96.2	_	1	

::\;\;\;

TAUS COET	1.3400 1.3400 1.5400	1.3400 1.3400
TANG URAG COEF	000000000000000000000000000000000000000	0000000
NURMAL DRAG COEF	. 7400 . 7400 . 7400	7400
6144E1E4 18	M W M B B W W M B B W W M B B B W W M B B B B	14,000

POTOTO POSSESSO DE PEROSONA DE POSSESSO DE POSSESSO DE PEROSONA POSSESSO DE PEROSONA DE PEROSONA DE PEROSONA DE

JULY, 1976 OT FT MAVE HEIGHT 27-771-01 C. CHERN ENGLISH UUTPUT UNITS INPUT CHITS

ASSACRATION AND PROPERTY OF THE PROPERTY OF TH

3	•
C	
•	•
œ	
en	
z	
▼	
ø) Z	
0	
U	
w	
> <	
< Z	
9	
T.	
0	
87	,
*	

Û

STREET STREET STREET STREET STREET STREETS STR

MANER ORANGES	11 H 109, 900 UD H 7,600	SEC	
AVE CELEMITY		FT/3EC	
LAMBU.			
(1		
G02 8 3	31.5137.47		
	2014874		
	13/74501		
•	- 1505120a		
A22 8	. 6229632RE-03		
*	.10693252E=01		
•	. 19039055E=04		
N 70	. C74189056+03		
. 4	. 40119559E-06		
	5412/323		
	78545573		
•	42275349		
	.3495169		
	34234182		
	40025562		
	- 02/0//		
() H			
	321527116-02		
	•		
10 05	.58040562	.29730221E-0385691995E-06 .19718087E-08	*08 - 12652A50E-11
10 65	7.49164.7	# C 1 1 1 1 1 1 1 1 1	

THETAR 0. 10. 20. 30. 40. 50. 60. 70. 80. 90. 100. 110. 120. 140. 150. 160. 170. 160. 170. 180. X(FT)R 0.0 9.1 15.2 24.3 32.4 40.5 48.6 56.7 64.8 72.9 81.0 89.1 97.2 105.3 113.4 121.5 129.6 137.7 145.8 0 0 0 9.1 10.5 110.5 110.1 109.6 109.1 108.0 107.4 100.8 105.2 105.6 105.1 104.5 103.9 103.7 103.6 105.5

WAVE PROFILE TARLE

R P O R T POSITION

SCORIE EN SON EN PROPERTIE

 \mathcal{X}

																								:							
VERTICAL	FORCE R I P S	2	9.9	0.0	5.0	5,2	4	•	2.A	•	` .	6.	.1.9	93,1	Ø • •	1.00	9.4	7.00	.8.5	•7.9	. h. 7	.5.6	-3.7	-2.1	1600	7.	1.6	2,8	4,3	5,4	
	/ E	KOLNT	165.	585.	455.	1301.	1005.	1879.	2110.	2297.	2411.	2452.	2369.	2200.		1356	1074	330	32.	474.	643.	1510.	1557.	1707.	1725,	1655.	1493.	1230.	925.	576.	
	ATTENDED A T	>	906	282,	413.	585.	757.	893.	1011.	1041.	1103,	1160	1136.	1068.	20 10 10 10 10 10 10 10 10 10 10 10 10 10		547.	9006	31.	-222.	-441	-606-	-724.	-616.	-840	-617.	-730.	-611.	-453.	-275.	
		*	-162.	-513.	-859.	-1165.	-1416.	-1653.	-1852.	-2027.	-2125.	-2130.	•2078.	-1425.	-1671.		307 I		•	419.	834.	1161.	1378.	1061	1507.	1440	1302.	1068.	4 00	200	,
		PSLNT	+ 2.5	+ 8.2	+13.3	+10.1	+ 22.3	+ 20.0	4.28.9	+31.0	+ 32.1	+ 31.8	+ 30.5	+ 27.8	4 2 4 . 0	0.01+	+12.5	1 1	-1.0	- 7.4	- 13.5	-10.1	-21.7	-63.0	-23.8	-24.6	1.02-	-17.1	-13.0	١٥٠١	
) (,	>	2.2	7.1	12.0	;	19.7	6.55	25,4	27.3	28,3	27.9	20.7	24.3	9.02	7.01	10.0		.1.0	5.0-	111.9	-10.1	.19.3	7.02.	~20°B	9.61-	-18.0	9.41-	-11.5	-7.2	
		*	1.3	4.1	5.0	0.8	10.5	12.5	13.8	14.0	15,2	15.4	14.7	13,5	11.6		7,0		3	-5.7	.6,3	7.8	0.01		-11.7	-11.5		7.9	.6.3	-3.6	
BOANG.		(366)	172,83	160.48	148,14	135,79	125,45	111.10	90.76	30.41	74.07	61.72	96.90	37.03	24.69		00.0		69.45.	-37.03	-40.34	-61.72	74.07	19.00	.4h.7b	1111.10	-123,45	-135.79	-146.14	.150.4H	
THIAL DIST.	NO. CHEST		-140,0		-120.0	-110.0	-100.0		-80.0	-10.0	0.00	0.05-	0.04-	0.08-	0.05		0.0	•	0.02	_	0 • 0 7	0.05	0.0	0.			100.0		0	0	,
-		:		~	~	4	S	•	•	∞	او	□		75	23		5:	2	11	9	10	0	22	7	2	~	25	%	27	12 K	

MAVE DIRECTION # 60,000 15.2564 KIPS 27,9453 KIPS 31.8386 KTPS K SHEAN FONCE M RESULTANT SHEAR FURCE . SHEAK FUNCE HAVE NUMBER B

X MUDLINE MUMENT = 1160,1065 FT-KIPS
PESULTANT MUDLINE MUMENT = 2432,4633 FT-KIPS

Z VERTICAL FORCE # -.6558 KIPS

UNITED COMPUTING 67. APEX/SL 8,6.0

07/20/76. 10,45.31.

DDDDDDDDDD	2	3	*	A A	0000000	000	Z		Z	PEEEEEEEEE	B		E
dadananadasa	25	2	*	* *	00	00	Z		z	EEEEEEEEEE	r		*
a .	nn	2	*	*	00	00	7 2 7	2	z	1	3		3
Q.	מח	3	*	*	20	00	Z	ZZ	Z		3		3
a. a.	3	0 1	*	¥ ¥	00	00	z	z	z		I		I
a a	20	2	*	* *	00	90	Z	z	z	.	R		I
daidaidaidai	3	3	***	YYY	00	00	Z	Z	Z	E .	*	=	-
dadadada	2	3	* * *	* * * *	00	00	Z Z	Z	Z	EEEEEEE	3	E	I
	3	3	*** ***	**	20	00	Z	Z	ZZZ	EEEEEEE	3	X X X	I
	20	3	À A		20	00	Z		zz		*	3	E
	2	3	>	_	00	00	z		Z	F	*	**	3
	20) (>	_	9	00	z		Z	<u> </u>	3	_	3
	3	חוו	>		00	8	2		Z	EE	3		- 5
	3	3	>		00	90	Z		Z	1	A E		1
	nnnnn	שטטניטטו	>	_	00	0	Z		z	FELEEEEEEE	ı		1
1			:		434000				1		ı		

12 FT WAVE HEIGHT

8.3 SEC_WAVE_PERIOD_

(0.8 knot)

DEVELUPED BY STARFOOM TECHNOLOGY, INC. HOUSTIN, TEXAS HOLEASE 2 MUD 12 JULY 1976 JUL
1 CUEF 12. C. 1. S. C. C. 1. S. C. C. C. C. C. C. C. C. C. C. C. C. C.

THE PROPERTY OF THE PROPERTY O

MASS COEF TABLE REPORT *** TANG URAG CUEF **** COEFFICIENT NURMAL DRAG CUEF 7600 7600 7600 7600 7600 DIAMETEN In

JULY, 1976 12 FT MAVE HEIGHT 27-771-01 C. CHERN DUTPUT UNITSENGLISH INPUT UNITS

* 2655/370 * 2655/370 * 2531/3696*02 * 2531/3696*02 * 1145/3146*00 * 1545/3146*00 * 645/30478*07 -.19621416E-01 .70510420E-02 \$1.419449 .4787234 .00542732 .0901464 141549251 1 450000 WAVE PROFILE TABLE

.21902454E-09 .41438650E+03

432195835-07 .35675547E=02

.35122707E-01 -,13837773E-04

.27670122E-02

1.2850779

5

5,9644529

,38706934

THETAR D. 10. 20. 30. 40. 50. 60. 70. 80. 90. 100. 110. 120. 110. 140. 150. 150. 150. 150. 170. XFT)R D.N 9.5 19.1 28.6 38.2 47.7 57.3 66.8 76.3 85.9 95.4 105.0 114.5 124.1 133.6 143.1 152.7 162.2 XFT)R D.N 9.5 113.1 112.6 111.8 110.9 110.0 108.9 107.9 106.8 105.8 104.9 104.1 103.3 102.7 102.2 101.9 101.7

İ

T:

ROBERT STATES OF BOOK ON THE STATES OF BOOK OF THE STATES

;

THE STATE OF THE S

Ų,

*	
•	
*	;
*	
	ì
•	ì
œ	1
C	
•	
•	ì
œ	1 1 1 1 1
	,
>	į
Œ	ì
4	
I	
X	
2	
മ	į
z	
0	١
-	1
-	١
H	
ø,	
0	
ā.	
w	
_ >	
> •	
3	
_	į
	-
•	
	į
	,

											2			. !			
00.00	VEHTICAL FIDGE KIPS Z	9.0	8000	0.0	50	7.0	7°.4	£	*2°,7	*8.4 *11.0	-13.2	-16.7	15.3	12°.4	O & & .	⇒ 8° €	2,2
MAVE ANGLE	TA JSR	671.	286. 814.	1326.	2329.	3519.	3897.	2200 2000 2000	4537.	#030. 3497.	2627.	1106.	721.	.2115. 2554.	2921.	2477.	2481.
	-AUDETVE HOMENT	•362. •142.	110.	57 78 0.	1083.	1527.	1843.	2108.	2186.	1969.	1399.	571.	*305. *6A6.	-980 -1212	-1365. -1419.	-1394. -1321.	-1225,
	×	565. 158.	-265. -724.	=1191. =1038.	-2062.	-2833. -3139.	-3434.	•3872. •3496.	-3476. -3819.	-3516.	-2457	-947.	1338	1674.	2453.	2517 . 2390.	2157.
		9.0	+ 5.1	+ 21.4	+ 35.4	+46.6	+57.4	+ 61.8	+60.9	+51.4	+33.9	+10.7	-13.6	-32.6	1.42.6	1 44.5	136.0
	H H S S S S S S S S S S S S S S S S S S	9.1-	12.0	19.3	31.8	42.7	50.6 52.8	54.3	53.63 89.63	44.5	29.2	9.0	-12.4	-24.0	*\$7.8 *\$4.0	-34.0	• 33.55 • 24.8
i	×	.5.3 -1.9	0.5	9.1	20.02	23.2	27.1	29.7	29.7 28.3	25.7	17.1	5.4	15.6	2.5	-20.7	-21.5	-19.2
LOAD CUNDITION 1	PHASE ANG.AAVE. TU-STAUC. (DEG)	176.63	157.67	146.71	125.75 115.27	104.79	75.35	52.63	41.92	20.95 10.48	-10.00	-31.44	-41.92	.62.88 -73.36	**3.84	-104.79	-125,75 -136.23
1040 CC	RIAL DIST.	•180.0 •170.0	150.0	-140.0	-120.0 -110.0	1000	. 40°0	0.00.0	-40.0	.20.0	10.0	20°0	0.03	70.0	0.00	100.0	120.0
	· · ·	~ ~	~1 ₹	w 0	~ £	0 0	111	13	2 2	17	61	22	24	\$ \$	27	6 0 N	22

	!		!	!	† -	. !
			00*00	VERTICAL FUPCE KIPS	9.0	10.8 1.0.1
1736.			WAVE ANGLE .	70	1305.	372. 113.
-874		5- 20 0. 0.		X X Y ROLLING MOMENTE	-666.	215.
.500	6	× α × π π π π π π π π π π π π π π π π π		×	1122.	303. •110.
- 26.5		2 0	1		- 12.5	1 5.3
*22.5		₩ 50 Q	:	7 × ×	116.7	2.5
-13.6	:	> = = = = = = = = = = = = = = = = = = =		×	-10.3	-3.0
-140.71			LUAD COMDITION 1	TO PRAGE TO WATRUC.	•157.19 •167.67	-176.15
	* *		רמים כ	TRIAL DIST. 10 10	150.0	100.0
33	1				34	36

MAVE DIRECTION # 60.000

Principle School Assesses Investigation

process services seeming

MAVE NUMBER & 1

29.9176 KIPS	54,7110 KIPS	62,3567 KIPS
X SHEAK FOXCE #	Y SHEAR FORCE A	RESULTANT SHEAK FORCE &
		RESULT

=3996,0753 FT-KIP8	2162,3815 FT-KIPS	4543,6232 FT-KIPS
HOMENT &	MOMENT &	MUMENT B
X MUDLINE HOMENT &	A HUDELINE MOMENT &	REBULTANT MUDLINE MUMENT &

Z VERTICAL PORCE .

.. 5979 KIPS

*UNITED COMPUTING 67, APEX/3L 8.6.0

07/20/76. 10,18,46.

deanddadadd	nn nn	20	**	À Å	00000000	000	E		Ξ	nn	33	000000000	
dadadddddddd	22	3	**	*	00	00	II		II		3	00000000000	
d d	0.5	3	*	*	00	00	I	Ī	TIT	20	3	00	
a a	חח	3	**	*	00	00	Į	II	I		3	00	į
	0	3	**	⊁	၁	00	I	II	I		≘	00	
3.3	2	3	* *	* *	00	3 0	I	ĭ	ĭ		3	90	
dadadadadada		3	* * *	* * * *	00	00	I		X		3	00	i
daddddddad	n n	2	**	* * *	00	00	I		I		3	90	
a. a.	3	3	* * *	**	90	00	Ĭ		ŧ		3		
à	20	3	444	<u> </u>	30	00	T T		E		3	00	1
<u>a</u>	מיו	3	*		90	0	I		Ĭ		3	_	
a.	3 00	3	*		00	0	ĭ		I		3	00 00	
a	20	3	**	 	00	3	I		E		3	00	i
<u>a</u>	20	3	*		00	30	ĭ		I		3	00	
3	UUUUUUUU	ימחחמי	*		0	0	ĭ		I	บบบบบบบบบบบบบบบบบบบบบบบบบบบบบบบบบบบบบบบ	3	00000000000	
a.	กกกกกกก	1000	**		00000	000	I		I	_ ขบบบบบบบบบ) D	0000000000	

8.8 SEC WAVE HEIGHT

1.5 FPS SURFACE CURRENT

(0.9 Knot)

20	PAGE 1
2. 0.72 3. 8 5. 6. 6. 72	
5055	
12. 0.74 36. 0.74 44. 0.74 124. 0.74 10.8 1	
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
10.8 144.0 144.0 10.8	
72. 0.72 1.0. 1.0. 1.0. 1.0. 1.0. 1.0. 1.0. 1.0	
144.0 0.74 1.0 1.0 0.10 1.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	
10.8 21.5 32.3 52.3 53.3 55.3 75.3 75.3 77.7	
10 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	
25.00 25.00 20.00	
75.4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
20 44 4	
107.7 0.2	
•	
STRAN 1 60021021010011 27=771=01 0F 1 00 1 170	

MASS CUEF TANG URAG CUEF **** COEPFICIENT MUSHAL DRAG CUEF 74600 74600 74600 74600 DIAMETER 24.000 34.000 34.0000 34.0000

17 FT MAVE HEIGHT JULY 1976 C. CHERN ..., ENGLISH DUTPUT UNITS INPUT UNITS

an especial experience of accession of accession of the expectant of the experience

SAN TANGER ENVER COLUMN TANGE OF SAN TANGE

C

SCHOOL SACRESCALE MATERIAL BASSESSEE SECTION S

107,700 FT 8,500 SEG 382,529 FT	43,458 FT/SEC .2A1547 FT/SEC .13409	30,352427 .45121242	24504594 41120717 -570574475-02 -241294015-11	.25242991E=02 .10414234E=02 .57917402E=06 .02794345	.53167824 1.4375951 53600574 559427852 1.1404677 2.0292163	.13044735E=01	2.0748947 .10609975E=01
							**64366337E*04
							.10376622E=06
							.63213708E=06

WAVE PROFILE TABLE

LACEBA PRAIRIO SOUPHOOL BYEE COC

D.

	,										.:		1	i ; !		
VERTICAL FUNCE RIPS	11.0 12.8	14.4 15.6	100 100 100 100 100 100 100 100 100 100	17.2	17.0	15.1	11.8 10.1	6° 7° 0° 0° 0° 0° 0° 0° 0° 0° 0° 0° 0° 0° 0°	1.5/	•6.7 •11.4	*15.5 *19.5	-22.5 -24.5	*26.5	25.5	11.00	
Teams sees see	1769.	136.	505.	1757.	3064.	4261.	5337. 5402.	6437. 6853.	7151.	7225.	6318. 5441.	4536,	1672.	970. 2041.	2940. 3514.	1871.
-HUDLINE MOMENT FT-KIPS Y	# 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	-379. -106.	197.	804. 1122.	1450.	2021. 2286.	2542.	3043.	3415.	SERJ. MAGE.	3096. 2679.	2160.	190	-417.	-1400. -1707.	
×	1527.	N 80 80 80 NA	1 1 2 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	•1562. •2125.	-2694. -3238.	-3751.	-4693	-5662. -6019.	*6396	-6350. -6038.	-5508. -4730.	-3759. -2630.	-1429.	1847	2585.	1471
8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	1 28.7	10.3	+ 20.0	+ 30.3	+ 50.6	+ 67.8	+ 61.1	+ 42.7	+ 97.5	+ 94.5	+ 79.0	+ 50.8 + 35.4	+ 14.9	- 20.2	1.22	4
A T E Sees	-24.5 -16.5	3	9.2	27.1	2.5.5 5.0.3	59.5	71.1	81.2	85.8	62.6	57.3	4 . 0 . 0 . 0 . 0 . 0 . 0 . 0 . 0 . 0 .	12.3	-16.2	6.69	1.45.
×	114.0	-5.9	3 50	13.6	24.2	32.5	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	7°77	47.0	4.8.6	4.00 4.00 1.00 1.00	26.0	80 9 43 70	-16.1	•22.6 •27.3	6.05-
PIADE TOTALCE	147.03 188.22	178.51	65.051 150.58	141.17	122.34	105.52 94.11	A4.70	65.63	37.64	26.23	100	-9.41	-28.23	-47.06	-65.88 -75.89	-84.70
THIAL DIST.	-210.0 1 -200.0 1	•190.0 •180.0	170.0	150.0	-130.0 -120.0	1100.0	000	170.0	0.03.	-30.0	0.0	20.0	0.04	0.00	0.00	0.00
*	-~	m s	~ •	~ 0	p C1	=3	77	2 4	10	50	22	23	\$	27	ر ک ک	1

WAVE DIRECTION # 60.000 3503,6516 FT-KIPS 7292,7789 FT-KIP8 -6396,0183 FT-KIPS 47.2562 KIPS THE PART OF STATE OF STREET 97,5334 KIPS 85,3207 KIPS -2,6511 KIPS X MUDITAE MOMENT # X SHEAR FORCE # REGULTANT SHEAR FONCE B MUDLINE MUMENT # RESULTANT MUDLINE MUMENT # SHEAR FORCE . Z VERTICAL FORCE . HAVE NUMBER ..

SESSION CONTRACTOR SESSESSES

Ti

ASSESSED TO THE PROPERTY OF TH

(E)

	1				D-0-0 10/41/4 -/0 1911-0-103	•		ָר פּיני פּיני	- -			
				•	09,55,16.		07/20/76.					
anadaddada	00	uū	*			000	2	-	1	1		f
dadadadada	2	22	· >	>			1	4	C 1	£ 1	* ;	
d d	2 0	3	· >	. >	90	3 6			E 1	£ 2	¥ ;	
10	130		*	,				1		¥ 1	X :	200
3	2 3	È	· >	- >	2 5				E :	¥ :	¥	9
a a	Ē	3	- >	- 3	9 6) :	E :	[:	E	* *	×	9
000000000000000000000000000000000000000	!	2 3	- 7		2	3	I.	Ī	I	×	¥	SS
	3	3	* *	>	20	0	Į		£	X	i ! !	
2222002220	?	3	* * *	* * *	20	90	I		1	***		
20	ממ	3	*	*) c	: 1			2 1		のたのののたのののの
3		? :		- ;	> :	2	<u> </u>		E	***		9000000000
. :	3	3	-	***	9	00	I. T		I	XXXXX	:	
2	≘	3		*	20	00	I		1			
a. a.	ם כ	3		*	0	0	3		1			
a	200	30	i	· ·	00		L 3		[1	2 3 2 3	3 3 4 3	
3	Ē	? =	-	. ;) (> 0	E :		E	<u>د</u>	K K	
. t	•	2			2	3	I		I.	×	¥	ø
	000000	00000	-	>	00	0	I		I	X X	×	
3	つつこうこうこうこう	コロニココ		*	00000	000	***		3		3	

22 FT WAVE HEIGHT 9.4 SEC WAVE PERIOD 1.7 FPS SURFACE CURRENT

1.7 FPS (1.0 Knot)

	I			3914
		DEVELUPED	ED BY SYNERCOM TECHNOLOGY, INC. A HOUSTON, TEXAS RELEASE 2 HOU 12	
	• •	,	4251 AJOS	
;	•	********		
15	- 0	1 2	5 3 3 4 4 5 5 6 6 7 7 5 6 6 7 7 5 6 6 7 7 8 6 7 7 8 6 7 7 8 6 7 7 8 6 7 8 6 8 6	7 8 5.11,0
COEF	12.	0,74		
	5 6.	0.74	1,54	
	, d G G	0.74	25 C C C C C C C C C C C C C C C C C C C	
	72.	0.74	1.34	
7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	144.0	-	1. 54.	
		0.01		
		21.6	3.0	
		32,5	•	
		43.3	0.5	
		54.1	9.0	
	1	64.9	7.0	
		75.7	10 ·	
		0 < 0 >	E 0	
			A.0	
2		2001	1.0 22 FT WAVE HEIGHT	
			CHERN	
	I			
	•			•

L 1 2E

**** CUEFFICIENT TARLE HEPORT ****

MASS CUEF	1. W&OO 1. W&OO 1. W&OO 1. W&OO 1. W&OO 1. W&OO
TANG DRAG CUEF	
NURMAL DRAG CUEF	7400 7400 7400 7400 7400
OIA4E1EX IN	16.000 24.000 36.000 44.000 74.000

22 FT MAVE HEIGHT

C. CHERN

JULY, 1976

27-771-01

INPUT UNITS

DOTPUT DVITS

		.52809982E=02
		-,16705619E-05
		-,18742808E-03
SEC SEC FT TVSEC		,32138905E=01 1,2322607
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	- 01404 - 66 570175 - 56 75181 - 16 58 75 1518 - 16 58 75 1518 - 16 58 75 1618 - 16 58 75 1618 - 16 58 75 1618 - 16 58 75 1618 - 16 58 75 1618 - 16 58 75 1618 - 16 58 75 1618 - 16 58 75 1618 - 16 58 75 1618 - 16 58 75 1618 - 16 58 75 1618 - 16 58 75 1618 - 16 58 75 1618 - 17 75 1618 - 17 75 1618 - 17 75 1618 - 17 75 1618 - 17 75 1618 - 18 75 16	3.0234902 10.91132A
######################################		01 TU 05 E1 TO E5

WAVE PROFILE TABLE

TMETAN 0. 10. X(FT)X 0.0 11. 0.0 110. 0EPTH(FT)N 120.5 120.

Prese. Profesol Described Bosses I. Described Described Bosses II. Described Bosses II. In 1955 and A.

NAVE ANGLE # 60.00

Œ
0
œ
_
>
α
•
I
I
_
Ø)
z
0
-
-
H
9)
0
О.
_
W
>
•
Z
-
*
•
#
-

LOAD CONJITION 1

3591. -1699. -28.6 90.10- 53-67.00

•28.9

HAVE ANGLE & 60	
:	
-1	4
LOAD CUNDITION	RIAL DIST. D.
ټ	RIAL

				i :			:	!	
VERTICAL	FURCE KIPS	* 24° 7	16.5	1.0 S	8 2 2 2	N. 4	9.55	15,6	1001
;	SO AND AND AND AND AND AND AND AND AND AND	4282.	4911.	4755.	4185.	3042	2566.	1600,	482
	-MUDLINE MOMENT FICKIPS	-2081.	•2391 •2381	-2319. -2200.	-2030. -1861.	-1703. -1523.	-1314, -1093,	-650. -592.	•279. 25.
1	* * * * * * * * * * * * * * * * * * *	3742.	4289 4285 4285	4152. 3439.	3060. 3359.	3046.	180%	1.556. 895.	393. •133.
		71.1	1 82.0 1 82.5	180.9	72.0	154.0	137.5	- 27.6	1007
į.	E E E E E E E E E E E E E E E E E E E	2.85. 2.85.	-71.5	-70.4	*63.2 *58.4	•53.2 •46.6	-39.4	-23.3 -14.7	v 4
		*34,5 *36,5	1.04	*39.9	-35,8 -33,0	30.4	-23.6 -19.5	-15.1	10.4
•	ST TU-STAUC.	60 S. 87	-92.25 -100.04	#109.02 #117.41	-125,80 -154,10	-142.57 -150.96	-159,34	-176.12 -184.50	-192,49
TRIAL DIST TU	NO. CHEST	1000	110.0	130.0	150.0	170.0	190.0	210.0 220.0	230.0
-		35	30	8 8	0 H	6.5	N E	67	90

0						† 	
MAVE DIRECTION = 60.000	72.5674 KIPS	129,0833 KIPS	148,0829 KIPS	-10134,8196 FT-KIPS	5613.3446 FTexIPS	11545.5170 FT-KIPS	-5.8546 KIPS
SAVE NUMBER B	X SHEAR FORCE B	Y SHEAR FORCE B	REGULTANT SKEAR FURCE B	X MUDLINE HUMENT &	Y MUDLINE MUMENT B	PESULTANT MUDLINE HOMENT &	Z VEHTICAL FOHCE .

geest besoevel with sign considerations and expenses accesses and the second and the second access the second

Û

	07/20/76.
0000 10 VILL 000 1000 000 000 000 000 000 000 000	09.39.26.

daddadddad	20	3	*	*	00000000	0000	I		I	999999999999	**	**	ţ
dedadddaadd))	3	*	*	00	00	ī	_	X		*	*	
a .	20	3	* *	>	00	00	III	Ť	I	14.	**	*	
0.0	20	3	**	**	00	00	I	I	I		**	44	į.
2 0	50	20	*	* *	200	0	Ī	III	I.	16.6	*	*	
2	3	š	* *	* *	90	0	I	ī	I	9.4	*	*	
a unadananan	5	<u>.</u>	* * *	* * *	00	00	Į	į	Į		***	YYY	
adadadaada	יים	3	* * *	***	000	00	I		J.		* *	***	
1	00	3	> > >	***	90	90	I T		X		* * *	**	
4) 	2	**		00	00	T 7		I		\		
1	3	3	>	>	200	0	ĭ		I	44	*		
a.	20	3	<u>`</u>	>	00	00	2 T		I	14	5		
1	00	3	5		. 00	00	I		I.		X	1	,
3.	E	33	ř	>	90	00	I		Ī	9	2		
a	JUUUULIUUL	00,000	*	>	00	00	ī		I	1	7		
<u>.</u>	טניטניטויט	ויוויי	\	\ \	0000000	0000	X		£	9.5	7	!	

27 FT WAVE HEIGHT

9.8 SEC WAVE PERIOD 2.0 FPS SURFACE CURRENT (1.2 Knot)

	• • •	OEVELOPEU		RCOM TEC			t				247	•		
			RELEAS	ON TEXA	BY SYMERCOM TECHNOLOGY, INC. HOUSTON, TEXAS RELEASE 2 HOU 12 JULY 1974	ן אַנ פּר	• • • •				· · · · · · · · · · · · · · · · · · ·	*	1 1	امر ا معرور ا
150	•	1 2 2 3	50		# 21 (V)	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5		50	7	₩ 0	;		1	i
CUEF	12.	0.74	1.34											
	77	0.74	1.34		i		İ	; ;					· .	i
	36.	0.74	1,34											
	t J	0.74	1,34											
	72.		1.54		:			! ! !						i
END 1	0.77	0.74	1,54											
Ŧ		1.0												
			7.0		!!!	!							1	1
		21,7	5.0											
		32.5												
		43.5		!									1	Ì
		54.4	£.0											
		65.2	τ.											
		75.1	. 0	i		!							-	1
		61.0	1.0											
		4.42	1.1											
END		104.7	2		1 . 1			!				!	1	į
			27 FT WAVE	HEIGHT										
			.:											
			JULY, 1976	1976	1									1
STUBE	1 00	60026026010011		71-01	104	00	270	270 10870	80					

 $(\mathcal{E}_{\mathcal{E}})$

(3)

(2.3

ANNA BERESCHER STONES BEFEREN FOR FOR STONES FOR STONES FOR STONES SEEDS FOR STONES FOR STONES FOR STONES

T

27.000 FT 108.700 FT 9.800 SEC	47.205 F7/9EC .234960 .17870	.0135A	28.477818 .4621344 •.47447554	-,7665023 .20243094E-01 .72716169E-01	**//**********************************	7 4 6 5 5 5 1 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	2.5577443 ./*5005/7 .960#4042 1.2932434	\$.0144765 .\$2347009E=01 .\$5072100E=01	3,9325693 ,68092655E=01 28170155E=03 13,157834 1,8465552
									155E-03 11371740E-04
									.360085825=66

WAVE PROFILE TABLE

ļ										
į ;			> <	F 10 00 00 00 00 00 00 00 00 00 00 00 00	2 0	>- &: -4 -3 -1	2 2 2 5	4		
	1040	LOAD CUMDITIUM 1						MAVE ANGLE H	60.00	
- (RIAL DIST	a. u		10 10 10 10 10 10 10 10 10 10 10 10 10 1			ANOR - ANA - MILNE		VERTICAL	
- !	NO. CLE	T 10-57-49C	×	, i	RSCN	×	F Tex P	PISKIPS PELNI	KIP8	
~ N	-260.0 -250.0	202.32	-31.3	-52.4	- 61.1	2797.	-1660.	3253. 2825.	9.2	
~ 3	-240.0	180.70	•22.9	-37.3	- 43.6 - 33.5	2017.	-1218.	2356.	14.0 16.2	
~ •	-220.0	171.19	-12.6	110.0	- 22.3	1063.	-693.	1269.	N° 6 7	
r 0	-200.0	155.63	00.4	15.0	+ 4.0	* A 60 0	320.	91.	22,5 25,0	
• 0	-160.0	140.07	14.2	20.02	+ 31.0	-1490.	708.	1569.	26.9 24.1	
11	150.0	124.50	28.4 35.5	53.4	+ 74.6	•2694. •3674.	1521. 1955.	3269.	24.0 29.6	
1.5	1140.0	108.94	a1.9 e7.9	77.2	+ 87.9	-2217	2375.	591a.	29.8 29.7	
15	120.0	43.33 #5.00	53.8	8.86 109.8	+112.1	-6007.	3224.	6617. 7531.	28.7 28.3	
17	0.00	77.62	73.0	121.4	+138.3	•7932. •8979.	4232.	8990. 10192.	28.0 26.3	
20	0.00	54,45	79.9	125.7	+ 150.1	-10094.	5441.	11468. 12834.	23,5	
21	0.00	10.00	1001	171.7	+ 195.0	-12697.	6773. 7475.	14390. 15651.	. N 9 8 18 18 18 18 18 18 18 18 18 18 18 18 1	
23	0.040	31.13 23.34	104.0	186.7	+213.7	-12437.	7931. 8137.	16472. 16840.	N. N.	
25 26 26	-20.0	15.56	103.1	183.1 175.5	+210.2	-14038. -14058.	A113.	16736.	-13.9 -23.3	
27	00.0	00.00 7.70	79.4	137.8	+182.2	-13012.	7301.	14920.	-32,1 -39,8	
30	30.0	-15.56	00 to 00 to	113.4 35.8	+131.4	-9681. -7596.	5519.	11143. A760.	-46.7	
31	0 0 0 0	-31.13	35.0	57.1	+ 66.9	-5382.	3140	62314	2.45.7	

rest consum, summer execute 7.4C. •\$6.0 1166. \$5¢1. 1430. 5561. 700. issis system statement to a second of the state of the st T. + 2.1 -1.0 CONTRACT THE PROPERTY OF SECURITY OF SECUR

TAVE POGRADA

VEHTICAL V FORCE KIPS	-46.9	-37.2	-26.4	-10.4	67.7	n 0	5.7	11.2	15.6	19.8 21.0
RECEIPT X Y NOTEMINATE RECEIPT NOTEMINATE NO	1185.	4233. 5057.	5522.	5684.	5191.	4050	3716.	2943.	1978.	796. 155.
HUDLINE NONE FT-KIPS V	-1802.	-2037. -2458.	-2696.	•2752	-2520. -2373.	-2205. -2025.	-1073.	-1505	-1053	-454. -136.
×	1091.	3711.	£619.	428.	4536.	3597.	3212.	2529.	1686.	053.
12162	- 30.1	- 72.7	-93.7	- 97.6	-92.1	-61.9	63.0	- 55.1 - a6.2	- 30.3	- 14.1
A A I P S	-27.3	-74.9	. 81.7 . 84.0		-80.1 -76.3	•71.1 •65.3	5.45-	-47.3 -39.4	30 8 20 9	110.0
8	•12.5 •25.3	-34.6	*45.8 *47.5	-44.0	-45.0	-40.8 -37.9	•35.2	-28,3 -24,1	19.3	17.8
ALG. BAKET 10-874UC.	-54.47 ->2.25	-70.05	-85.80 -73.58	101 101 e	-116,72	-132,29	-147.85	-165.41	-178.98	-194,54
AL 0181. 10 CHEST FT	40.0	100.00	110.0	130.0	150.0	170.0	190.0	220.0	243.0	250.0
TRIAL NO.	35	36	36	2 1 2	0.2 0.3	2 UN CC	6 9	67	50	52 53

Y E P O R Y sees	WAVE DIRECTION # 60.000	104,9350 KIPS	187,3805 KIPB 214,7657 KIPB	-14745,3502 FT-KIPS	8136.9282 FT-KIPS	-4.0207 KIPS	
A W H M D S O W D T ####	MAVE WUMBER & L	X GYER B	Y SHEAR FORCE # REGULTANT GHEAR FORCE #	X MUDLINE FUNENT =	RESULTANT MUDITANT BEST B	Z VERTICAL FORCE .	

Ć.

C

TO THE PROPERTY OF THE PROPERT

-

THE PROPERTY OF THE PROPERTY O

RESOTE BATCE

*UNITED COMPUTING 67. APEX/8L 8.6.0

	99 099 099 099 099 099 099 099 099 099
	11111111111111111111111111111111111111
07/20/76.	יורנונונונונונונונונונונונונונונונונונונ
09,10.02.	00000000 000 000 000 000 000 000 000 0
	nninnnnnnnnnnnnnnnnnnnnnnnnnnnnnnnnnnn

32 FT WAVE HEIGHT

10.4 SEC WAVE PERIOD

2.3 FPS SURFACE CURRENT (1.4 knot)

AD-A165 651 FATIGUE ANALYSIS EAST COAST AIR COMBAT MANEUVERING A/6
RANGE OFFSHORE KITTY H. (U) CREST ENGINEERING INC TULSA OK SEP 76 27-771-100 CHES/NAVFAC-FPO-7616
UNCLASSIFIED N62477-76-C-0179 F/G 13/13 NL



MICROCOPY RESOLUTION TEST CHART

NATIONAL RUPEAU OF STANDARDS 1963 A

TO SECURE OF SECURE OF SECURE SECURES SECURES SECURES SECURES SECURES SECURES SECURES SECURES SECURES SECURES SECURES SECURES SECURES SECURES SECURES SECURES SECURES SECURIOR

	; ; ;															
	PAGE 1														. .	
	•															
				7 6								}	11 6 901			
			• •	6 6 7								1	#01 06001 025			
		V, INC.		5 5 6								.				
	2	TECHNOLOGY, INC. TEXAS HID 12	976	9 0							.	9	5			
;	SEALUAU	5 . N	305.4	3 3	3 3						EAVE HEIGHT	JULY: 1976 27-771-01				
	4	EVELOPEO B		2	10.00			2000		į	*	i				
;	**		* * *	0000	0.7	0 7 6 7	•	20.00 0.10 0.10 0.10 0.10	50.00		•		: 			
ক্ষ				15	COEF 12		END 144	!			į	24370	END			;
į				LINE NO.		M = W	10 ~ (~ .		102	200	2 2 3	22	1 1		

5 0.		*** COEFFICIENT	TABLEREPORTSONS		
	DIAMETER	NURMAL DRAG COEF	TANG DRAG CUEF	HASS COEF	1
-	12,000	0027.	0000*0=	1.3400	
	000-42	7400	00000	0040.1	
1 ÷) 3 0 0 0 0 0 0	0017			
	74.000	. 7400	0000-0-	1.3400	
• •	124.000	.7400	0000*0*	1,3400	
. :					
	t				· · · · · · · · · · · · · · · · · · ·

6:

CESTERS PROPERTY PROPERTY FOR THE PROPERTY OF

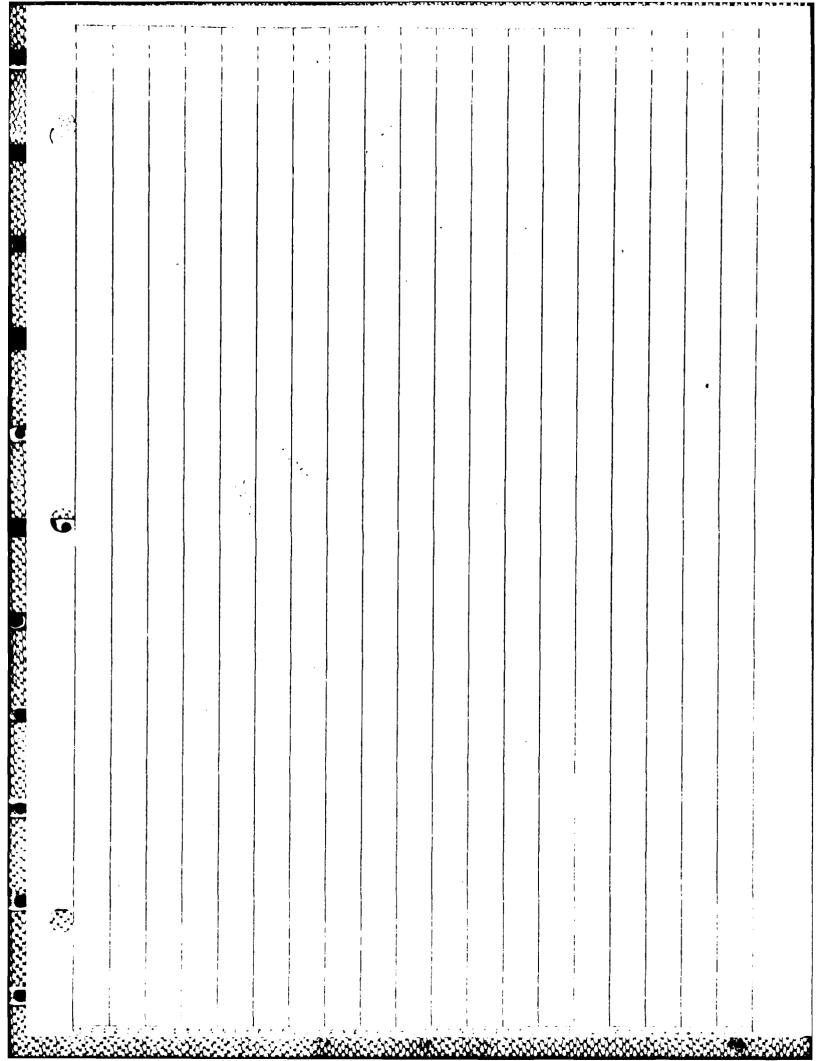
*

din di di di di di di di di di di di di di			
e de la companya de l	14 9¢	CHERN	
ا المراجع والمراجع		JULY, 1976	
 		27-771-01	
•	INPUT UNITS		
	UUTPUT UNITS		
•			
9% - 4			

•	
- 3	
- 3	
•	
٠	
C	
_	
•	
8	
€.	
_	
-	
2	
2	
4	
_	
-	
•	
Z	
2	
U	
_	
>	
4	
4	
3	
-	
•	
ы	
_	
¥	
0	
-	
•	

7	
-	

								62574430E-04 .12064390E-05	10725811
								. 40273109E-02	53589327
								.14222494	2,6037747
32,000 109,300 10,400 510,704	. 18993	. 5592USO . 5592USO . 53096768	-1.0625884 -55671185E-01 -46394685E-01	20130173500 201309145-01	. 6 4 1 5 5 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	. 1224657 . 1141899 . 1354869 . 422/272	.55720116E=01	4.0897247	15,437322



E.A																		
							·											
		00.04	VERTICAL VORCE KIPS	12.51	14.5	19.2	23,1	20.4 31,1	33.6	35.4	W	37.2	37.0 35.0	35.54 2.05.00	2A,6 19.2	6 A	114.0 8.85.0	136.6 146.5
	**	HAVE ANGLE	TITES/SECTIONS NOW NOT NOT NOT NOT NOT NOT NOT NOT NOT NOT	3629.	2799.	1755,	2 to 0 •	1017.	2764. 3705.	2675. 3646.	6637. 7688.	8928. 10355.	11892.	15653.	19690.	22341.	23084,	21295. 19382.
	0 a		FINE HOME FIRST	*1839. *1053.	-1435	*931	-305. 48.	427. 850.	1297.	2654.	3120.	4214.	5009.	7511.	10130.	10710.	11149	10387. 9506.
وندا	> & I		×	3129.	2403.	1488.	384.	-923. -1653.	=2440. =3278.	-4953.	-5857.	-7871. -9130.	-10486.	-13640.	-17299.	-19606.	-20213. -19701.	-16590. -16691.
	2 0		RSCRT	-72.1	188.4	-33.9	17.6	+22.5	+ 54.4	+ 85.8	+114.7	+ 104.4	+179.9	+222.0	+264.1	+289.3 +293.5	+290.7	+ 262.2 + 230.1
	F M 60 C &		I X >	•62.1	-47.4	-28.4	7.2	30.0	48.1	75.4	100.8	126.7	158.0 175.7	195.3	231.3	255.0	253.0	227.9
	> 4		×	.36.6	-24.0	-18.0		17.4	25.4 35.0	60.0	9.4.6	77.4	98.0	105.6	127.4	142.0	142.1	129.5
	•	LOAD CUNDITIUN 1	PYSON TO COLOR	197.37	183,28	164.18	155.08	140,98	120.88	112.79	96.69	77.54	70.49	56.39	35.29	28.20	14.10	-0.00
		L040 C	AL DIST	-280.0 -270.0	250,0	-240.0	-220.0 -210.0	-200.0	-180.0	150.0	-140.0	-120.0 -110.0	10.00	10.0	-50.0	10.0	10.0	10.0
	3 2 8 8 8 9			~ ~ ~	Ma	v	~ 0	• 01	121	11.	201	137	20	22	23	28	28	200

		, =28.20	* ***	107.5	+124.9		5391.	10014	67.0	©
			u) > < I	- H 69) 90 20 11	>- 0: -4 I	C & &	•		
	LOAD	CONDITION						MAVE ANGLE	00.00	
	HIAL DIS	-	//	• • • • • • • •			HUDE THE	N	VERTICAL FORCE	
Ž i	35	-	×	X IPS	PSLNT	×	FT-KIPS K RSENT	RSLNT		
	000	•35.25 •42.29	43.5	71.0 55.2	+83.2	-6591.	3833.	7625. 4520.	=72.0 =74.1	
,	70.0	44.93.	4.5	1.7	1 31.6	-1301. 986.	943.	1607.	-71.1 -63.1	
	90.00	-65.84 -70.89	-28.U -39.3	-53.4 -72.0	160.3	2790.	-1486. -2251.	3161.	*53*3 *55.1	
	110.0	-77.54 -84.59	-47.0	44.5	- 96.7 - 100.0	4876. 5338.	-2724.	5585.	-39.0 -33.1	
	130.0	-91.04	. 55 £ . 1	. 99. . 99. . 99.	-110.3	5502. 5478.	-3076. -3068.	6304. 6279.	-27.3 -21.8	
	150.0	-105.74 -112.79	*53.9	-95,3 -92,8	- 109.5	5324.	-2968.	5846. 5846.	-16.6 -12.1	
	170.0	-114.63 -126.88	4.50.4 4.69.4	-89.6 -85.2	-102.9	+ 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	-2691.	5555. 5183.	1 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
l	0.000	-153.93 -140.98	0.44	-81.0	193.6	4186. 3959.	-2422. -2299.	45.48	2) in	
	210.0	-148.03	.42.3	•73.1 •68.3	1.74.1	3440	-2142. -2005.	3489	4 0 N E	
	230.0	-162.13 -164.18	*36.8 *33.3	.62.5 .55.8	172.5	3152.	-1844.	3654.	9.5	
	0.09%	-176.23	29.0	. 44.0 . 34.2	1.02.1	2430. 2012.	-1454. -1221.	2832. 2553.	18.00 16.00	
	240.0	-190.33	-18.9	29.5	1 34.6	1525.	* 952*	1798.		

							•
MAVE DIRECTION # 60.000	142,0683 KIPS	253,6307 KIPB	290,7094 KIPB	-20212.9884 FT-KIPS	BUIXET POING BILL	23083.6385 FT-KIPS	SOLD SOLD
MAVE NUMBER # 1	X GHEAR TORCE B	W STRAN TOXON	REGULTANT SHEAK FORCE &	X MUDLINE MUMENI B	Y MUOLINE MUMENT &	RESULTANT MUDLINE MUMENT .	2 VERTICAL FONCE &

C34

UNITED COMPUTING 67. APEX/SL B.6.0

	R Z Z	L L L L L L L L L L L L L L L L L L L	LL LL LL LL LL LL LL LL LL LL LL LL LL	7	איי ווווווווווו איי ווווווווווווווווווו
	27 27 22 22 22 22 22	Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z	2	E 2 2	2 2 2 2 2 2 2 2
07/20/76.	999999999999999999999999999999999999999	999		999999999999999999999999999999999999999	5555555555 55555555555 55 55 55
08.07.04. 07.	7272777777777	77	2777777	77	727777777777777777777777777777777777777
80	***		* * * * *		
	***	*	* * * * * * * * * * * * * * * * * * *	* * * :	
	333	333	333	333	2000000
			İ	35.2	-
		4 a a a	4414414144 441444444444444444444444444	1 2 2	2 2 2 2

37 FT WAVE HEIGHT 10.9 SEC WAVE PERIOD

2.7 FPS SURFACE CURRENT (1.6 knot)

PAGE 1				0 6 7 7 8												10990 109 3 11
TO SEAL CAULT	TEXAS	RELEASE 2 MID 12 *		N N N N N N N N N N N N N N N N N N N									:	TOTAL SAYS	このは、アエルコン	27-771-01 DF 1 00 1 370
	* DEVELUPED BY	4 4	****	LINE NU. 15050	0.74	24. 0.74	10000	72. 0.74	END 144.0 6.74 1.54 VOUX 1.0 0.2	\$2.0 0.5 \$3.0 0.8	0.1 0.20	7.1 7.00	 0.23	109.9 T. 1.6		81*A* 1 60030030010011

١.

?

									20507421E-03 .1640 9 562E-05	.18212654 .S1109639E-01		120. 130. 140. 150. 160. 170. 160. 4
			•						. 170590685-02	, 62138653	4 67 4 4 600	707 125 6 136 7 106 116 17.5 125 6 136 7 166 6 104 1 101 9
1- M	9EC F1/8EC								. 25076760	3,5011192	h 45 ()	
HEIGHT B		D/L = .194463 LAMMUA = .20041	6ETA 8 .01137	27.	 * * *	! .	 USS # 1,972251 C1 # 1,5614029 C2 # 5,1523647	C4 8 .79125594E=01	01 70 05 5.9978448	E1 10 E5 17.627504		THETAE 0, 10, 20, 30, XFFTJE 0,0 15,4 - 30,7 - 46,1

Co.

8 L 2 V L 8 Z G D

* × ×

BEAUTOR EG

ST.

T





电子 计自己的复数 医多种性坏疽 医多种的 医多种的

VERTICAL FORCE RIPS RSLNT Z	3946. 3598. 12.0	3149. 2749. 16.4	2244. 1669. 21.1	1043. 23.1 557. 25.2	409. 26.9 1203. 30.5	2064. 34.1 3012. 35.9	8007. 37.8 5034. 39.4	6094. 41.2 7190. 42.4	8/890. 4653. 2653.	11562. 40.1 13474. 46.7	15698. 49.6 16325. 51.6	21148. 52.6 23789. 47.4	m 20	29457. 13.7 31096. ••0	
TOTAL MUDITIVE MUMENTALITY OF THE FIRM TO A MOUNT OF THE PROPERTY OF THE PROPE	-1994. -1827.	*1634. *1415.	-1172.	-580.	122	945.	1869. 2368.	2859. 3370.	3953.	5410.	7333.	11297	12429	14501.	
**************************************	3405.	2354.	1914.		.590.	+1835. -2660.	- 35cc - 45cc	.5382. .6548.	-7399. -8094.	-10215.	-13680. -16217.	-18065.	-23011.	-26323. -27295s	2446
RULNT	183.4	1.58.3	187.4	-21.5	+ 4.8 + 25.8	+ 54.9	+ 77.3	+110.2 + 126.3	+102.0	+ 185.0 + 206.3	+232.7	+294.1 +323.2	+348.7 +370.5	+ 346.7 + 595.0	. 104 C
A A A A A A A A A A A A A A A A A A A	-71.0	N 20	1.00.1	-17.3	23.5	53.0	8.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	97.0	125.4	161.0	202.d	254.5 254.5	305.8 524.7	334.6	7 488
×	5.27	=35°0	-25.2 -19.0	-12.4 -5.0	2.01	19.1	30.3	52.4	77.3	98.5	124.5	140.2	167.5	19000	194 1
ANG. TAVE TU-WITHUR.	195.43 188.91	175.68	164.37	150.34	143.51	150.28	117.26	104.23	91,20	78.17	50.03	56.11	34.09 32.57	19.54	10 91
THIAL DISH.	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	-240.0	-250.0	0.082-	-220.0	-200.0	-160.0	-160.0	-140.0 -130.0	-120.0	1000	.70.0	0.00	0.04.	0.04
F ,	→ ~	~) 3	v o	~ •	۰ ۵	12	21.	2 5 J	~ =	22	22	25	25 .	200	0

			1			•			
	20.5	2374.	-1235.	2033. 5944.	1 I	• 32,1	30°0	-145.41	300°0
	15.9	3313.	.1691.	2000	1 200	. 50°. 6	-30.2	-175.68	270.0
	0.0 11.0	3693.	-2029. -1572.	3476.	-76.5	-73.4 -67.4	-42.9	-162.05	250.0
	8 N . 9	4593.	-2308.	3971.	1.90.0	1.82.	0.82.	-144.83	240.0
		5045. 4889.	-2526. -2423.	4178.	- 104.6	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	51.4	-150.80	210.0
	.6.6 .3.5	5541. 5258.	.2751.	4410.	109.2	-04.7	.54.3 .52.8	-125.77 -150.28	190.0
	*14.7 *10.6	6234. 5908.	# WO WE.	5445.	1117.0	-101.9	-57.6 -55.7	-110.7u	170.0
	-25.3	6703.	•3273. •3169.	5649.	-121.0	-105.9	9.65.	-104.23	150.0
	*37,9 *31.3	6569.	•3214. •3292.	5724.	1110.4	-101.5	57.0	-84.65	140.0
	152.3	5037. 6029.	-2445.	8409° 5260°	1 90.5	-19.8	-43.3	-71.06 -78.17	110.0
	•76.3 •63.0	1059. 3399.	-359.	446. 3000	1 34.0	-51.1	-15.7	-54.65	100.0
	-90.3 -85.5	5513.	2721.	-1564.	+ 51.5	2 % C	26.4	-56.11	70.0
	-86.6 -89.6	13006.	6498. 4534.	-11266.	+ 151.8	130.4	77.8	-34.57	0.04
-	•74.7 •61.6	21076.	10435. 8506.	-18311.	+ 254.5	219.9	103.0	-14.54	30°C
	VENTICAL FORCE KIPS	- Z 102	FISHENCES CONTRACTOR NOTENT CONTRACTOR OF THE MOMENT CONTRACTOR OF THE	× ×	ROLL	KIPS X	*	T. PHASE ANG.HAVE- ST TU-STRUC. (UEG)	MIAL DIST. TO CHEST FT
	00.00	MAVE ANGLE						LUAU CUNUITIUN 1	י מעמי
		*	2	1 1 × ×	2 2 3	F W 00	2 4	•	:
	2.59=								

ASSELUAD SUNNARY REPURT ONS

(3)

para III in ance addition received because because affects and the second and the

(

C							
MAVE DIMECTION 8 60.000	SON POSOL	Sels Site	396.5225 KIPS	-27655.0575 FT-KIP8	15172.1334 FT-KIPB	31543.5547 FT-KIP8	=14,2643 KIPS
TANK NOTHER B	S STEAN YORGE S	Y OHEAK PUNCE B	MESULTANT SHEAR FUNCE B	X MUDLINE MUMENT B	Y HUDLINE MUMENT &	RESULTANT MUDLING MUMENT B	Z VERTICAL FUNCE &

UNITED COMPUTING+ 67, APEX/3L 8.6.0

•
-
176
Ξ.
•
_
۰
_
•
6
о
•
80
_
0
•
•
-
•
42
-0

01000000000	3	3	A A	*	77777777777			9.9.9.9.9.9.9.9.9.9.9.9.9.9.
34343434	3	20	*	*	222222222			
99	2	20	*	*	7 72			777777
30	3	, Ri	**	>		200		3
99	20	22	*	· >	7.2	• u		7 •
99	2	3	*	>	7.7	9 (?:
danadadadada		3	***	***				2
dddddddddd		3	**	*	7777777	9 4		7.
9 .	2	2	*** ***	**	27	9999		3 =
3	23	3	A A	**		2000	9.0	
a a	3	2	>		77			- -
2	2	0 0	~	· >	77			3 =
2	3	מבי	•	\			44	
99	2	3	>	. >	77 77			7.
<u>a</u>	מטטטט	000000	-	. >-	77777777777	09999999		
	A PROPERTY OF	Tomation .		,				37777

11.4 SEC WAVE PERIOD

3.1 FPS SURFACE CURRENT (1.8 knot)

**************************************	***************************************
ROUSTON, TECHNOLOGY, INC. HOUSTON, TEXAS RELEASE 2 HUO 12	
1 1 2 2 3 3 4 4 5 5 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	6 6 7 7 8
2 CUEF 12. 0.74 1.34 3 54. 0.74 1.34 4 55. 0.74 1.34	
END 144.0 0 VCUR	
112 123 134 135 136 136 136 136 136 136 136 136 136 136	
C. C. CHERN	
23 STRAN 1 60030010011 27-771-01 DF 1 00	420 11040 114 3 11
	•

REPORTAGE U A V E 52,232 185398 1.400 95.477 73835285E-03 438955536-04 ,85544483E-01 . 1 5021424E-02 .98248165E-01 1.5111477 1.2151959 4.4521614 1.0504735 2.4723957 69111965 .0043193 1.8925274 11375627 .7344828 .4157530 LAMBUA LENGIH CELEMITY 624 833 8 3 5 8 2 4 8 5 5

SOCIONAL PRODUCTION

COCCOST INCOMENS A NAVANCE TO COCCOST IN

T

-. 44588183E-05 -. 54006649E-03 65632920E-02 1.1998956 .40887586 4,5442523 6.9974427 19.708967 E1 TO ES 01 10 05

.91137036E-01

29264431

HAVE PROFILE TABLE

होंड़ें													! !				
•	00		13,8 16,0	18.0 20.3	22.4	26.8	32.1	38.9 80.8	43, 3 45,8	87.9 50.1	53.7	59.A 62.6	67.6 71.8	67.3 58.7	47.5 33.0	18,9	18.1
	TAVE ANGLE	PINTERS/-PERFECTION NOMENTAL PROPERTY PROPERTY A ROLMT	3609. 3198.	2734.	1631.	292.	1282.	3127.	5225. 6333.	7522. 8645.	10460. 12587.	14607. 17214.	20347.	27222.	33632.	MAGA1.	#1631s
	2. C.	-MUDLINE HOME! FT-KIPS	-1636, -1635,	=1412. -1164.	-880,	-213.	558.	1976.	2460. 2976.	3525.	5769	6850.	9443.	12875.	15918.	19515.	19957
•	>	×	3106.	2341.	1374.	201.	-1154.	-2756. -3665.	-4610.	-6645	-9236.	-12896. -15234.	-18023. -21043.	-23985. -26862.	•29627. •32133.	-34258. -35794.	-36535a
	2 0	A	- 40.0	161.2	136.0	1 11.0	+ 27.0	+ 63.4	+ 99.5	+ 134.7	4174.9	+ 227.4	+ 296.2	+375.4	+ 470.9	+ 510.9	+523.4
	D 0 0	A T A P	-69.4	-52.1	130.0	10.5	405.1	56.1 72.1	67.0	116.3	153.7	200 200 200 200 200 200 200 200 200 200	261.1	329.8	392.3	439.0	4485.7
	> < z	×	-41.5	-32.0 -26.3	-19.9	1.5.1	11.5	29.5 38.3	47.2 55.7	73.4	80 ° 70 ° 70 ° 70 ° 70 ° 70 ° 70 ° 70 °	106.3	159.9	179.4	214.1	241,3	253.2
:	LUAD CONDITION 1	T. Prase ST TO-STRUC.	191.37	164.28	157,16	145,09	133.00	120.91	100.82	90.78	76.00	72.55	60.46	48.30	36.27	24.19	12.09
₹.	3 0407	TRIAL DIST	300.0	-280.0	250.0	-240.0 -250.0	-220.0 -210.0	-200.0	1160.0	150.0	140.0	-120.0	0.000	0.00.0	0.05-	0.04-	20.0

:			506.5	360,3	+415.3	di.	16711.	34048	. 10.7	
			> <	50	D 80	> X		•		
	רסעם כי	CUNDITION 1	; ; ;					HAVE ANGLE	00.00	
7#1#L	CHEST FT	ANG. FASE TURETRUC.	×	T 000	ROLNI	PT-KIPS KOLMT	HUDLINE HOME: FT-KIPB Y	7. C. C. C. C. C. C. C. C. C. C. C. C. C.	VERTICAL FUNCE KIPB	
	MO.00.00	-18.14	180.9	312.4	+ 361.0	-25778-	14645.	29646.	~ C	
	000	-30.23	120.3	203.0	+ 236.0	-16961.	9778.	14578.	-105.0 -106.3	
ł	70.0	-42.32	56.2	45.2	+ 110.7	-8462.	2051.	9799.	-107.S	
i	100.0	-54.41	5.3	.37.1	1 5.4	1327	1065	1608.	90°.	
,	110.0	-66.50	-35.2	6.00 0.00 0.00	100.6	3432. 4052.	=1840. =2698.	3894. 5552.	-70.0	
,	130.0	•76.59 •84.64	-56.9	-101.7	1110.6	5671.	-3100. -3431.	6506. 7013.	-49.2	
	150.0	90.66	-64.1	-113.5	-130.3	6234. 6155.	-3497.	7198.	-34.1	
1	170.0	-102.77	-65.3	-111.0	- 120.6	5954.	•3325. •3165.	6620.	-21.3	
-	200.0	-114.67	500.2	-105.5	- 121.5	5339.	-3023.	6135. 5784.	12.0	
	220.0	*126.96 *133.00	.57.6	-100.4 -00.4	1115.6	4636. 4665.	*2792. *2708.	5565.	N	
	240.0	-139.05	-55.7 -54.6	4.00.	7 111.6	4532. 4376.	•2625. •2537.	\$238. 5058.	0.1	
	250.0	-151.14	*53.2 *51.5	-91.9	-100.2 -102.0	4211.	•2445. •2337.	4659.	4.0	
	280.0	-165,23	-46.7	-84.6 -79.5	97.6	3813.	-2212. -2080.	4132.	10.7	
	290.0	-175.32	5.5	-73.2	1 65.2	3276.	-1917.	1606.	4.61	

**** T T D S O H H T B D S O T D] ****

STATES OF THE ST

			·	
MAVE DIRECTION # 66.000	253,1981 KIP8	455,6887 KIPS	\$21,3075 KIP8	
	X GEGAR TIRCE &	T SHEAR FORCE &	REGULTANT SHEAK FUNCE B	

-36534,9702 FT-KIP8	Y MUDLINE MUMENT & 19957.3174 FT-KIPS	41630,5004 FTEKING
-	•	
HOMENT	HUMENT	HUMENT
X MUDITINE HOMENT	Y MUDLINE MUMENT &	RESULTANT MUDLINE MUMENT #
	-	Z
		RESULT

Z VERTICAL FURCE .

-14.6606 KIPS

325

UNITED COMPUTING 67. APEX/SL 8,6.0

16,17,56, 07/19/76,

	3	٠, د			5	2	2	0.			2		2	2	Q			
		0.00000	Č	00 00	ם סמ		- [00	20	2 5		- -	ם ספ	0.00	0 00	ממט	00000000	ם מטמסטו
	999999999	777777777777	777777777777	77	77	72	7.7	77	2222222	7.7		77	77	77	77	2 22	7777777777	0 2222222222
•												L 14						9.9
	7177777777	7777777777	777777777777	77	11	77	77	77	2272727	77	"		"	1	***	7	2222222222	222272727222
	*	*	**	*	->	- >	- 33			*** ***	***	>	>	**	. >	- ;	١	>
	7 7 7	7 חח	700	700	>			3	3	2	3	70	3	3	3 2		COCCOCOCO	nnanana
		nn dadadadadadad	On de de	On de de	Off dd dd		TITI dedeadeddddd				nn	nn dd	nn da	OI) da	22			5
					_	-		_	. 4			-	-					==

47 FT WAVE HEIGHT

12.0 SEC WAVE PERIOD

3.5 FPS SURFACE CURRENT (2.1 Knot)

	PAGE 1						
		6 7 7 8					470 11100 120 5 11
4.0	AD-2 TECHNOLOGY, INC. TEXAS P MOD 12	3 10					1 00 1 40
	OPEU BY SYNERCE HOUSE RELEASE ALLE	2 W 3	4 W & W & W & W & W & W & W & W & W & W	7 7 M M M M M M M M M M M M M M M M M M		C. CHERN C.	:
: · · · · ·	DE < F	.050	0 0 0	0	2 N 9 P K O	- ACHR -	
			1 CDEF 12.	7 VCUR 144	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	O S S S S S S S S S S S S S S S S S S S	END

ストスの記録 野のかかか まれんなかる かっち

	35		W			
			TABLE REPORT			
	DIAMETER	NORMAL DRAG CUEF	TANG DRAG CUEF	HASS CORF		1
	24.000	.7400	0000*0*	1.3400		
	76.000 76.000	0077.	0000000	1. We 00		
	184,000	0074	00000	1.5400		i i
						!
•			- **			
			· e .			
						!
(
					•	
						1
					+	
						t
				•		
- , j	:					
						,

Ü

gestal Materioson Westerral (Volumental Contractor) (Secretary Separation (Secretary))

(

																	-02 45900675E-04	15494776
																	-,12473226E-02	.45305799
																	.18945103E-01	1,6882774
F 10	2366																.64333759	5,7459277
MEAN MATER DEPTH # 111,000	 0/1 =17		BETA # .00971	CUZ # 20.495992	 *	.	ATT A SCORYLEGION		A55 # 41339419E-03	-	#24 # 1.562630	 844 B 2.2470940	C1 = 1.9864023	•	C3 # -11730590		DI TO 05 8.0101329	E1 10 ES 21,656775

רטעס כר בייטיי	COMPITION						MAVE ANGLE #	90,00
0191. TO CHEST	PIAGE 10-10-10-10-10-10-10-10-10-10-10-10-10-1	, ×	E STATE OF S	RELNT		FIGHTHS ROMENT COLOREST	RSLNT	VERTICAL FORCE KIPS Z
	176.10	. e S . a	-76.5	0.00	5241.	-1909. -1734.	3761. 3395.	No.
i	166.97	-36.6 -31.1	-60.1	1 59.0	2546.	-1527.	2969.	17.2
	155.84	-24.9 -18.3	-39.2	- 46.4 - 32.5	1672.	-1036. -751.	1967. 1376.	21.7 23.7
	144.70	*10.8 *3.0	-14.0	17.7	591.	-429.	730.	25.8 27.7
	133.57	13.0	14.7 29.6	+ 15.0	-671. -1376.	284. 681.	729. 1536,	29.7 33.5
	122,44	32,2	65.0 61.0	+ 50.4	-21 to 3.	1107.	2412. 3369.	57°54
	111.31	41.00 4.00 4.00	7/.6	+ 87.9	• 3895 • 6859	2064.	5505.	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
	100.18	59.4	109.9	+124.9	=5893. =7006.	31340	6675.	60.00 52.1
l '	89.05	78.5	105.4	+ 164.3	-8264. -9825.	4393. 5216.	4360. 11123.	N
.	77.42	102.7	190.6 219.0	+ 216.5 + 248.5	-11756. -13955.	6196. 7397.	13289.	70.6
	66.79	135.1	252.6	+286.6 +330.7	•16656. •19893.	8730. 10387.	18805. 22441.	75.4 03.2
1	55.00	179.5	333.8	+ 428.1	-23440.	12391.	24514. 30657.	\$° 60 0° 80 0° 80
	84.52 38.96	226.9	#19.2 #61.1	+ 470.7	-30719.	16382.	34814. 39023.	70°7
	33,39	272.2	500.7	+ 569.9	-3FUSO.	20335.	43143.	57.5 41.7
	22.26	309.2 321.5	564°. 564°.	+ 0000+	- 4 2 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	23877.	50418.	0.4
	11.13	327.9	592,	+ 077.5	-47933.	26035.	54547.	715.

		3679B 10.07 3670B	361.4	3	· 676.	.5	2,265.	. 92/15	•35.3	
33		00.00	319,0	568.7	+ 652.1		25764.	53411.	-54,5	(F)
		•	> 4 7	₽ 00 00 00 00 00 00 00 00 00 00 00 00 00	3 s	> a	- C	•		
!	CO GVU	OAD COMOTHEN								
12.2										
0	CA CA CA CA CA CA CA CA CA CA CA CA CA C	AVG. TAVE TO-STRUC.	00000000000000000000000000000000000000	SdIC A Sees	Recessors	×	FISHEN TO BE	RSLNT	FORCE	
3 W	20.0	2:	303.0	535.5	+ 615.3		24594.	50589.	-72.7 -05.8	
9 ~	000	-16.70	249.3	432 369	+ 499.5	-35712.	20212.	41035. 34968.	•102.1 •112.7	
90 6		-27.83 -35.39	177.1	301 3	+ 349.5	=24797. =19277.	14256.	28603. 22265.	-120.3 -124.8	,
0	40.0	-58.96 -64.52	100.9	167 1		-1a07u,	8166.	16266.	-126.1 -126.0	
~ ~	00.00	-50.09 -55.66	34.0	50.6	+ 61.0	-5227.	3126.	6091.	•121.4 •112.1	
4 a a S	110.0	=61.22 =66.79	-17.5	0 .0 L	79.6	1349.	-537. -1912.	1452.	-95.6 -70.7	
•	130.0	•72.35 •77.92	-51.1	-107.4	100.4	50 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	-2613. -3311.	5772.	.62.5	
60 0	150.0	•33.48 •89.05	.65,3	-115.8	- 133.0	6316.	•3557. •3613.	7249.	-63.9	
0 ==	170.0	-04.61 100.18	-67.5	-119.0	130.6 134.4	6330.	•3555. •3412.	7260.	-28.7 -22.6	
~ ~	200.0	-105.75	5,84-	-114.1	13101	5832	•3252 •3092	6678. 6269.	-17.6 -13.1	
55	220.0	-110.66	-61.4	-106.6	-123.2	5126.	-2965. -2864.	5922. 5734.	E . 0 .	
0.	240.0	-128.01 -133.57	59,6 59,4	-104.3	- 120.2	4722	•2787. •2725.	5576. 5452.	•4.9 •2.9	
•	250.0	-139.14	. 59.0 . 58.5	-102.8	-118.5	4509.	-2664.	5330.	0.1.	
0 -	250.0	-150.27 -155.84	-57.8 -56.8	-100.2	-115.7	4356,	-2543. -2470.	5073.	2.2	
N M	300.00	-101.40	.55.3	195.4	1110.5	#104. 1014.	-2377.	4781.	5.6 7.6	
1	110.0	1172.51	9.078	0.48.	7.801.7	7041	70.00			

MEPONTESSE	327,3636 KIPS 567,7713 KIP8	672.7858 KIPS	=48012,9779 FT=KIPB 26202,5507 FT=KIPB	54726.2002 FT-KIPS	-35,3413 KIPS				
MAVE NUMBER .	N GMEAR FORCE &	RESULTANT SHEAR FORCE B	X MUNLINE MUMENT B	REBULTANT MUDLINE MOMENT	Z VERTICAL FORCE .				

SOOO RESCHE SATES

拉拉

UNITED COMPUTING 67. APEX/8L 8.6.0

	٩
-	ı
•	e
;	٠
•	7
•	١
	1
•	
•	۰
-	
•	١
_	ľ
	۰
2	
•	2
4	
- 2	
•	1
	1
	٩
_	
•	۰
¥	ı
Ľ	,
	ı
	١
¥	ı

		nn	DIA	A	*	77777777777		Telegologica de la constanta de la constanta de la constanta de la constanta de la constanta de la constanta de	-	_	1
		3 3	2	>	*	777777777		1111111111	. >	' >	
	0.0	3	3	*	*	7 22	1		(×	(> (>	
	66	20	20	AA	*	22	1		XX	N.X.	1
	30	3	20	*	*	77	. ie.	77	×	XX	
	99	2	2	*	*	77	14.	2	××	××	
	ddddddddddd	חה	200	YYY	AAA	27		15	XXXX	×	
		20	20	* * *	* * *	1211111			XX	•	
	0.	200	2	**	**	77		77	×		
,	a	nn	00	AA		22	in the same of the	- 11	XXX		
	9	חח	2	•		77	. Is.		×	×	
	<u>a</u>	00	2	>	_	77	1	3	×	XX	
!		Dr	חח	A				- CE	XX	XX	}
	9	7	3	*	•	77	14.	33	×	××	
	<u>a</u>	20000	ດກຸດກຸດກຸ	>		22222222222	•	333333	×	×	
i I	44	ากกกก	. กกกกก	À	1	2222222222	9.6	13333	X	X -	1

52 FT WAVE HEIGHT

12.6 SEC WAVE PERIOD

3.9 FPS_ SURFACE CURRENT (2.3 Kno+)

PAGE 1		•					
	DEVELOPED BY SYNERCOM TECHNOLOGY, INC. * HOUSTON, TEXAS RELEASE 2 MOD 12 * JULY 1976	1 2 2 3 3 4 4 5 5 6 6 7 7 7 8 6 6 6 7 7 7 8 6 6 6 7 7 7 8 6 6 6 7 7 7 8 6 6 6 7 7 7 8 6 6 6 7 7 7 8 6 6 6 7 7 7 8 6 6 6 7 7 7 8 6 7 7 8 7 8	28. 28. 20. 20. 20. 20. 20. 20. 20. 20. 20. 20	1. 34 1. 34 0. 3		20 ~ M ►	C, CHEMN JULY, 1976 27-771-01 27-771-01 DF 1 00 1 520 11160 126 3 11
	DEVELOPI	LINE NO. 1 S O S O S	COEP	END 144.0 0,74 VCUR 11.0	W 3 R 4	END 111.6 100.6 100.6 111.6 11	STRAN 1 60034034010011

CONTRACTOR CONTRACTOR

			Ü		
 		ASSEPTION OF NICIENI	TABLEREPORT	****	
ا ا ا ا ا ا ا ا ا ا ا ا ا ا ا ا ا ا ا	DIPETER 12x	NORMAL DRAG CUEF	TANG DRAG COEF	HABS COEF	
e Sele	12.000	. 7400 . 7400	000000000000000000000000000000000000000	1.3400	
	30,000	0027	00000	1.3400	
- - - - - - -	72.000	0037.		00 34 W	
	144,000	9 7 40 0	0000*0*	1.3400	
•					
•					
i v i L <mark>®</mark> js					
•					
ا ادر در در در					
ا ا ا ا ا					
•					
ا ا ا	:				
•					
. (

SALESTEEN STATES SALESTEEN SESSEN SESSEN SESSEN SESSEN SESSEN SESSEN SESSEN SESSEN

لتنا

SEE FEDRIE SEEFFORDU MY AR SOUTOFSEE

8EC 8T 8T					.94958605 .43967494E=01 =.23444274E=02 =.19668291E=03
MATER DEPTH B 111,600 MAVE PERILUD B 12,600 MAVE LENGTH B 700,091 VE CREENITY B 55,500	 24.521927 .84914537 -1.7037025 -3.4677995	.403789916-01 .17172378-01 .25103456	171427626 02 1 3653936 1 5427380 1 9242301 6 3305441 3 1065792	5.5047799 2.3059466 14.082869 13740661	6,9671120

١

WAVE PROFILE TABLE

, ,		S.					Ű.				
			•	3 4 3	POSIT	1 0 N O I	> a 4 I I	R P O R T	* *		
,, , 1,; •••••		LOAD CON	CONDITION 1						MAVE ANGLE .	00*09	
o al mand Paranasi	TRIAL NO.	DIST. TO CREST FT	PHASE ANG. HAVE: TO-STRUC: (DEG)	x	I >-		* * * * * * * * * * * * * * * * * * *	FIRST NOMENTERSONS NOT NOT NOT NOT NOT NOT NOT NOT NOT NOT	NT CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC	VERTICAL FORCE KIPS	
ا نواردون	1 .54	340.0 1	7~ •	-49.1	-82.9 -75.8	46 46 46 46 46	3324,	-1950. -1795.	3884,	12,5	
. 🚗 .	3 -320	00	59.41	-40.7	. 57.2	1 68.6	25685.	*1605. •1397.	3128.	170.0	, ,
•	5 .300.		54.27	-29.7	-47.6 -30.3	1 45.1	1 C C C C C C C C C C C C C C C C C C C	-1156	1704.	22.0	
ا درجی	7 -280.		45.98 38.84	16.5	.23.6 .10.7	1 24.0	9.00 36.00	* 616.	1107.	24,1 26,1	
	10 -25	0.0	33,70	-1.0 7.3	4.2 4.3	+ 10.0	-243-	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	246. 968.	27.0	
ا در د	11 -240	00	23.41	15.9	X3.0 48.7	+ 36.6	•1561.	792. 1219.	1750. 2610.	34.1 38.1	
1 2	13 -220	00	13.13	34.1	64.9 81.8	+ 73.3	•3145. •4053.	1690.	150 50 50 50 50 50 50 50 50 50 50 50 50 5	4 4 • 4 • 6 • 6	
L Tevy	15 -200	000	02.84	52.7	97.8	+1111.1	*5021. *6062.	2681.	5691.	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
. D	17 -180	00	92,56	71.5	152.1	+ 150.3	=7224°	3820.	9175.	55.4	
ا نردائد	19 -16	0.0	77.13	1000	174.3	+ 196.2	-10214.	5416.	11561.	75.3	
ر دیگری ا	22 -140	0.0	71.99	125.5	253.5	+265.0 +307.4	-14664.	7752.	16587.	79.2	
ye 46 4	23 -12	000	61,71 56,56	167.9	315.2	+357.1	-21183.	11033.	23884.	97.0	
ا	25 -10	00	51.42	223,7	414.8	+471.3	-29366. -33739.	15623.	33264.	108.2	4
(->?}₁₁:	27 - 65	00	41.14	261.0	520.4	+591.4	-38311.	20350. 22852.	43380.	94.6	
ن نام کورن	30 -5	00	30.65	358.1	623.4 669.0	+ 709.1	-47663. -52114.	25372.	53496. 59067.		
.	31 -4	-40.0 -10.0	20.57	380.1	706.9	+ 805.S	-56063.	30014.	63592.	20.2	

ent a respectivities of the source "external expects" ship of a horsens are executed a section and the source of t

		Parismusia de la misso			7 1 C 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	1, 1, 1, 1, 1, 1, 2, 2, 2, 2, 2, 2, 2, 2, 2, 2, 2, 2, 2,	1000 September 1000	*Parte ************************************	67119 67109	50000000000000000000000000000000000000		
	35	-50.0	10.26	412.7	746.3	+954.6		33050.	.06480	.16.3	(Carlo	[!
		}										
**************************************			•	3 4 2	1 8 0 a	TION SU	x x x	F 0 F	*			
		LOAD CC	LOAD CUNDITION 1						HAVE ANGLE	00.00		· · · · · · · · · · · · · · · · · · ·
	THIAL											
	N O	CHEST	ANG. FAVE. TO-STRUC. (DEG)	/•••••×	A I P A A I P A A I P A A I P A A I P A I	1 2 3 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	FISHER ACTION OF THE PORTS OF THE PROPERTY OF	-MUDLINE HOME FI-KIPS	ENTERNATIONS SERVICES	FORCE KIPS Z		r ;
	35	0.0	5.1 to .00	#14.2 #06.3	746.1	+853.4	-61570.	33532.	70109.	4.00.19		j
	36	10.0	-5.14	360.0	690.2	+ 792.3	-57495.	31845.	65726. 60759.	-83.0 -102.1		!
	3.0	0 ° 0 %	15.43	327.8	570.9	+ 658.3	-47317. -40820.	26733.	S4347.	#117°B		
	24	50.0	-25.71 -30.65	242.8	332.7	4 480.6	-33439. -27114.	19500.	39143.	-139.0 -144.3	,	₋
	E E W	70.0	-38.00 -41.14	151,3	252.9	+ 294.7	-20049.	11995.	17081.	-146.1 -145.0		
	5 P P	100.00	-46.28	6.8.6 34.0	109.6 50.0	+ 129.6	-9570. -5145.	5620.	11098.	-140.6 -134.5		· - !
	60	110.0	-56.56 -61.71	4.9	-1.7	4 5.2	1383.	1040.	1731.	-122.3 -102.4		
333	000	130.0	-50.85	* 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	-77.1	1 4 113.5	3902	-2110. -2985.	6117	-80°-0		
	50	150.0	-77.13	4. 4. 4. 4. 4.	-113.4	14130.0	6533	*3678	7069.	- 54 . V		i
	52 53	170.0	•67.42 •92.56	-70.3	-123.8 -123.4	1142.0	6549. 6462.	•3714° •3636°	7563.	=36.2 =28.7		
3333	55. 55.	200.0	-97.70 -102.84	•66.5	-120.7	00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	6192. 5690.	•3476. •3298.	7101.	-22.5		
	5.00	220.0	-107.99 -113.13	**************************************	-113.5	- 130,5	5540.	#3120. #2983.	6.558. 5954.	*15.3		•
	5 S	230,0	•118.27 •123.41	-62.0 -61.6	*108°3	-124.8	4986.	-2875. -2803.	5756.	=7.4 =5.5		, ₁
	90	250.0	-128.55 -133.70	•61.6 •61.6	-107.7	124.1	4772.	-2754	5419.	9.0		r
	63	270.0	-138.84 -145.98	-61.6 -61.6	-107.8	-124.3	4633.	-2673. -2634.	5349.	o n .		
	3 W	240,0	-149.12	61.7	-107.2	123.7	4689	-2598,	SIAT.	96		

		3 3	1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	120.6	200	-2551.	\$000°	6 A	
	•	> 4		2 0	> 6 4 1	- ac	•		
	LOAD CONDITION 1			1			HAVE ANGLE &	00.00	
• • •	TALE COLUMN COLU	×	4 8 P		×	HUDEINE HOME!	MANAGENT MOMENTANCES MANAGES MAN	VFRTICAL FORCE KIPB	
	*154.55	.59.1	102.0	1117.0	4162.	•2413. •2315.	4620.	7.0	
	1 7 £ . Ø 3	.55,3	3 0 1	4.109.a	3600.	-2225.	4410.	e	
	:								
,									
	! !								
 									

		Coll.	
S : 2			
£ : 6			
2 8	ANNUS CAULANNA		
2 3 8	MAVE NUMBER B	MAVE OTRECTION # 60,000	
a r a	X SHEAR FORCE B	ala, 2120 KIPS	
	Y SHEAR FORCE #	746,1377 KIP3	
. 8	RESULTANT SHEAR FORCE B	8513, 4009 KIPB	
	X MUDLINE MOMENT &	#61570_1077 FT#KIPB	
	A MUDITINE MOMENT B	SUSUI. 6468 FT = KIPS	
· • • • • • • • • • • • • • • • • • • •	REGULTANT MUDLINE HUMENT .	70108.6404 FT-KIP8	
	Z VERTICAL FORCE R	SPIN NOIS.	
in office			
·			
4. • •			
		•	1

gest innoval analist statistic innoval analis statistic proper second analis

6

UNITED COMPUTING 67. APEX/SL 8.6.0

				222
	= = = =		***	>>>> >>>>
07/19/76.			1 H H H H H 1 H 1 H 1 H 1 H 1 H 1 H 1 H	
15,11,13, 07,	77 777777777777777777777777777777777777	77 27 27 27 27	77 72 72 73	1112112121212 271212121212 2 2
15	***	1	***	222
		***	**	
	533	3333	3333	ักกกกกก กกกกกกกกกกกกกกกกกกกกกกกกกกกกกก
	333	33333	 2333 6663	ממחת מחת מחת מחת מחת מחת מחת מחת מחת מחת
				444

57 FT WAVE HEIGHT

13.2 SEC WAVE PERIOD

(2.5 Knot)

12.00	F)		•		1
1700 - 17		0 E F F I C 1 E	A B L E R E P O R T	# # # # # # # # # # # # # # # # # # #	
000000 0000000 00000000 00000000 000000	DIAMETER	URAG	TANG URAG COEF	MABS	
000000000000000000000000000000000000000	12,000	7400	0000.0=	0078.	
000000000000000000000000000000000000000	36,000	0007.	00000	1,3400	
000000	72,000	0014	000000000	0028.5	
	184.000	. 7400	0000*0=	00404	
		-			

	U.S. NAVY - ACMR STRUCTURES MLW 105 FT
	ST FT WAVE HEIGHT
	C. CKERN
	JULY, 1976
	27-771-01
 	IMPUT UNITSENGLISH
	DUTPUT UNITS
اً الله الله	
ا انت	
2 10	
_	

The second and the second of t

T.

-,61075395E-63 40041056 -. 34503876E-02 .99152762 . 88469563E=01 3.0238185 WAVE PROFILE TABLE 8.5079400 1,3291466 FT/SEC 15.7.000 15.7.000 15.7.000 15.7.3.000 15.7.3.000 15.7.3.000 15.7.3.000 15.0000 15.000 15.000 15.000 15.000 15.000 15.000 15.000 15.000 15.0000 15.000 15.000 15.000 15.000 15.000 15.000 15.000 15.000 15.0000 15.000 15.000 15.000 15.000 15.000 15.000 15.000 15.000 15.0000 15.0 #0200581E-05 4425465E-02 9.8594854 25.075211 41631441E+0 .2176312 23.542731 .15055725 93123023 14200577 .4717313 8.472356n 4.3667914 2.7132101 965960 LAMHOA MAVE PERIUD MAVE LENGTH HAVE CELEHITY 10 65 D1 T0 05 DEPTH(FT)= 150.2 <u>...</u>

REPORT

CONSTANTS

× ×

SHOP B TOKES

Ğ

1

Ğ

00.09 =	VERTICAL / FORCE KIP8 2	13.6	16.4 16.0	17.0	21.7	25.5 27.6	20° 5	37.9	4 4 4 4 5 4	55. N. S. S. S. S. S. S. S. S. S. S. S. S. S.	63.2 71.0	70.8	96.2	122.7	125.5
MAVE ANGLE	POLNT X Y ROLLT NOT NOT NOT NOT NOT NOT NOT NOT NOT NO	3520	3173.	2350. 1882.	1374.	299.	1964.	2796. 3718.	4726. 5823.	7015.	9929.	14354.	20784.	. 30110. 35503.	41143.
	-HUDLINE HOME	-1940.	-1621. -1428.	-1216.	-737	1145.	526.	1319.	2226. 2705.	3295.	2629.	6682. 8051.	9645.	13978.	19251.
	×	3306.	2728.	2010.	1159.	112.	•1084. •1746.	•2465. •3279.	-4169. -5135.	• 1993 • 7389	18774° 1055°	-12704.	-18411.	-26669. -31362.	-36361.
	α •	1 99.1	- 82.4 - 72.5	1 49.7	736.9	+ 8.2	+ 24.0	+ 59.2	+ 115.0	+134.6	+179.0	+240.5 +279.8	+320.5	+ 4444.0	+581.3 +054.7
	I >	.48.3	-70.7	-52.4	- 30.8 - 18.2	2,2	37.2	5.0	20 TO TO TO TO TO TO TO TO TO TO TO TO TO	118.4	157.4	211.9	336.9	392.2	512.0 576.5
	• ×	4.00.4	-42.4	.32,2	-20.3	1.7	10.0	27.3	25° 4	74.1	45.3	113,8	153.8	242.4	310.2
CONDITION	ANG.18 OF TO STANCE	171.45	151.93	152.40	142,68	135,35	125.63	114.30	104.78	95.25	85.73	76.20	66.68	57,15	47.63
רטעט כו	AND CHEST	.360.0	-340.0 -330.0	-320.0 -310.0	-300°0 -240°0	-260.0	-260.0	-240.0 -230.0	-220.0	-200.0	180.0	150.0	•140.0 •130.0	-120.0	10000

70570. 38.7
MAYE ANGLE B 60,00
A A A B A B B B B B B B B B B B B B B B
DUTNE HOMENTS SELECTIONS NOTE A ROLL SALES.
> x x x x x x x x x x x x x x x x x x x
z 0
- H O O d H O O O O O O O O O O O O O O O
10
CONDITION 1
LOAD COND

1040 CUNDITION 1 1056 CUNDITION 1 1066 14 2	MAVE ANGLE 60.00
**************************************	i i
MG, 44 VE NG, 44 VE U-31 RLPS (UEG) X Y KIPS KIPS HSI -62,9 -126,9	į
0.0.6.9 X Y Y R. 1.0.0.8.8.8.8.8.8.8.8.8.8.8.8.8.8.8.8.8.	VERTICAL FURCE
-8565109.6 - 126.5 4491. -4063.1 - 109.6 - 126.7 4491. -4062.6 - 109.6 - 125.7 4357. -9362.1 - 107.5 - 124.1 4273. -94102.6118.5 4020.	
17 -62,6 -109,6 -128,7 0357, -62,6 -108,6 -128,7 0357, -93 -62,1 -107,5 -124,1 0273, -94 -105,6 -118,5 0020, -95,0 -102,6 -118,5 0020,	5221, .1
.69 -61.1 -107.5 -124.1 4273, .69 -61.1 -105.3 -121.7 4157, .45 -59.6 -102.4 -118.5 4020,	5114. 5033.
.45 -59,6 -102,4 -118,5 ±020,	

WAVE DIRECTION # 60.000 90448,2157 FT-KIPS 42379.7094 FT-KIPS 679905,1935 FT-KIPS 518,7518 KIP8 **** COAO SUNNARY REPURT **** 841 0010 AIPS -46.0527 KIPS 1081.5375 KIPS X SHEAR PORCE . T SHEAR FORCE & RESULTANT SHEAR FONCE . X MUDLINE HOMENT'S RESULTANT MUDLINE MUMENT & W MUDLINE MOMENT M Z VERTICAL FORCE # MAVE NUMBER

) SOCIETY PROCESSION OF THE PR

DTIG END